

EARLY DAYS  
OF TV: WHAT EVER  
HAPPENED TO CHANNEL 1?

\$1.25 MAR. 1982

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| MD 577-01, 10, 16 | 34.80 |
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| FD 32 or 34-8000  | 44.95 |
| FD 34-4001        | 48.60 |

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|-------------------------------------|-------|
| 5 1/4" PLASTIC LIBRARY CASE         | 2.50  |
| 8" PLASTIC LIBRARY CASE             | 3.50  |
| PLASTIC STORAGE BINDER w/ Inserts   | 9.95  |
| PROTECTOR 5 1/4" (50 Disk Capacity) | 21.95 |
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| ANADEX DP 9501               | 1295.00 |
| C-ITOH 25 CPS PARALLEL       | 1440.00 |
| C-ITOH 25 CPS SERIAL         | 1495.00 |
| C-ITOH 45 CPS PARALLEL       | 1770.00 |
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| EPSON MX-80 F/T              | \$CALL  |
| EPSON MX-100 GRAPHIC         | \$CALL  |
| EPSON GRAFTRAX               | 90.00   |
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| IDS-560G PAPER TIGER         | 1195.00 |
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| NEC SPINWRITER 7730 P. RO    | 2645.00 |
| NEC SPINWRITER 7700 D SELLUM | 2795.00 |
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| OKIDATA MICROLINE 80         | 389.00  |
| OKIDATA MICROLINE 82A        | 569.00  |
| OKIDATA MICROLINE 83A        | 799.00  |
| OKIDATA MICROLINE 84         | 1199.00 |
| QUME 9/45                    | 2149.00 |
| MALIBU 200 DUAL MODE         | 2695.00 |

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|------------------------|--------|
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| ABT APPLE KEYPAD       | 119.00 |

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|----------------------------------|--------|
| MICROSOFT Z-80 SOFTWARE          | 299.00 |
| MICROSOFT RAMCARD                | 159.00 |
| VIDEX 80 x 24 VIDEO CARD         | 299.00 |
| VIDEX KEYBOARD ENHANCER II       | 129.00 |
| VIDEX ENHANCER REV 0-6           | 99.00  |
| VIDEX SOFT SWITCH                | 29.00  |
| M & R SUPERTERM 80 x 24 VIDEO 80 | 315.00 |
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| NEC 13" COLOR MONITOR            | 399.00 |
| SANYO 12" MONITOR (B & W)        | 249.00 |
| SANYO 12" MONITOR (GREEN)        | 269.00 |
| SANYO 13" COLOR MONITOR          | 469.00 |
| SSM AIO BOARD (INTERFACE) A & T  | 165.00 |
| SSM AIO BOARD (INTERFACE) KIT    | 135.00 |
| ZENITH 13" HI RES. GREEN MON     | 139.00 |
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| T/G JOYSTICK                     | 54.95  |
| T/G PADDLE                       | 34.95  |
| VERSA E-Z PORT                   | 21.95  |
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| MICRO SCI A40 W/O CONTROLLER     | 409.00 |
| MICRO SCI A70 W/CONTROLLER       | 629.00 |
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| PROMETHEUS VERSACARD             | 229.00 |

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|-------------------------------|--------|
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| NOVATION D-CAT DIRECT CONNECT | 165.00 |
| NOVATION AUTO-CAT AUTO ANS    | 219.00 |
| NOVATION APPLE-CAT            | 349.00 |
| UDS 103 LP DIRECT CONNECT     | 175.00 |
| UDS 103 JLP AUTO ANS          | 209.00 |
| HAYES MICROMODEM II (APPLE)   | 299.00 |
| HAYES 100 MODEM (S-100)       | 325.00 |
| HAYES SMART MODEM (RS-232)    | 249.00 |
| HAYES CHRONOGRAPH             | 225.00 |
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| ISO-2 6-SOCKET | 53.95 |

## BARE DRIVES

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| 100-3 SINGLE HEAD 80 TRK | 299.00 |
| 100-4 DUAL HEAD 80 TRK   | 429.00 |

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| APPLE    |        |
| FORTRAN* | 165.00 |

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| BASIC COMPILER*         | 315.00 |
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| Z-80 SOFTWARE           | 299.00 |
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## APPLE SOFTWARE

|                                 |        |
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| DB MASTER (NEW)                 | 179.00 |
| PFS: PERSONAL FILING SYSTEM     | 79.00  |
| PFS: REPORT                     | 79.00  |
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## NEW! Bearcat® 350

**The Ultimate Synthesized Scanner!**  
List price \$599.95/CE price \$399.00/\$50.00 rebate  
Your final cost is a low \$349.00

**7-Band, 50 Channel • Alpha-Numeric • No-crystal scanner • AM Aircraft and Public Service bands • AC/DC Bands: 30-50, 118-136 AM, 144-174, 421-512 MHz.** The new Bearcat 350 introduces an incredible breakthrough in synthesized scanning: Alpha-Numeric Display. Push a button—and the Vacuum Fluorescent Display switches from "numeric" to word descriptions of what's being monitored. 50 channels in 5 banks. Plus, Auto & Manual Search, Search Direction, Limit & Count, Direct Channel Access, Selective Scan Delay, Dual Scan Speeds, Automatic Lockout, Automatic Squelch, Non-Volatile Memory. Order your Bearcat 350 today!

## Bearcat® 300

List price \$549.95/CE price \$349.00/\$50.00 rebate  
Your final cost is a low \$299.00

**7-Band, 50 Channel • Service Search • No-crystal scanner • AM Aircraft and Public Service bands • Priority Channel • AC/DC Bands: 30-50, 118-136 AM, 144-174, 421-512 MHz.** The Bearcat 300 is the most advanced automatic scanning radio that has ever been offered to the public. The Bearcat 300 uses a bright green fluorescent digital display, so it's ideal for mobile applications. The Bearcat 300 now has these added features: Service Search, Display Intensity Control, Hold Search and Resume Search keys, Separate Band keys to permit lock-in/lock-out of any band for more efficient service search.



## NEW! Bearcat® 350

## FREE Bearcat® Rebate Offer

Get a coupon good for a \$50 rebate when you purchase a Bearcat 350 or 300. \$25 rebate on model 250 or 20/20. \$15 rebate on model 210XL. \$10 rebate on model 160 or 4-6 Thin Scan. To get your rebate, mail rebate coupon with your original dated sales receipt and the Bearcat model number from the carton to Electra. You'll receive your rebate in four to six weeks. Offer valid only on purchases made between February 1, 1982 and March 15, 1982. All requests must be postmarked by March 31, 1982. Limit of one rebate per household. Coupon must accompany all rebate requests and may not be reproduced. Offer good only in the U.S.A. Void where taxed or prohibited by law. Resellers, companies, clubs and organizations—both profit and non-profit—are not eligible for rebates. Employees of Electra Company, their advertising agencies, distributors and retailers of Bearcat Scanners are also not eligible for rebates. Please be sure to send in the correct amount for your scanner. Pay the listed CE price in this ad. Do not deduct the rebate amount since your rebate will be sent directly to you from Electra. Orders received with insufficient payments will not be processed and will be returned. Offer subject to change without notice.

## Bearcat® 250

List price \$429.95/CE price \$279.00/\$25.00 rebate  
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## NEW! Bearcat® 20/20

List price \$449.95/CE price \$289.00/\$25.00 rebate  
Your final cost is a low \$264.00

**7-Band, 40 Channel • Crystallless • Searches AM Aircraft and Public Service bands • AC/DC Priority Channel • Direct Channel Access • Delay** Frequency range 32-50, 118-136 AM, 144-174, 420-512 MHz. The Bearcat 20/20 automatic scanning radio replaces the Bearcat 220 and monitors 40 frequencies from 7 bands, including aircraft. A two-position switch, located on the front panel, allows monitoring of 20 channels at a time.

## Bearcat® 210XL

List price \$349.95/CE price \$229.00/\$15.00 rebate  
Your final cost is a low \$214.00

**6-Band, 18 Channel • Crystallless • AC/DC** Frequency range: 32-50, 144-174, 421-512 MHz. The Bearcat 210XL scanning radio is the second generation scanner that replaces the popular Bearcat 210 and 211. It has almost twice the scanning capacity of the Bearcat 210 with 18 channels plus dual scanning speeds and a bright green fluorescent display. Automatic search finds new frequencies. Features scan delay, single antenna, patented track tuning and more!

## Bearcat® 160

List price \$299.95/CE price \$194.00/\$10.00 rebate  
Your final cost is a low \$184.00

**5-Band, 16 Channel • AC only • Priority Dual Scan Speeds • Direct Channel Access** Frequency range: 32-50, 144-174, 440-512 MHz. The Bearcat 160 is the least expensive Bearcat crystallless scanner. Smooth keyboard. No buttons to punch. No knobs to turn. Instead, finger-tip pads provide control of all scanning operations.

## NEW! Bearcat® 100

**The first no-crystal programmable handheld scanner.** Allow 30-120 days for delivery after receipt of order due to the high demand for this product.

List price \$449.95/CE price \$299.00  
**8-Band, 16 Channel • Liquid Crystal Display Search • Limit • Hold • Lockout • AC/DC** Frequency range: 30-50, 138-174, 406-512 MHz.

The world's first no-crystal handheld scanner has compressed into a 3" x 7" x 1 1/4" case more scanning power than is found in many base or mobile scanners. The Bearcat 100 has a full 16 channels with frequency coverage that includes all public service bands (Low, High, UHF and "T" bands), the 2-Meter and 70 cm. Amateur bands, plus Military and Federal Government frequencies. It has chrome-plated keys for functions that are user controlled, such as lockout, manual and automatic scan. Even search is provided, both manual and automatic. Wow... what a scanner!

The Bearcat 100 produces audio power output of 300 milliwatts, is track-tuned and has selectivity of better than 50 dB down and sensitivity of 0.6 microvolts on VHF and 1.0 microvolts on UHF. Power consumption is kept extremely low by using a liquid crystal display and exclusive low power integrated circuits.

Included in our low CE price is a sturdy carrying case, earphone, battery charger/AC adapter, six AA Ni-cad batteries and flexible antenna. For earliest delivery from CE, reserve your Bearcat 100 today.

### TEST ANY SCANNER

Test any scanner purchased from Communications Electronics™ for 31 days before you decide to keep it. If for any reason you are not completely satisfied, return it in original condition with all parts in 31 days, for a prompt refund (less shipping/handling charges and rebate credits).

## Bearcat® Four-Six ThinScan™

List price \$189.95/CE price \$124.00/\$10.00 rebate  
Your final cost is a low \$114.00

Frequency range: 33-47, 152-164, 450-508 MHz. The incredible, Bearcat Four-Six Thin Scan™ is like having an information center in your pocket. This four band, 6 channel crystal controlled scanner has patented Track Tuning on UHF, Scan Delay and Channel Lockout. Measures 2 3/4 x 6 1/4 x 1 1/4". Includes rubber ducky antenna. Order crystal certificate for each channel. Made in Japan.

## Fanon Slimline 6-HLU

List price \$169.95/CE price \$109.00  
**Low cost 6-channel, 3-band scanner!**

The Fanon Slimline 6-HLU gives you six channels of crystal controlled excitement. Unique Automatic Peak Tuning Circuit adjusts the receiver front end for maximum sensitivity across the entire UHF band. Individual channel lockout switches. Frequency range 30-50, 146-175 and 450-512 MHz. Size 2 3/4 x 6 1/4 x 1 1/4". Includes rubber ducky antenna. If you don't need the UHF band, get the Fanon model 6-HL for \$99.00 each, and save money. Same high performance and features as the model HLU without the UHF band. Order crystal certificates for each channel. Made in Japan.

### OTHER SCANNERS & ACCESSORIES

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| NEW! Regency† D300 Scanner                         | \$219.00 |
| NEW! Regency† D100 Scanner                         | \$169.00 |
| NEW! Regency† H604 Scanner                         | \$129.00 |
| Regency† M400 Scanner                              | \$259.00 |
| Regency† M100 Scanner                              | \$199.00 |
| Regency† R1040 Scanner                             | \$149.00 |
| SCMA-6 Fanon Mobile Adapter/Battery Charger        | \$49.00  |
| CHB-6 Fanon AC Adapter/Battery Charger             | \$15.00  |
| CAT-6 Fanon carrying case with belt clip           | \$15.00  |
| AUC-3 Fanon auto lighter adapter/Battery Charger   | \$15.00  |
| PSK-6 Base Power Supply/Bracket for SCMA-6         | \$20.00  |
| SP50 Bearcat AC Adapter                            | \$9.00   |
| SP51 Bearcat Battery Charger                       | \$9.00   |
| SP58 Bearcat 4-6 ThinScan™ carrying case           | \$12.00  |
| MA506 Regency carrying case for H604               | \$15.00  |
| FB-E Frequency Directory for Eastern U.S.A.        | \$12.00  |
| FB-W Frequency Directory for Western U.S.A.        | \$12.00  |
| FFD Federal Frequency Directory for U.S.A.         | \$12.00  |
| TSG† Top Secret† Registry of U.S. Government Freq. | \$10.00  |
| ASD Frequency Directory for Aircraft Band          | \$10.00  |
| B-4 1.2 V AAA Ni-Cad batteries (set of four)       | \$9.00   |
| A-135cc Crystal certificate                        | \$3.00   |

Add \$3.00 shipping for all accessories ordered at the same time.

### INCREASED PERFORMANCE ANTENNAS

If you want the utmost in performance from your scanner, it's essential that you use an external antenna. We have six base and mobile antennas specifically designed for receiving all bands. Order #A60 is a magnet mount mobile antenna. Order #A61 is a gutter clip mobile antenna. Order #A62 is a trunk-lip mobile antenna. Order #A63 is a 3/4 inch hole mount. Order #A64 is a 3/8 inch snap-in mount, and #A70 is an all band base station antenna. All antennas are \$35.00 and \$3.00 for UPS shipping in the continental United States.

### BUY WITH CONFIDENCE

To get the fastest delivery from CE of any scanner, send or phone your order directly to our Scanner Distribution Center. Be sure to calculate your price using the CE prices in this ad. Michigan residents please add 4% sales tax. Written purchase orders are accepted from approved government agencies and most well rated firms at a 10% surcharge for net 10 billing. All sales are subject to availability, acceptance and verification. All sales on accessories are final. Prices, terms and specifications are subject to change without notice. Out of stock items will be placed on backorder automatically unless CE is instructed differently. Most products that we sell have a manufacturer's warranty. Free copies of warranties on these products are available prior to purchase by writing to CE. International orders are invited with a \$20.00 surcharge for special handling in addition to shipping charges. All shipments are F.O.B. Ann Arbor, Michigan. No COD's please. Non-certified and foreign checks require bank clearance. Minimum order \$35.00.

Mail orders to: Communications Electronics™, Box 1002, Ann Arbor, Michigan 48106 U.S.A. Add \$7.00 per scanner or phone product for U.P.S. ground shipping and handling, or \$14.00 for faster U.P.S. air shipping to some locations. If you have a Visa or Master Card, you may call anytime and place a credit card order. Order toll free in the U.S.A. Dial 800-521-4414. If you are outside the U.S. or in Michigan, dial 313-994-4444. Dealer inquiries invited. Order without obligation today!

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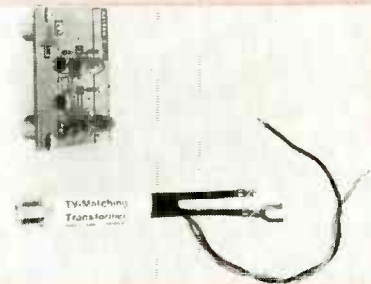
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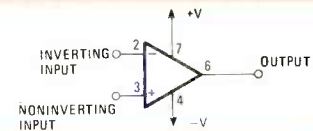
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**ON THE COVER**

So far, the only way you could hear real digital sound reproduced on your own equipment was to invest in a \$3000 PCM attachment for your VCR. Shortly, though, digital audio, using your existing amplifier and speakers, will be available for about the cost of a good turntable. New techniques—particularly in the area of laser scanning—will put 60 minutes of ultra-high-fidelity audio on one side of a disc you can hold in the palm of your hand. To find out what's in store, and how it works, turn to page 39.



**GOOD UHF TELEVISION RECEPTION** has always been more difficult to get than VHF. Part of the solution lies in a good antenna-system. An antenna-mounted preamplifier can also help. A preamp you can build that offers 25-dB of gain is described starting on page 59.



**OPERATIONAL AMPLIFIERS (OP-AMPS)** are an important—but frequently misunderstood—member of the IC family. Learn what makes them so useful and how to work with them beginning on page 54.

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# VIDEO ELECTRONICS

DAVID LACHENBRUCH  
CONTRIBUTING EDITOR

## VCR DILEMMA

How to cope with the legal problems posed by the technological revolution is becoming a major political issue. Nowhere else is that as evident as it is in the case of home videotaping. In this instance, the immediate issue is whether private individuals who tape copyrighted programs off the air, or from cable TV, should pay for the privilege—and if so, how. The Appeals Court ruling in the Betamax case held that taping of such shows for personal viewing is a violation of the Copyright Law, and that manufacturers and sellers of VCR's are contributory infringers of the law. The three-judge court's decision indicated strongly that because Congress hadn't considered video technology when it passed the recent, revised, Copyright Law, perhaps congressional action would be necessary to cope with the problem.

Although the decision is being appealed to the Supreme Court, the action is likely to occur in Congress, where legislation has been introduced both to permit free taping and to add a fee to VCR's and/or videocassettes to be paid to the copyright holders of TV programs. The major antagonists are the electronics manufacturers, represented by the EIA, and the big movie companies, represented by Motion Picture Association of America. The EIA and its adherents argue that "time-shift" taping is merely another way of viewing a program at a more convenient time, accomplished in the privacy of the taper/viewer's home, and that the copyright owner of the program has already been paid for the televising of the show. The MPAA counters that home taping robs the copyright owner of his product without compensation and, at the very least, diminishes the value of the program in re-runs.

## RENTABETA

In pre-recorded videocassettes, rental is becoming a major business. One study has indicated that for every program cassette sold, 20 are rented. But in the past, movie-cassette rental was open only to the 3% of the population who owned video recorders. Now the opportunity is being extended to the other 97%—the non VCR owners—through Rentabeta, developed by Superscope.

The principle of Rentabeta is simple—"the take-home movie in a video player." The rental package includes a Toshiba portable VCR, specially modified so that it is a play-only machine, in a case which can be locked by the dealer so the cassette cannot be removed. The customer chooses the cassette he wishes, it's loaded by the dealer into the player, and he carries the entire package home. Although rentals are expected to differ from dealer to dealer, the suggested price for rental of a machine loaded with one cassette is \$8. Dealers may supply more than one cassette and leave the player unlocked so that the viewers can change cassettes themselves. Rentabeta players can be modified so they can't be rewound, permitting each cassette to be viewed only once. That has been suggested as a possible method of keeping positive track of the number of times each cassette has been viewed, so that producers of the rented movies can be paid royalties.

## KODAK ANSWERS SONY

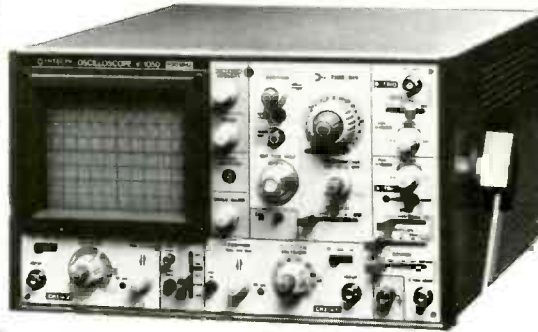
Responding to Sony's Mavica electronic still-camera (see **Radio-Electronics**, January 1982), Eastman Kodak President Colby Chandler said that his company had the capability to build an all-electronic camera. However, the solid-state sensor alone would cost as much as an entire film-camera, and picture information per frame would be about one-quarter that of a 110-size film frame or  $1/20$  of a 35-mm frame. He said that an electronic sensor with a million picture elements could make an acceptable 2×4-inch print, but he noted that a 110 frame has more than 2 million elements, and 35mm over 10 million (while Sony's Mavica sensor has 280,000).

He hinted at a possible Eastman Kodak electronic film-viewing system combining chemical and electronic technology, in these words: "Along with their initial print order, users of such a system might receive an image carrier that drops easily into a videoplayer attached to a TV set. With a hand-held remote unit, consumers might have selective control of images on the TV screen. At the touch of a button, the user could enlarge its image and freeze it for closer viewing. At the touch of another, the viewer could encode the film frame. Now the image—as the viewer has chosen to see it—would return to view in the form selected, when next it is inserted in the player." He indicated that that is one product being evaluated for the consumer market. **R-E**



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# WHAT'S NEWS

## New device cuts HV transmission losses

A new type of thyristor (silicon controlled rectifier) that promises to slash operating costs of high-voltage direct current (HVDC) power-transmission lines, was described by GE scientist Victor Temple at the International Electron Devices Meeting at Washington, DC, last December. Thyristors are power semiconductor-devices that are used to switch and control large amounts of electric power, turning it on and off in a few microseconds.

HVDC lines can carry twice as much power as AC lines with the same peak voltage rating,

thus slashing transmission costs. But the high costs of the converter stations that turn the AC into DC for long-distance transmission and back into AC for local distribution can cut deeply into those savings.

Thyristors for HVDC application are made from thin, .04-inch thick slices of silicon that are three inches in diameter. Normally they are activated by an electrical gate current. The new thyristor is activated by weak pulses of light carried on fiber-optic cables. Because of its innovative design, it can handle large currents while consuming little power itself, thus reducing converter-station losses.

Light-activated thyristors are

not new, but all previous types have had the disadvantage that the weak gate signal activates only a small portion of the thyristor. The current pouring through heats that portion to unsafe temperatures, and may cause melting breakdown.

In the new thyristor, resistors inserted in the silicon wafer between amplifying stages limit the current to safe levels. A resistor is etched in the wafer between the gate-amplifying stage and the pilot-amplifying stage. Another resistor is inserted between the pilot and the main stage.

In addition to HVDC converter stations, GE's light-fired thyristor has potential power-control applications in heavy industry, such as steel mills, and in locomotives.

## Tektronix opens direct mail center

On January 1, 1982, Tektronix opened a direct-order channel, through which purchasers, by calling a toll-free number, may obtain information or order instruments.

The National Marketing Center, in Beaverton, OR, will expand customer service as well as meet the needs of new electronics purchasers. By calling 1-800-547-1845, customers can reach experienced sales engineers who will supply immediate technical consultation, applications assistance, and answers to a wide variety of measurement and safety problems.

The Center offers a direct contact for customers who purchase just one or two instruments and would not normally be served by a field service engineer.

The toll-free number will be staffed from 5 am EST till 8 pm EST.

## Right to videotape supported by EIA

The right to private citizens to tape television programs for their own use must be protected

by law at once, testified Jack Wayman, Senior Vice President of the Consumer Electronics Group of the Electronic Industries Association, before the U.S. Senate Judiciary Committee. That legislation is necessary, he said, as a result of the recent court decision that holds it illegal for consumers to videotape selected programs off the air, even for private, non-commercial use.

Wayman pointed out that, in general, copyright owners are not damaged by private taping of TV. "Surveys show," he said, "that 70 to 90 percent of all VCR owners use their VCR's primarily to 'time shift'—to view programs they could not have watched at the time of transmission." That kind of taping indirectly benefits the copyright owner by increasing the broadcast audience and thus the value of the program to the broadcaster.

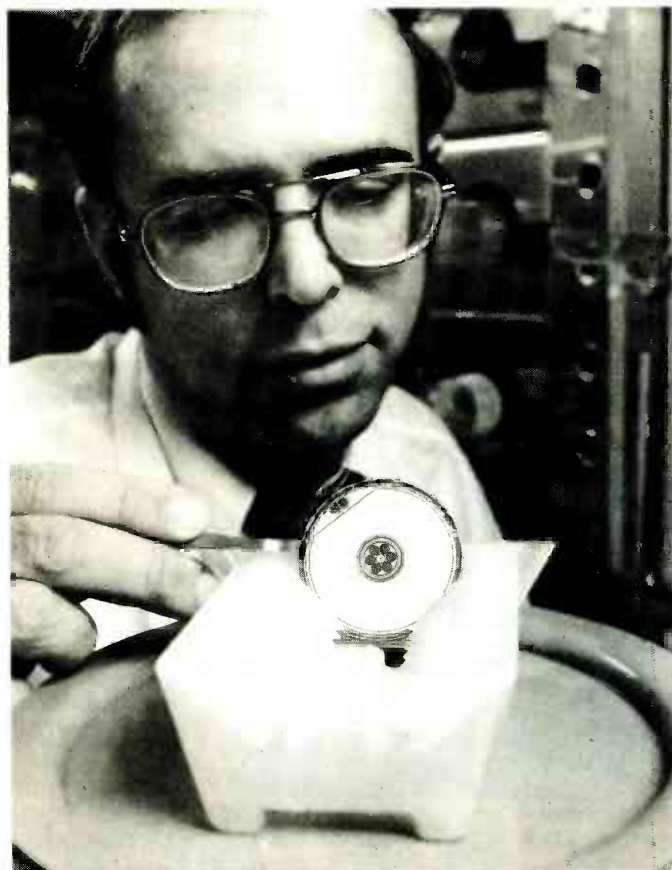
If Senate Bill 1758, legalizing private copying, is not passed immediately, Wayman said, some movie company might obtain an injunction against VCR's. That could cause severe economic damage not only to manufacturers, but to the dozens of American companies that distribute the product, and the more than 25,000 retail outlets that are now selling VCR's as well as blank and pre-recorded tapes. The industry could be paralyzed for a long time, while the matter remained in litigation, possibly going all the way to the Supreme Court.

The analogous right to record audio material has never been seriously challenged, as long as the recordings were not offered for sale, though drastic penalties have been imposed for selling such recordings.

## Fort Worth will get a videotext system

Tandy Corp./Radio Shack plan to install and operate an electronic information base (videotext) in the Fort Worth/Tarrant County area. Objectives will be to provide subscribers with continuously updated information,

*continued on page 12*



GE's NEW THYRISTOR, inspected here by Dr. Victor A.K. Temple, promises great reductions in high-voltage DC power-line costs. Through its innovative design, it can handle large currents while consuming little power itself, reducing the conversion losses of HVDC transmission systems. Work on the device, still in the early developmental stage, is being sponsored by the Electrical Power Research Institute, the research arm of the electric utility industry.



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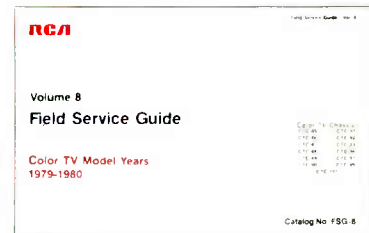
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# WHAT'S NEWS

continued from page 6

on demand, 24 hours a day.

News will be from local, regional, state, and national sources and will include sports, special events, business and financial news, and weather information.

Equipment used will be the TRS-80 Model II computer and the newly developed Communications Multiplexer.

According to Charles Phillips of Radio Shack, "We have not made a final decision on whether or not a subscription fee will be charged, but while much of the information will be free to the viewer, certain items will carry an access charge. We also plan to offer advertisers the opportunity to sponsor certain information pages."

The system will be offered to residents of the test area in early 1982.

## RCA's Satcom III relays cable TV

The third RCA communications satellite, Satcom III-R, launched last November into a geosynchronous orbit 23,000 miles above the equator, is intended to serve customers in the cable-TV industry. The 2,385-pound satellite was placed in position at 132 degrees West. It was the 11th U.S. domestic commercial satellite to go into orbit.

Like the earlier Satcoms, Satcom III-R has 24 transponders each of which can carry 1,400 voice circuits, one FM/color TV transmission, or 64 million bits

per second of computer data.

The Satcom satellites cover all 50 states and Puerto Rico. More than 4,000 earth stations, serving 14 million homes, have access to those spacecraft. Without the spacecraft, thousands of miles of ground cables and microwave links would be required to perform the same service.

Satcom III-R is powered by two solar array panels and three nickel-cadmium batteries. Maximum output is 950 watts at 35 volts (regulated) at the beginning of service and 750 watts at the end of the satellite's 10-year life. The batteries supply power during the two solar eclipse periods that take place each year.

## New high-current cell supplies 5-15 amperes

A new high-current lithium thionyl-chloride cell just announced by the Altus Corp of San Jose, CA, is capable of putting out 5 amperes continuously and up to 15 amperes in short pulses.

The new flat-disc cell, designated the AL250, has an open-circuit voltage of 3.5 volts, operates at temperatures from -40 to +70 degrees centigrade, and can stand prolonged storage at extreme temperatures without noticeable losses in capacity or response time. Its shelf life is estimated at more than 10 years.

The cell is said to be abso-



ALTUS AL250, 3.5-VOLT, 5-AMPERE CELLS

lutely safe under abusive conditions, such as incineration, crushing, or penetration.

## FCC urged to speed satellite TV licenses

The Satellite Television Corporation (STC), a subsidiary of COMSAT, has urged the FCC to process pending direct-broadcast satellite (DBS) applications on an individual basis.

Individual processing will "...eliminate the possibility that consideration of a few troublesome proposals would delay the issuance of authorizations to applicants whose DBS systems clearly will serve the public interest."

STC was the U.S. pioneer in proposing DBS service for the United States. If the FCC moves expeditiously to approve DBS applications in early 1982, STC will be able to initiate its DBS pay-TV service in late 1985, or early 1986.

STC has asked for FCC approval to offer a satellite-to-home subscription television service using DBS satellites. It would offer three channels of premium programming, without advertising. Individual subscribers would receive the scrambled signals using 2½-foot dish antennas.

## New message service between U.S. cities

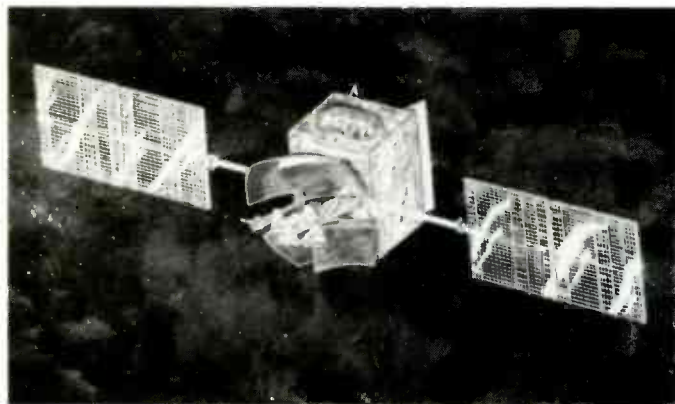
RCA Network Services, an operating unit of RCA Communications, Inc., has filed an application with the FCC to construct and operate a nationwide digital electronic message-service (DEMS) among the nation's fifty major metropolitan areas.

The company believes that the first six areas—Atlanta, Chicago, Houston, Los Angeles, New York, and San Francisco—could be operational within 15 months of FCC approval and that the entire network could be in operation in seven years.

The DEMS network will provide high-speed, end-to-end private-line and switched services to the public. It is designed to handle digital bit-streams at rates ranging from 2.4 kilobits/second to 1.5 megabits/second, offering a flexible service to handle a wide variety of user applications: communicating word-processors, remote computer entry, high-speed facsimile, and videoconferencing.

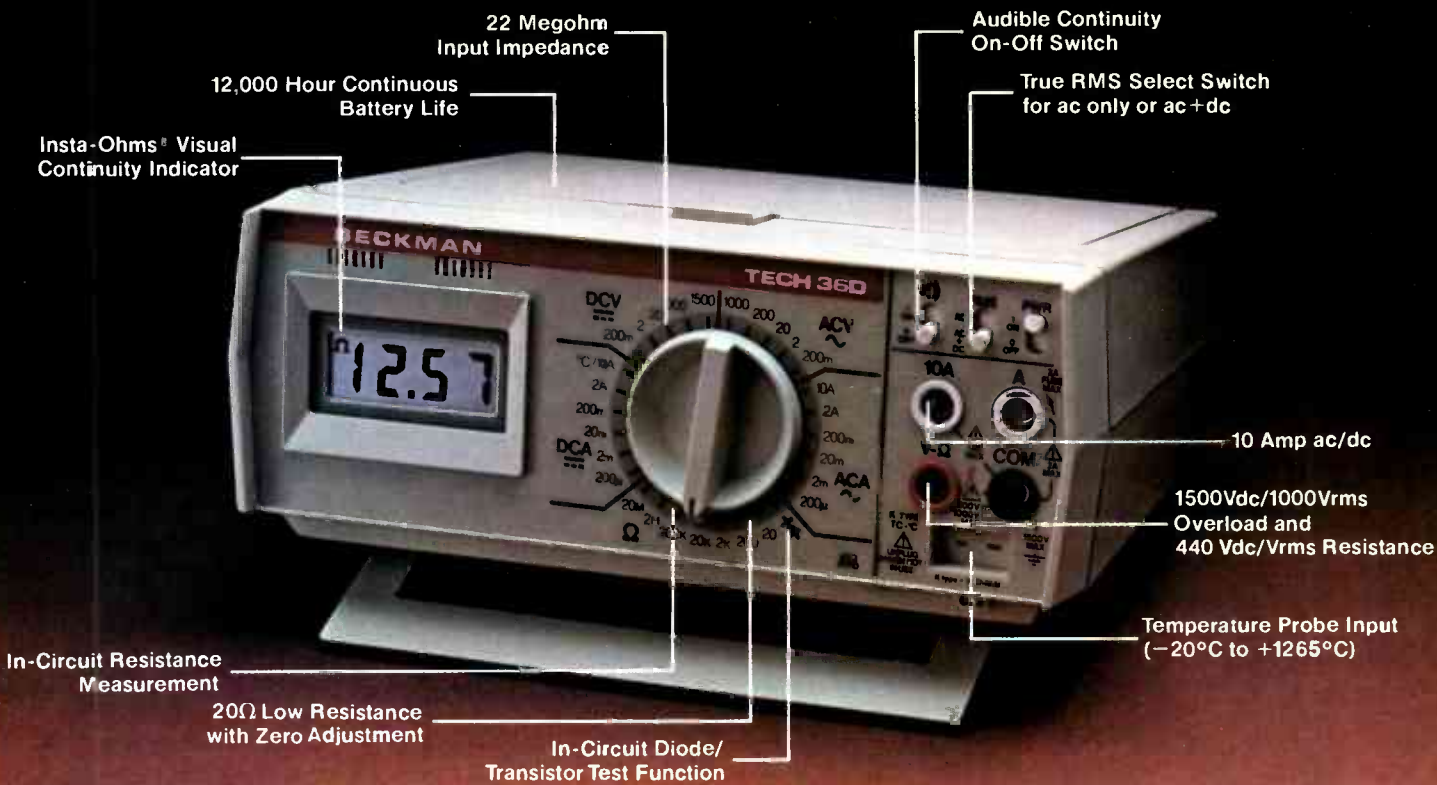
RCA's proposed service will use satellite and microwave facilities for long-haul transmissions and the new Digital Transmission System (DTS) technology for transmission within cities.

R-E



RCA's SATCOM III-R SATELLITE





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Facts from Fluke on low-cost DMM's

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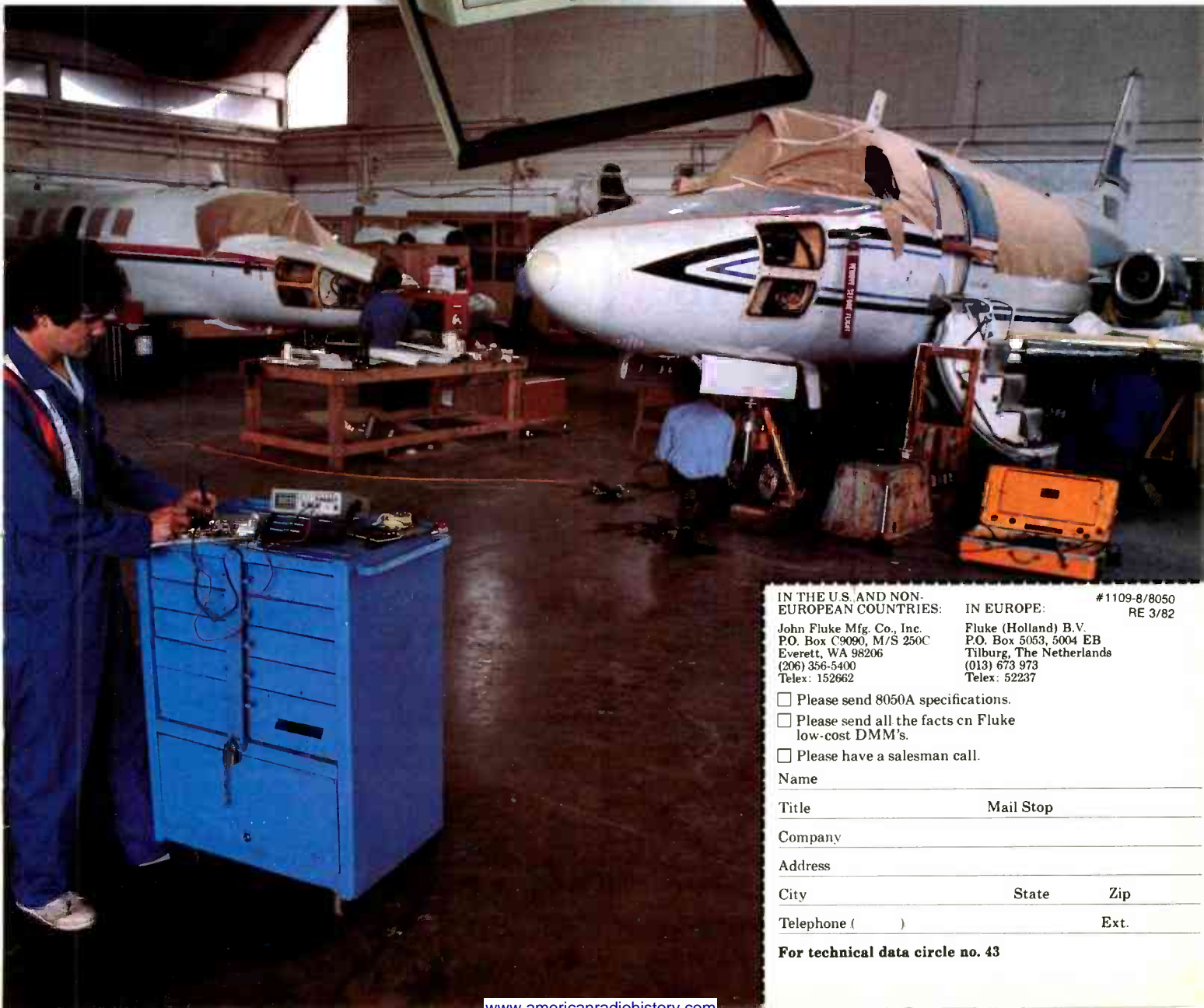
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For technical data circle no. 43

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# LETTERS

## UNICORN-1 ROBOT

I was impressed by the very thorough series of articles, "Unicorn-1 Robot," that appeared in **Radio-Electronics**, August 1980 through June 1981. However, there appear to be a few errors that should be noted.

In the March 1981 issue (page 65), the relay driver circuit will not work as explained in the text. As shown, the 2N2222 transistor and relay will be turned on in absence of a command. That is opposite the condition that is desired. In other words, what is required at the transistor base is a logic-low to de-energize the relay in the stand-by mode.

There are a couple of modifications that can be made without altering the printed-circuit boards. The choices are:

Latch Board: take the output signal from the Q pins 6 and 8, or:

Relay Driver Board: drive the transistor directly from the decoder board or latch board by eliminating the octal inverter

(2813A) and placing jumper wire between input and output pins of the IC socket.

The suggestion to use PNP transistors is not recommended because that places 5-volts across the base-emitter junction and the driver in series; that could damage the transistor.

In the April 1981 issue (page 68), Fig. 80, and (page 69), Fig. 82, the latch board input and output signals on pins 9 and 11 of the 7474 IC are reversed.

WALTER PALANKER,  
Magnolia, NJ

## PROGRAMMING FLAW

I am the proud owner of a new personal computer system, and because of that, your October 1981 issue of **Radio-Electronics** caught my eye. I got a lot out of that issue!

I did a lot of shopping around before I decided on the TRS-80, 16K, color outfit. Along with it, I purchased some software

*continued on page 22*

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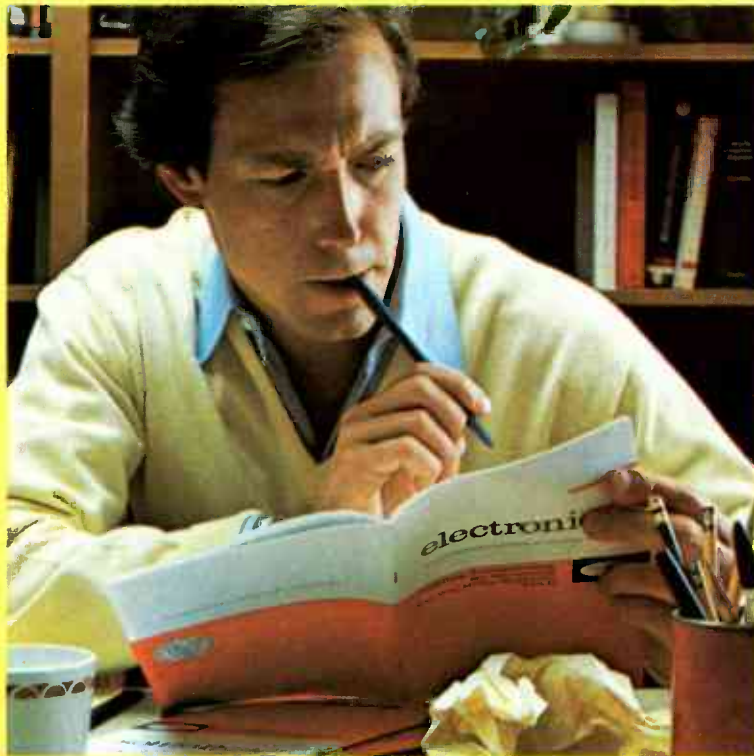
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For some jobs in electronics, you must have a Federal Communications Commission (FCC) License. For others, some employers tend to consider your license a mark in your favor. Either way, your license is government-certified proof of your knowledge and skills. It sets you apart from the crowd.

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Pattern shown on oscilloscope screen is simulated.

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RE--33

## LETTERS

continued from page 16

which included the "Computer Learning Lab." When I ran that particular program I discovered what I thought to be a major flaw in programming. That error was verified by my local dealer. I wrote to Tandy at the address listed in your magazine. That was over a month ago, and I thought that you might be interested to learn that no one has had the decency to acknowledge either the probable software problem or my letter.

Naturally, my impression is that the sales for Tandy stop short of customer service.

Thank you for your attention and for a truly informative magazine.  
MRS. WENDY C. LOOMIS,  
Binghamton, NY

Dear Mrs. Loomis:

Thank you for purchasing a Color Computer from Radio Shack. I am distressed to hear that you discovered a programming bug, notified Radio Shack, and that no one has gotten back to you to solve or confirm your problem.

Not having seen a copy of the article in the October 1981 issue of *Radio-Electronics* to which you referred, and not knowing which address you were told to write to, I cannot comment on why there has been no response to your problem.

The only programming error which we have found since releasing the "Color Computer Learning Lab" is in the chapter covering Sorts (Lesson 14). The sort routine, as shown in the manual and on the tape, will not sort the last value. Changing line 230 as follows will fix the problem:

230 FOR B = A+1 TO N.

That change should be made on pages 93 and 98 of your manual and to the program tape. Our customer-service group has this correction, and should have sent it to you. Any further problems concerning the Color Computer or the software for the Color machine should be sent to: TRS-80 Customer Service, 400 Atrium, One Tandy Center, Ft. Worth, TX 76102.

You should include a phone number where possible, as sometimes it is quicker to call with the information or answer.

Radio Shack believes very strongly in support after sale. I am truly sorry for any inconvenience we may have caused you. Be assured that we will make every effort to assure that it does not happen again.

BARRY O. THOMPSON,  
Product Line Manager—Color Computer

### VHS DECKS

Your magazine and several others continually state that Akai has the only VHS decks with stereo sound. That isn't so; we have several Panasonic NV-8200 VHS decks, as well as some Sony Beta SLO-323 decks, both of which have two-channel audio, and have been giving us excellent service, since we put them into use last summer.

Also, with the increased interest in getting the best audio/video performance from one's own equipment, it might be interesting to your readers if you could come up with a circuit to add video and audio input jacks safely to existing receivers that lack this capability.

JIM CASSEDY,  
Production Technician, Alcon Video/  
Film Prods.,  
San Francisco, CA

### CX DECODER

There are a couple of small corrections to be made to the first part of the "CX Decoder" article, appearing in the December 1981 *Radio-Electronics*.

On page 46, the last sentence in the first paragraph of column 3 should read: "That higher bias also results in a higher gain in the peak mode than in the CX mode when expansion is not taking place." On the schematic, the value of R29 was left out; that should be 1K. I'm sure that I confused the draftsman, because my schematic shows pin 11 of IC4 connected both to -15 volts and ground. In any case, pin 11 of IC4 should go to ground, and not to -15 volts.

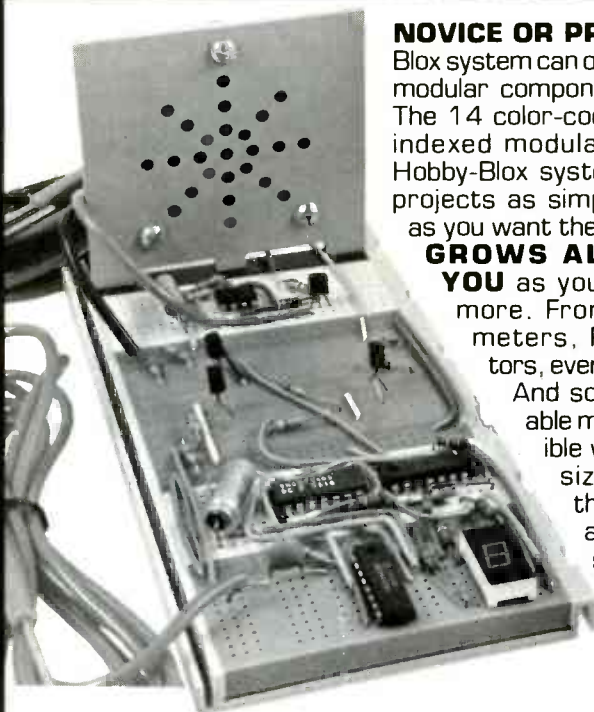
We will pack an errata slip with each kit-part order to catch those three points. The only other potential problem that I noted is that the print of the PC board seems to have blurred lightly, and you may get complains of shorting between adjacent conductors, because the board is so tightly laid out.

Aside from that, I am delighted with the article.

JOEL M. COHEN

R-E

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# SATELLITE/TELETEXT NEWS

GARY ARLEN  
CONTRIBUTING EDITOR

## AUCTION SELLS TRANSPONDERS

In an unusual effort to allocate transponders aboard Satcom IV (which was due to go up in January), RCA Americom—which operates the satellite—sponsored an auction at swanky Sotheby Parke Bernet gallery in New York, better known for selling expensive art items. When the 45-minute action was over, six companies had paid a total of \$90.1 million for the seven transponders which were being offered. The highest bid was \$14.4 million, offered by "Transponder Leasing Co." That bought transponder two, probably for future voice and data communications services. Some names were familiar, and all of them paid more than \$10.7 million per transponder. Among them were Home Box Office, which will operate on transponder 15; RCTV, the new service offering "The Entertainment Channel" of cultural and theatrical performances, which purchased transponder 11; Warner Amex Satellite will use transponder four; UTV Cable Network, a new entertainment and merchandising service, will have transponder 23; Inner City Broadcasting will go on transponder 16, and Bill Batts, an individual representing a Tennessee religious broadcasting group, will transmit on transponder three.

All of those allocations are in addition to the previous commitments—including some video as well as data services—which were already set for the new bird.

Meanwhile, some of the new Satcom IV residents are expanding their other transponder activities. HBO, of course, is well ensconced on several other current and future birds. RCTV recently entered into an agreement with Spanish International Network, which would give RCTV use of another Satcom IV transponder.

## THE FCC'S TELETEXT NON-STANDARD

In keeping with official Washington's policy of "deregulation," the FCC has decided not to establish a formal teletext technical standard for the U.S., choosing instead to let the "marketplace" decide which format should be used. That means that competing French, British, and Canadian technologies will have to fight it out to win allies who will use their respective technologies on U.S. television stations. CBS says that it intends to begin transmitting teletext nationally during 1982; that could encourage its affiliates to adopt the French Antiope format, which CBS favors. Meanwhile, others are beginning to use other formats; for example, WKRC-TV Channel 12 in Cincinnati is planning to test the British Prestel format.

Although it won't adopt formal teletext standards, the FCC is currently considering a number of related technical issues. The Commission will consider the possibility of permitting teletext to be transmitted via lines 14 through 18, plus lines 20 and 21 of the vertical blanking-interval. The FCC is also considering possible future use of lines 10-13, using a phased-in schedule, once it is confirmed that those lines won't cause visual degradation of regular video images on TV receivers.

## AROUND THE SATELLITE CIRCUIT

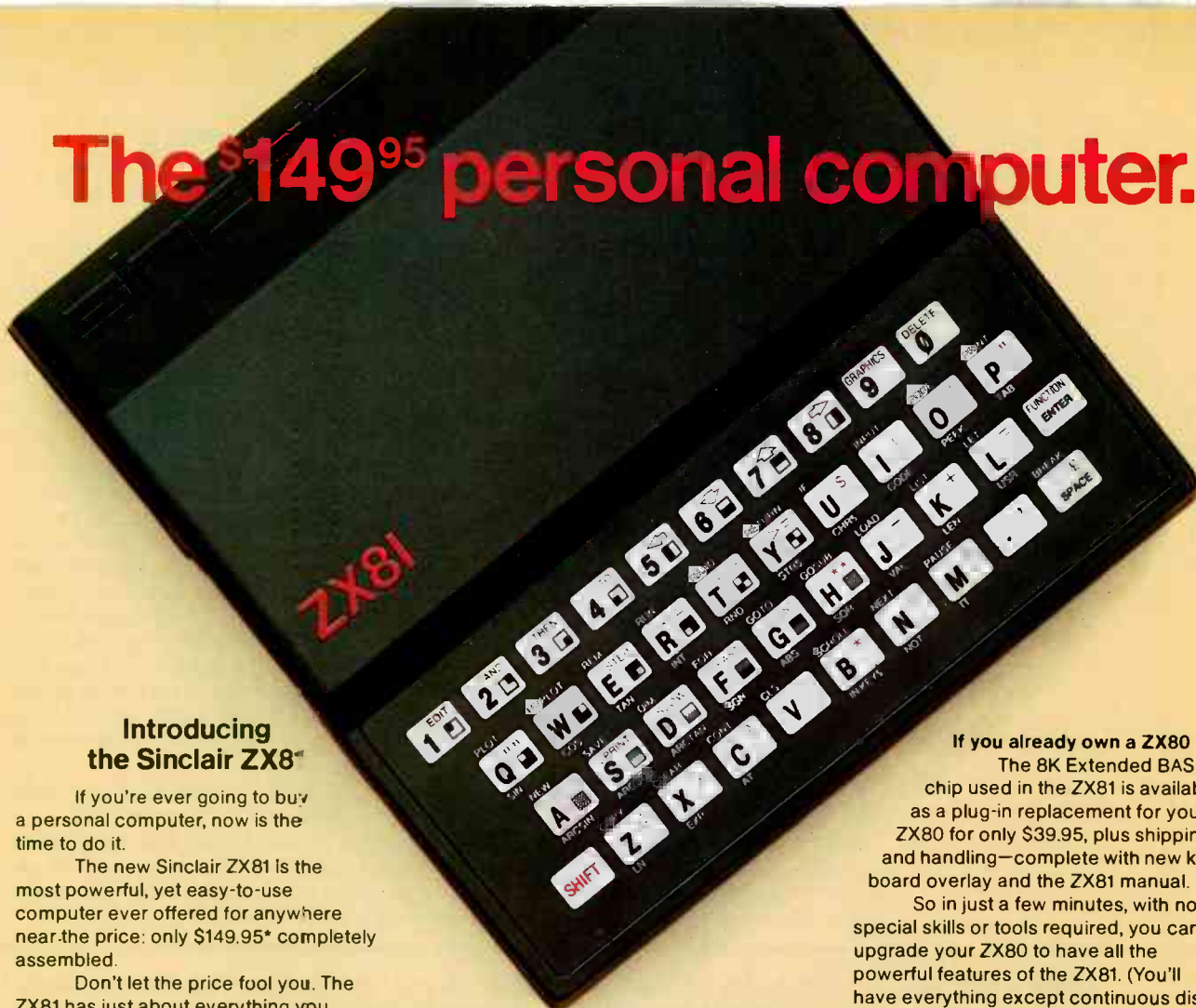
The continuing scramble skyward by several leading program suppliers promises to offer ever-more attractive shows during the coming year. Among the newest entries is "The Disney Channel," a service due to get under way early next year (1983). It will use two transponders aboard Westar V, which will be launched this fall. Walt Disney Productions and Westinghouse Broadcasting are cooperating to develop the 16-hour-per-day channel of pay-cable programming.

**American Satellite Co.** will provide all-digital satellite transmission for the Home Music Store, a new home-recording service offered by Digital Music Co. The electronic feed, due to get under way in July (1982) will provide cable-TV subscribers with master-tape-quality digital music for listening and licensed recording. Cable subscribers will need a special decoder to input the high-quality audio feed into their tape recorders. Music will be uplinked from Los Angeles to ASC's Westar transponders.

**Comsat has proposed** to provide the first full-time satellite TV service from the U.S. to an overseas location. The new service, due to begin in Fall 1982, will permit continuous video transmission from the U.S. to Australia, where it will be used by that nation's Channel 9. Comsat officials say that the type of international feed, which will be uplinked from a new facility in Southern California and travel via a Pacific Intelsat bird, is the forerunner of a "new kind of international TV service which will develop in the next few years."

R-E

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- Built-in interface for ZX Printer
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The ZX81 is also very convenient to use. It hooks up to any television set to produce a clear 32-column by 24-line display. And you can use a regular cassette recorder to store and recall programs by name.

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So in just a few minutes, with no special skills or tools required, you can upgrade your ZX80 to have all the powerful features of the ZX81. (You'll have everything except continuous display, but you can still use the PAUSE and SCROLL commands to get moving graphics.)

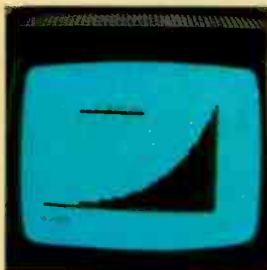
With the 8K BASIC chip, your ZX80 will also be equipped to use the ZX Printer and Sinclair software.

### Order at no risk\*\*

We'll give you 10 days to try out the ZX81. If you're not completely satisfied, just return it to Sinclair Research and we'll give you a full refund.

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\*\*Does not apply to ZX81 kits.



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# EQUIPMENT REPORTS

## Realistic PRO-2020 Programmable Scanner



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| Realistic          | PRO2020 |   |      |   |   |      |   |   |           |    |
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| EASE OF USE        |         |   |      |   |   |      |   |   |           |    |
| INSTRUCTION MANUAL |         |   |      |   |   |      |   |   |           |    |
| PRICE/VALUE        |         |   |      |   |   |      |   |   |           |    |
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|                    | Poor    |   | Fair |   |   | Good |   |   | Excellent |    |

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*continued on page 34*

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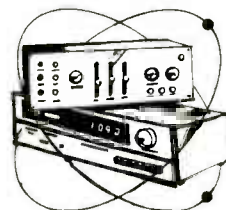
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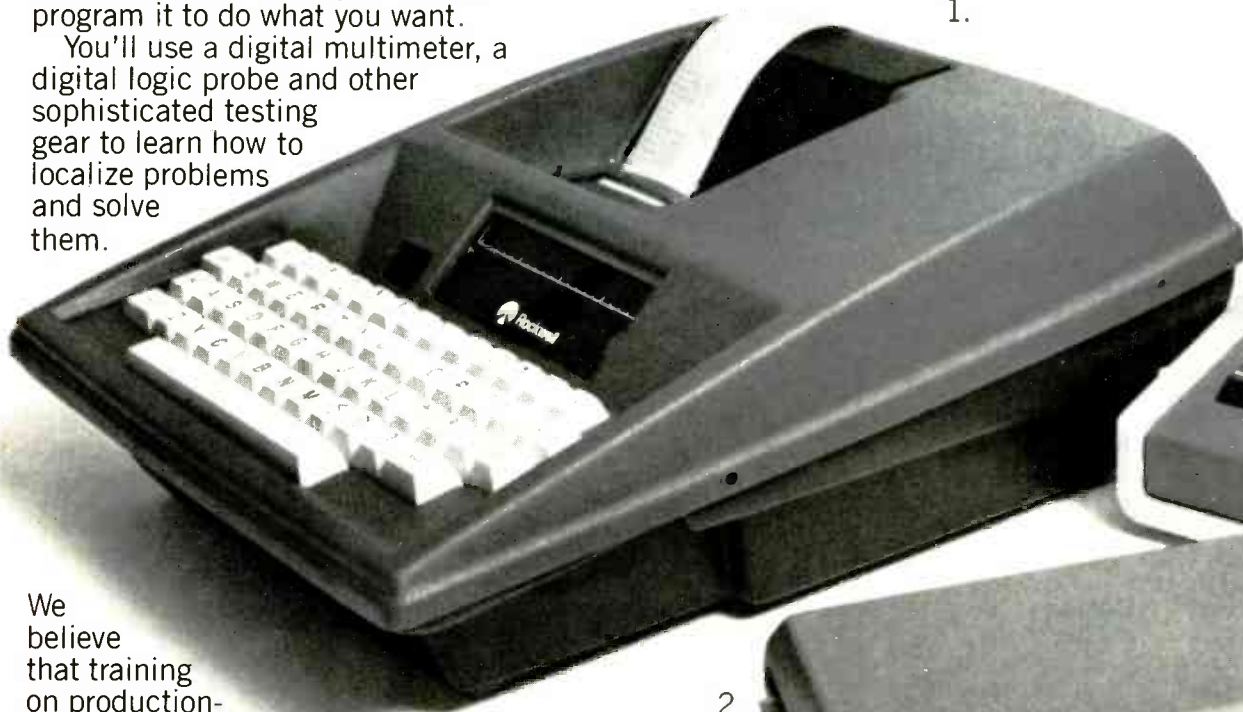
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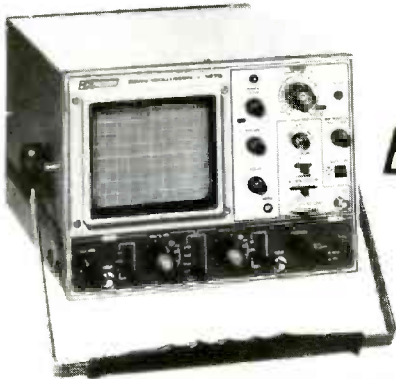
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- Variable amplitude and fixed TTL square-wave outputs
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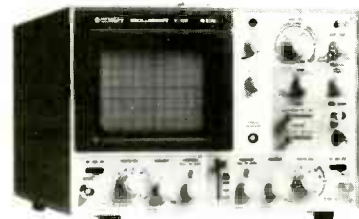
MODEL 3020

- Four instruments in one package—sweep generator, function generator, pulse generator, tone-burst generator
- Covers 0.02Hz-2MHz
- 1000:1 tuning range
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## EQUIPMENT REPORTS

continued from page 26

ing ranges available on the program-able-scanner market.

The *PRO-2020* will scan up to 20 channels and has automatic up- and down-search capability as well. Mobile or fixed-station operation is possible, and a 9-volt battery is used as a backup to hold memory in case of power failure.

The large fluorescent display indicates channel number, frequencies, scan status, search monitoring, and

other functions. A priority feature for any of the 20 channels is included. Functions, channel selections, etc. are entered using a large 24-button keypad; there is audible feedback (the scanner "beeps" at you) each time a programming key is pressed. A LOCK OUT key allows you to disable unwanted channels temporarily, and a built-in SKIP function lets the scanner jump over those unwanted channels, speeding up the scan rate.

Fast (9 channels/second) and slow (4 channels/second) search and scan speeds can be selected using the keypad. A keypad-selected DELAY function can be used if you want to keep the

scanner on a channel for two seconds after the end of a transmission; that function allows you to catch a reply transmission that you might otherwise have missed by moving immediately to the next active channel.

### Inside the cabinet

The dual-conversion (10.7 MHz and 455 kHz) superheterodyne circuitry uses an LSI microprocessor chip, an LSI phase-locked-loop system, seven CMOS IC's, eight additional IC's, 40 transistors, and 45 diodes.

Spurious-signal rejection is specified as 50 dB for VHF frequencies; spurious-signal rejection for UHF frequencies is not indicated. IF selectivity is +9 kHz at -6 dB; +15 kHz -50 dB.

The sensitivity of this model is greatly improved compared to previous Radio Shack scanners. When checked against a competitive scanner costing nearly twice as much, the apparent sensitivity was nearly identical; when we measured the sensitivity of the two units, they were within 0.1 dB of each other. The claimed sensitivity was 0.5  $\mu$ V for the low and high bands, and 1.0  $\mu$ V for the VHF aircraft-band and at UHF frequencies.

This large (10 x 11 x 3) scanner also includes a screw-on collapsible whip antenna for close-in reception. A rear-apron external-antenna jack allows the use of a rooftop antenna for improving the quality of long distance and weak-signal reception.

The instruction manual is well written and useful. It contains concise step-by-step programming information as well as an informative practical guide to scanner applications and frequency allocations.

A block diagram is also included; although it would be of little use in the maintenance of the receiver, it does give the technically-inclined user some idea of how the scanner works.

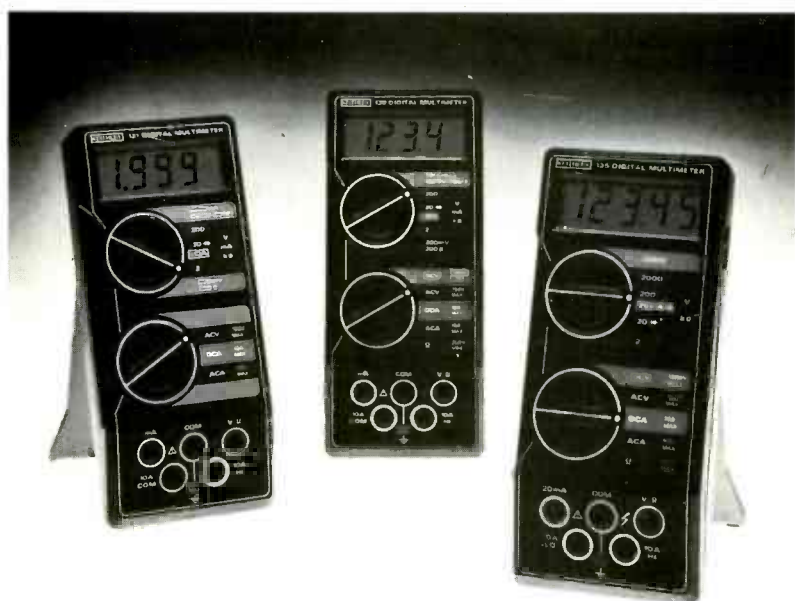
### Our test

Signal sensitivity was found to be uniformly good over all frequency-ranges. Measurements showed the *PRO-2020* to be virtually identical to the most sensitive of its competitors. While search and scan speeds are not as rapid as those of some other scanners, the receiver does have a unique feature—a sophisticated window-detector that assures the user that the scanner will stop precisely on frequency, without overshoot or undershoot.

In this age of bells and whistles, the Realistic *PRO-2020* offers high performance and straightforward design at a reasonable cost. The *PRO-2020* sells for \$299.95 and is available at Radio Shack stores.

R-E

## ADVANCE IS PROUD TO INTRODUCE the KEITHLEY Line of High Quality Digital Multimeters Featuring The New 130 Hand-Held DMM



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| MODEL | ACCURACY |       |     |      |          | SENSITIVITY |            |             |           |               |
|-------|----------|-------|-----|------|----------|-------------|------------|-------------|-----------|---------------|
|       | DCV      | DCA   | ACV | ACA  | $\Omega$ | DCV         | DCA        | ACV         | ACA       | $\Omega$      |
| 130   | 0.5%     | 1%    | 1%  | 2%   | 0.5%     | 100 $\mu$ V | 1 $\mu$ A  | 100 $\mu$ V | 1 $\mu$ A | 100m $\Omega$ |
| 131   | 0.25%    | 0.75% | 1%  | 2%   | 0.2%     | 100 $\mu$ V | 1 $\mu$ A  | 100 $\mu$ V | 1 $\mu$ A | 100m $\Omega$ |
| 135   | 0.05%    | 0.5%  | 1%  | 1.5% | 0.2%     | 100 $\mu$ V | 10 $\mu$ A | 100 $\mu$ V | 1 $\mu$ A | 100m $\Omega$ |

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Microwave Oven Tester**



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|--------------------|------------|---|---|------|---|---|---|------|---|----|-----------|
| OVERALL PRICE      | [Red bar]  |   |   |      |   |   |   |      |   |    |           |
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| INSTRUCTION MANUAL | [Red bar]  |   |   |      |   |   |   |      |   |    |           |
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|                    | Poor       |   |   | Fair |   |   |   | Good |   |    | Excellent |

FOR MANY YEARS, THE GC ELECTRONICS Co. has been making a huge variety of parts for electronics work. They've been around for longer than I can remember, at the same address, 400 S. Wyman, Rockford, IL 61101. Now, they've gone into the test-instrument field.

This one is the *Magnameter*, catalog No. 20-226. It's a specialized microwave oven tester, for analyzing the operation of the magnetron by reading secondary voltage and current. The meter has two ranges, with a toggle switch to select between the two. With the range switch in the HIGH position, the meter reads secondary voltages up to 10 kV. In the LOW position, the meter reads up to 10 volts. That range is used to measure the plate current of the magnetron, by reading the voltage drop across the plate resistor. For those ovens with no plate resistor, a heavy-duty 10-ohm tester is included, encased in plastic with alligator clips on both ends. That can be connected in the ground loop of the power-supply circuit. If the oven has a plate resistor of a value other than 10 ohms, a handy conversion chart is included for reading current.

The construction of the instrument is good: the case is high-impact plastic, and the test leads are very heavily insulated; twice the size of ordinary ones. Rubber-booted alligator clips are used

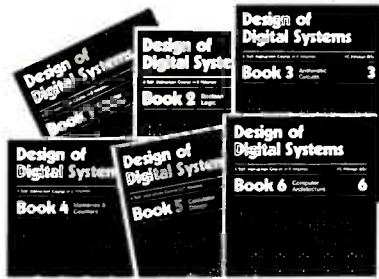
on all three leads—ground, low, and high. After the tests are completed, a DISCHARGE switch on the side of the case can be depressed to short out any remaining charge left in the circuit. A neon lamp labelled HIGH VOLTAGE, and located on the front panel, glows whenever high voltages are present in the circuit—even if the oven is off.

The *Magnameter* is a compact instrument, and it comes with a tilt handle that can be used as a bail or stand. Test-leads are permanently connected, and all connections are made with the microwave oven's power switch turned off. The test leads are long enough to let you set the meter on top of the micro-

wave-oven chassis.

The two major faults associated with microwave ovens are shorted magnetrons and shorted power transformers. By disconnecting the plate lead to the magnetron and measuring the output voltage of the power supply, then reconnecting the plate lead and measuring the plate voltage and plate current, you can isolate those two faults very quickly, and that's the name of the game.

The *Magnameter* seems to be built to give good service for a long time. List-priced at only \$86.68, it looks like quite a lot of meter for the money; it should come in handy if you're going into that end of the electronics business. **R-E**



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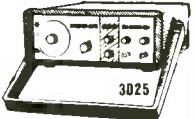
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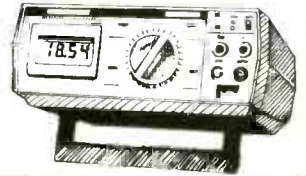
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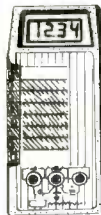
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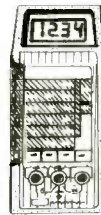
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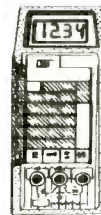
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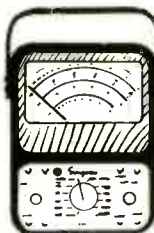
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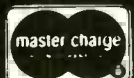
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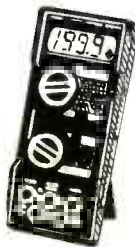
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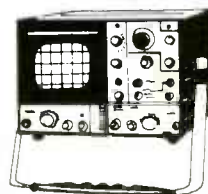
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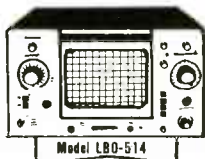
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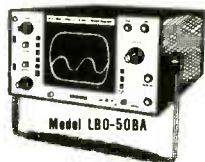
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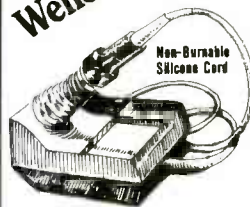
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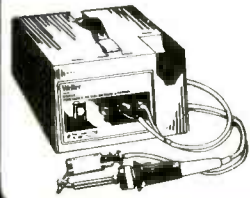


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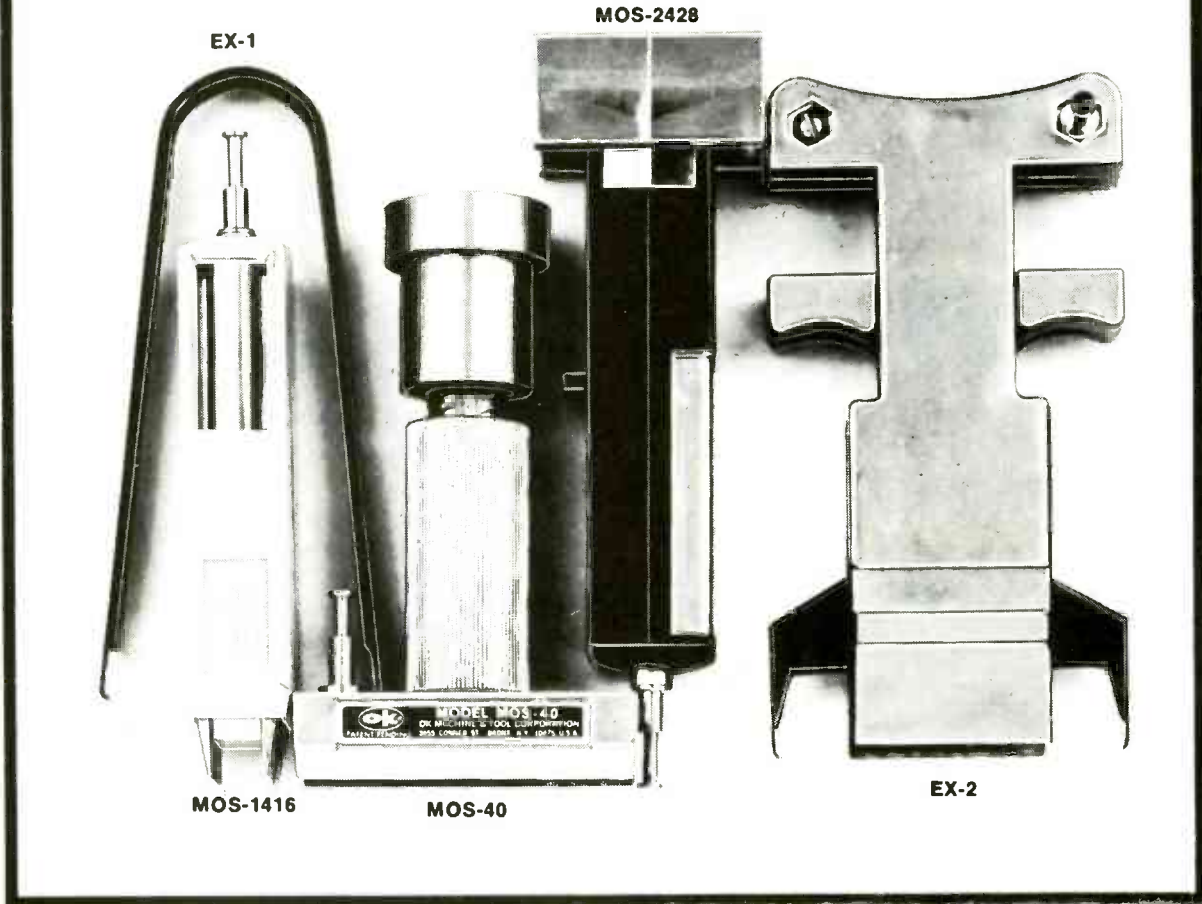


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# NEW TECHNOLOGY

## DIGITAL AUDIO DISC



*So far, digital-audio recording technology has confined itself to tape. Now, digital discs are about to make their debut.*

**LEN FELDMAN**  
CONTRIBUTING EDITOR

THE SPRING OF 1981 WILL PROBABLY GO down in history as the time when a major revolution in the science of sound recording took place. During April and May of that year, Holland's Philips Company and Japan's Sony Corporation, in jointly held presentations in Europe and the United States, announced their plans for the introduction of what has come to be known as the compact digital audio disc, or C-DAD.

If the companies meet their production target-dates, Japanese and European music lovers should be able to purchase a new kind of disc player in late 1982, while U.S. audio enthusiasts will have to wait a bit longer—until the beginning of 1983. From all indications, the long wait will be worthwhile, for the new digital C-DAD disc (sometimes acronyms become part of the language long before the item they represent is available) offers a level of performance that has been impossible to obtain with conventional analog records, no matter how carefully they were recorded and processed.

### C-DAD format

The new Philips-Sony C-DAD disc is shown alongside a conventional LP record in Fig. 1. It is capable of playing one hour of stereophonic music *per side*, and can also hold up to four channels of audio on a side with reduced playing time.

Information on the C-DAD disc consists of approximately six billion digital

"bits," which are linearly encoded along a helical track of pits and flats. The tiny pits are about 0.6 microns in width and 0.2 microns deep. The pits and flats represent the "ones" and "zeros" in the digital code used to store the signals. A solid-state laser beam is used to sense the sequence of pits and flats using a spot of light with a diameter several times smaller than that of a human hair. As shown in Fig. 2, the laser beam reads the presence or absence of the pits contained in the disc's surface beneath a protective plastic coating. The scanning rate is approximately 4.3 million bits-per-second. Variations in the reflected light rays are then converted into digital code and



FIG. 1—THE 4.7-INCH DIAMETER C-DAD disc contains one hour of music on a side compared to a little over 20 minutes for a conventional 12-inch LP.

finally, through D/A conversion, back into a continuous audio waveform.

Since there is no physical contact between the pickup and the surface of the disc, the pickup must be guided by a dynamic-tracking servo system. The lack of physical contact also means that record wear is totally eliminated.

Unlike the turntables used to play today's analog records, the rotating platter that spins the C-DAD disc has a variable rotational speed—200 rpm when the laser is at the circumference of the disc and around 500 rpm when it is 50 millimeters from the center, the inner radial limit. Scanning takes place from *inside* to *outside* and rotation is *counterclockwise*. The total storage capacity of the C-DAD disc is over 8 billion bits per side—far more than is necessary for the 60 minutes of playing time that has been standardized for the disc. That provides a great many additional possibilities for designing C-DAD players. Both the Philips and Sony prototype players that were shown last spring (see Fig. 3) were able to "read out" such additional useful information as the number of the selection being heard, its length, the sequence of numbers programmed to be heard, etc. Owners of C-DAD disc players will be able to make use of sophisticated programming circuitry, enabling them to determine which songs they want to hear and in what sequence they want to hear them.

### Audio quality and performance

The frequency response of the sys-

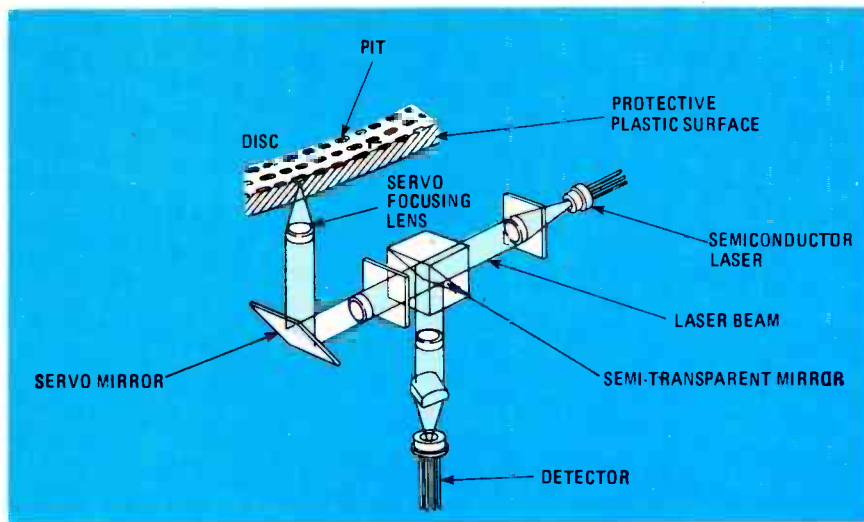


FIG. 2—THE C-DAD SYSTEM uses a tightly focused laser beam to read digital information represented by a series of pits on the disc.

TABLE 1

| Specification                  | C-DAD disc      | LP record          |
|--------------------------------|-----------------|--------------------|
| Frequency response             | 20–20,000 Hz    | 30–20,000 Hz       |
| S/N ratio                      | More than 90 dB | More than 60 dB    |
| Dynamic range                  | More than 90 dB | Max. 55 dB (1 kHz) |
| Channel separation             | More than 90 dB | 25–35 dB           |
| High-frequency distortion rate | Less than 0.05% | 0.2%               |
| Wow & flutter                  | 0%              | 0.03% (WRMS)       |
| Playing time                   | 60 Minutes      | 30 Minutes         |
| Disc diameter                  | 4.7 inches      | 12 inches          |

tem is absolutely flat from 20 Hz to 20,000 Hz. The digital sampling-frequency is 44.1 kHz, which would theoretically give a response up to 22.05 kHz. Some margin, though, is left for high-frequency cut-off filtering.

The signal-to-noise ratio for the 16-bit digitizing format is better than 90 dB (theoretically, it could be as high as 97.5 dB); dynamic range—the difference in level between softest and loudest sounds that can be handled—is also better than 90 dB. Channel separation is 90 dB as well, while total harmonic distortion, referred to peak levels, is 0.05% or less (0.03%, theoretical).

As with any true digital-sound system there is no measurable rumble or wow-and-flutter. Tracking, decoding, and rotational speeds are synchronized by a central clock generator inside the player and the clock is itself governed by information encoded in the track on the disc. Since the digital data representing the music is stored briefly in semiconductor memory in the player before being clocked out at a steady rate to the digital-to-analog converter, there can be no wow or flutter in the conventional sense.

There is also no audible intermodulation-distortion of the type that plagues conventional analog recordings to such a large degree. To fully appreciate the significance of these performance levels, see Table 1, which compares the

C-DAD system with conventional LP records.

### Competing digital-disc systems

Of the many digital-audio disc systems that have surfaced over the last several years, two besides the C-DAD system have been successfully demonstrated and been under consideration by a 51-member Digital-Audio Disc Council. That group deliberated about standardization for about three years

(and has only recently been disbanded) in Japan. The two other systems are:

1. A capacitance-pickup system, developed by JVC as an adjunct to its VHD videodisc system which is to be marketed in early 1982 and which has been given the name AHD (Audio High Density).
2. A mechanical "groove-type" system developed by Telefunken.

Discs for the variable-capacitance system (AHD) are made of conductive materials. As shown in Fig. 4, digital signals in the form of tiny pits are engraved in these discs. As a miniature metal electrode follows the pits, signals, represented by changes in electrostatic capacitance, are detected. To maintain the necessary accuracy, the pits are engraved on the surface of the disc along with pilot signals impressed on either side of the audio signal pits. Since there are no physical grooves impressed into its surface, the pilot signals are used as part of a dynamic-tracking servo system to keep the electrode stylus properly positioned along the signal track of the AHD audio disc.

In the mechanical system developed by Telefunken, playback is accomplished in a manner similar to that used by ordinary analog players (see Fig. 5). That is, signals cut into the grooves of the disc are first converted into mechanical vibrations as the stylus traces them and the vibrations are then transmitted through a pickup arm to a piezoelectric converter, where they are changed into electrical signals.

Table 2 offers a comparison of these two systems and the Sony-Philips C-DAD one. Of the three, only the Sony-Philips and the JVC systems seem likely to reach the marketplace in the near future. JVC's argument in favor of its system is based largely upon the fact that a single player would be able to



FIG. 3—C-DAD PLAYER prototypes shown in 1981. Sony's is at left; Philips' at right.



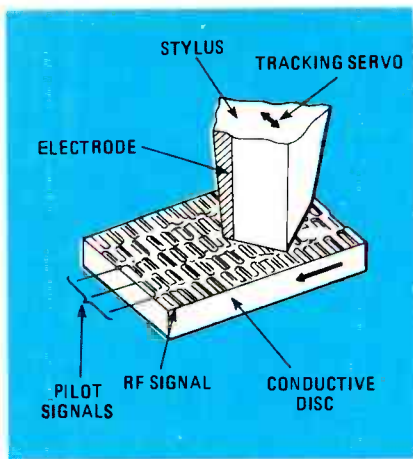


FIG. 4—JVC'S AHD digital-audio disc system works on the same principles as its VHD video-disc system.

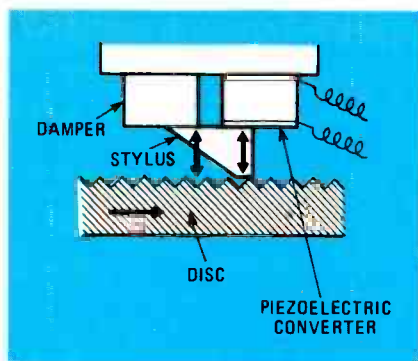


FIG. 5—THE MECHANICAL SYSTEM developed by Telefunken for digital discs is similar to that used for today's analog records.

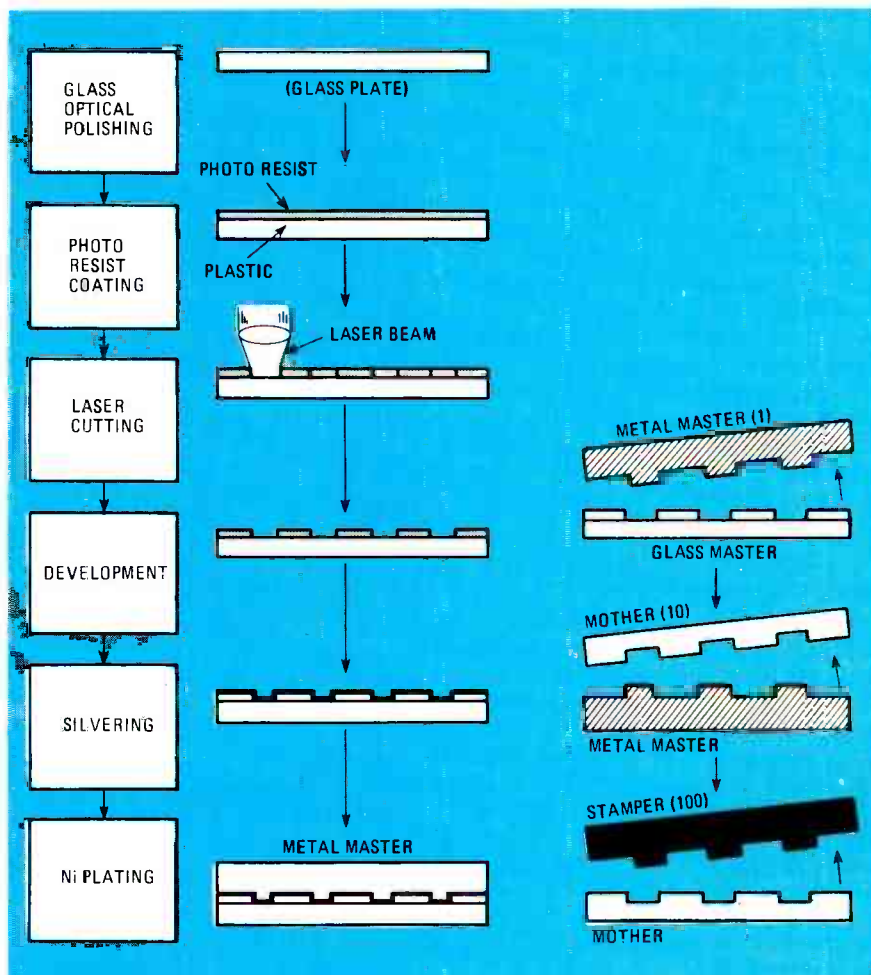


FIG. 6—STAGES INVOLVED in the manufacture of C-DAD discs. Numbers in parentheses at right indicate how many of each piece are produced.

TABLE 2

| Characteristics      | Sony-Philips            | JVC                      | Telefunken   |
|----------------------|-------------------------|--------------------------|--|
| Signal-pickup method | Optical                 | Capacitance              | Mechanical   |
| Pickup               | Non-contacting          | Contacting               | Contacting   |
| Signal location      | Beneath surface         | On surface               | On surface   |
| Grooves              | No                      | No                       | Yes  |
| Surface material     | Transparent plastic     | Carbon-impregnated vinyl | Various  |
| Disc caddy (holder)  | Not required            | Required                 | Required   |
| Disc size            | 120 mm                  | 260 mm                   | 135 mm<br>70 mm                                    |
| Playing time         | 60 minutes (2 channels) | 60 minutes (4 channels)  | 60 minutes (2 channels)<br>30 minutes (2 channels) |
| Format               | 16-bit                  | 16-bit                   | 14-bit   |

handle both its videodiscs (the VHD discs that are to be marketed in 1982) and the AHD digital-audio discs, since both use a capacitance-pickup principle. Of course, a digital-to-analog converter/processor would have to be added to the JVC system for decoding the digital-audio discs; the addition of such a D/A converter/processor would make the lower-cost argument somewhat questionable.

The JVC AHD disc, like its companion VHD disc, is a little over 10 inches in diameter and comes supplied in a "caddy" or holder that protects the

disc surface when it is not being played. The smaller, optically-tracked, C-DAD disc requires no such protective sleeve, of course, and is in no way affected by dirt or dust on its surface since the focal point of the laser beam is beneath the transparent surface of the disc. An important point that has been emphasized many times by Sony and Philips is that the small C-DAD disc and its correspondingly small player can easily be adapted for use in cars and other moving vehicles, since the vibration of a vehicle should have little or no effect upon laser tracking.

#### The trend towards C-DAD

There seems to be a growing trend towards endorsement of the C-DAD system by equipment manufacturers and "software" (recorded material) producers around the world. Matsushita Electric Company (whose line of brands includes Panasonic, Quasar, Technics and National), although committed to the JVC VHD system for videodiscs, has nevertheless indicated that it will produce disc players for the Sony-Philips system. Recently, the worldwide Polygram Group, one of the leading international record manufac-

turers, and CBS/Sony, Inc., the largest record company in Japan, announced plans to produce music programs in the C-DAD format. In 1982, for example, CBS/Sony will release more than 100 C-DAD albums in Japan simultaneously with the introduction of the C-DAD players. On the hardware side, companies such as Marantz have already demonstrated their own versions of players which are compatible with the Sony-Philips optical-laser disc system. And, while the 51-member Digital Audio Council mentioned earlier did not specifically endorse the C-DAD system, its final report noted its compact size and its applicability to mobile use, which many interpreted as being just about as close to an endorsement as such a committee would ever be likely to come.

### How C-DAD discs are made

Once you get past the hurdle of paying for a C-DAD optical-laser player (about the price of a high-end turntable), the software or discs themselves should be no more expensive, on a "per-minute-of-music" basis, than high-quality LP records. The process of making digital discs is quite different from the process currently used to make analog LP records, but once it has been mastered, it should be possible to turn out the new discs on a mass-production basis that will reduce disc prices drastically.

Mechanical cutting-techniques are impractical for digital-disc production because the pits to be carved are far too small. Instead, the process shown in Fig. 6 is used. First, a glass plate coated with photo-resist material is exposed to a digitally-modulated laser beam. The plate is then developed to form pits corresponding to the presence or absence of digital signals. After a silvering process, that glass plate becomes the "master."

It is next pressed against a nickel plate to make an inverse copy (the pits become small bumps and the flats become depressions) of the photo-etched depressions on that plate. A digital master is thus produced which, in turn, is used as the "mother" for making production "stamper." Each stage inverts the surface of the disc (pits-bumps-pits-bumps, etc.). The stamper has bumps.

The final production stages are shown in Fig. 7. Using the stamper, C-DAD discs are produced in large quantities in much the same manner as conventional analog records. The signal-bearing surface of each disc is then coated with a reflective material, followed by a coating of protective, transparent plastic. Aside from any labelling and packaging that may be required, that completes the manufacture of a single-sided disc.

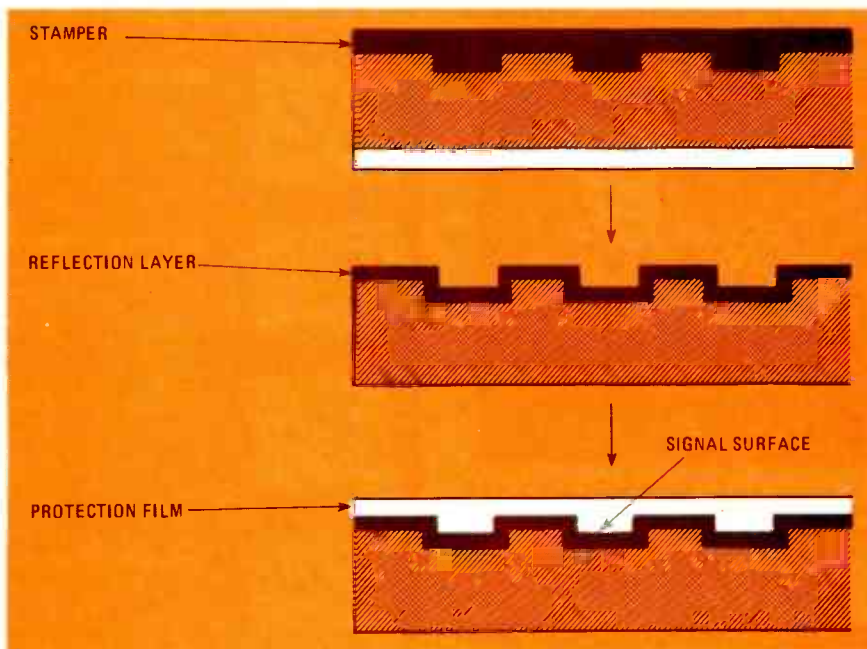


FIG. 7—FINAL STAGE in C-DAD disc production involves adding a reflective layer to the surface and protecting it with a clear plastic coating.

## “DIGITAL” vs. DIGITAL

FOR THE PAST SEVERAL YEARS 12-INCH “DIGITAL” discs have been available from companies such as Telarc, Teldec, London, and others.

It is a common misconception that those are *true* digital discs, but that is not the case.

*True* digital discs carry the audio information as a series of binary-coded numbers—that is the method used by the C-DAD.

*Digitally-mastered* discs—the 12-inchers currently on the market—are so called because the *master tapes* from which they are produced are digitally-encoded. The discs themselves carry a conventional analog signal.

Those discs do have an advantage over ones recorded using analog processes all the way through—the quality of the master tapes is higher and some of that quality is carried over into the analog pressing. Dynamic range is greater, tape hiss is non-existent, etc. The discs themselves, though, are still prone to the shortcomings of analog recordings—surface noise, restricted dynamic range, tracking problems, and so forth.

While “digital” (digitally-mastered) discs certainly represent a tremendous improvement over their all-analog predecessors, their quality is still far removed from that obtainable from all-digital recordings.

R-E

For a two-sided disc, an additional process to combine two single-sided discs would be required, but it is entirely possible to produce such two-sided discs.

### Digital source-material

Recognizing the advantages of digital recording almost as soon as it was made available on a commercial basis to recording studios several years ago, many recording companies around the world have been producing digital master-tapes for release as digitally-mastered, improved *analog* LP's (often erroneously referred to as “digital” records). Although many of those recordings have been praised as being clearly superior in sound quality to conventional LP's, they obviously cannot approach the performance levels that will be reached by C-DAD discs once they are made available. (See sidebar for more information.)

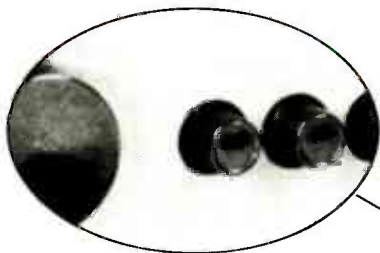
The fact that so many digital master tapes now exist in the archives of major recording studios bodes well for the future of true digital-discs. All those tapes can be used to make true digital-audio discs, with no degradation in quality from master tape to disc. The Sony-Philips system, in fact, uses the same 16-bit PCM (Pulse Code Modulation) encoding currently being used for professional digital-audio purposes. Therefore, C-DAD recordings can be made in studios using existing PCM equipment. It is also possible to translate existing analog recordings, using PCM processors, to the C-DAD format. However, should that be done, the resulting product would not exhibit the increased dynamic range and other improvements made possible by digital-recording technology.

R-E



# TELEVISION

## WHAT EVER HAPPENED TO CHANNEL 1?



Ever wonder why your VHF-television dial starts with Channel 2? Find out why in this brief look at the early days of television and how it all began.



DAVID A. FERRE

WHEN A TELEVISION RECEIVER IS PURCHASED in the United States, you can take it anywhere in the country, plug it in, pull up the "rabbit ears," and tune in a station. That is possible because we have national broadcasting standards that are common throughout the country. Yet, at one time commercial television was going to be introduced to the American public without standards; fortunately, that "experiment" ended before it even started. But let's not get ahead of our story!

### Up to 1934

During the first few months of 1933, RCA demonstrated the first successful all-electronic television system. Broadcasts were made from the RCA experi-

mental television transmitter, W2XBS, located at the top of the Empire State Building in New York City. The characteristics of that early all-electronic television system were modest:

- Lines: 240
- Frames: 24 per second
- Scanning: sequential (no interlacing)
- Bandwidth: 2 MHz
- Video carrier: AM modulated, full sideband
- Audio carrier: AM modulated, full sideband

Yet, the results were far better than any mechanical television system had ever accomplished. For those experiments, the video carrier was at approximately 45 MHz.

It may be hard for us to appreciate

fully what RCA had accomplished in 1933. But to give you an idea: Many of the experimental television broadcasters were still using frequencies in the 2- to 3-MHz range, and bandwidths of 100 kHz. In addition, the earlier systems were mechanical using gears, motors, mirrors, etc. As television advanced, each step pointed towards non-mechanical systems, and higher bandwidths and carrier frequencies.

The Federal Communications Commission was established by an act of Congress on June 22, 1934. It was about that time that a portion of the VHF radio spectrum was allocated to television for the first time (see Fig. 1). Previously, any frequency above 30 MHz was available to experimenters. Those experimenters included a number of pioneering amateur-radio operators; there were also experimental stations that included television. In 1934, the experimenters were moved to the frequencies above 110 MHz, while television was allocated two bands, 42-56 and 60-86 MHz. There were no channels associated with the allocations, but it was a beginning; television was making its first move.

### 1934 to 1938

Progress was slow for television during those years. The depression was at its worst, and even mighty RCA lost

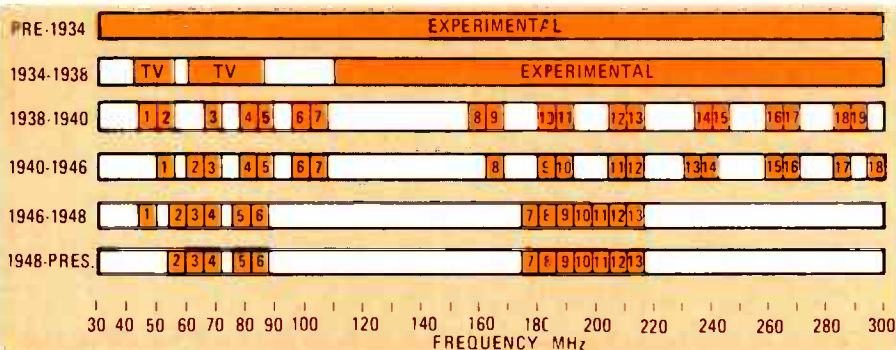


FIG. 1—HOW THE TELEVISION ALLOCATIONS have changed over the years. This chart shows the approximate frequencies of the channels; the exact frequencies are given in Table 1.

money. But advances were made in RCA's all-electronic system. In June, 1936, RCA announced the start of a massive field test. A total of 100 experimental-television receivers were distributed to RCA employees for placement in their homes and offices (see Fig. 2). RCA then began regular television broadcasts from W2XBS, using their new Radio City television studios. Those studios were linked to the Empire State Building transmitter by an experimental 177-MHz radio link and a coaxial cable. The composition of the television signal used for that test was as follows:

- Lines: 343
- Frames: 30 per second
- Scanning: interlaced (2:1)
- Bandwidth: 5.75 MHz
- Video carrier: AM modulated, full sideband
- Audio carrier: AM modulated, full sideband

On June 15, 1936, the FCC began informal hearings concerning the radio spectrum above 30 MHz. There was an increasing demand for those frequencies and a new word began to be heard at the FCC; that word was standards. The Radio Manufacturers Association (RMA), the trade association for the radio and television equipment manufacturers, had formed a sub-committee on television. They attended the June, 1936 hearings because of their interest in the possible future commercialization of television. In addition to urging definite channel allocations, the RMA had a set of television channel standards to present (see Fig. 3-a). Although those standards were incomplete in some respects, one important recommendation that the RMA made to the Commission was that the bandwidth of a television channel should be 6 MHz—the same bandwidth that is used today. The RMA television standards were:

- Lines: 441
- Frames: 30 per second
- Scanning: interlaced (2:1)
- Bandwidth: 6 MHz
- Video carrier: AM modulated, full sideband
- Audio carrier: AM modulated, full sideband

It is interesting to note that the proposed 441-line standard was beyond the capabilities of any system that had been demonstrated up to that point. It wasn't until eight months later, on February 11, 1937, that a manufacturer (Philco) gave a convincing demonstration of a television system that completely met the RMA standards.

The FCC hearings that had started on June 15, 1936, resulted in the allocation of 19 television channels, each with a bandwidth of 6 MHz. The new allocations, which are shown in Fig. 1 and Table 1, became effective October 13, 1938. The RMA revised and completed their set of television standards, which were essentially the same as the 1936



FIG. 2—ONE OF THE LAST in existence, this receiver was one of the ones used in RCA's test of the first all-electronic television system. The vertically-mounted picture tube was viewed through a mirror in the cabinet top.

standards except for one important difference: The video carrier would now be transmitted with a full upper sideband and only a partial lower sideband, as shown in Fig. 3-b. That vestigial sideband system was eventually adopted by the FCC and is used today.

Television now had allocations and channel numbers. Our mysterious Channel 1 was assigned to the 44- to 50-MHz band as shown in Table 1. RCA's experimental station quickly received a permit for one of those new television allocations and selected Channel 1!

### 1938 to 1940

The television industry was generally pleased with the FCC allocation of 19 TV channels. They were hoping for a continuous band of frequencies to simplify tuner design, and were somewhat disappointed that 12 of the 19 channels were above 150 MHz; those frequencies were virtually unused, and thought to be useful only for television-relay networks. But the seven channels between 44 and 108 MHz were enough to begin plans for commercial television operation. By then it was believed that the RMA standards would be adopted by the FCC and commercialization could begin. But not everybody agreed with the RMA standards, and the FCC wasn't about to approve any standard unless the television industry was in almost total agreement.

On October 20, 1938, just one week

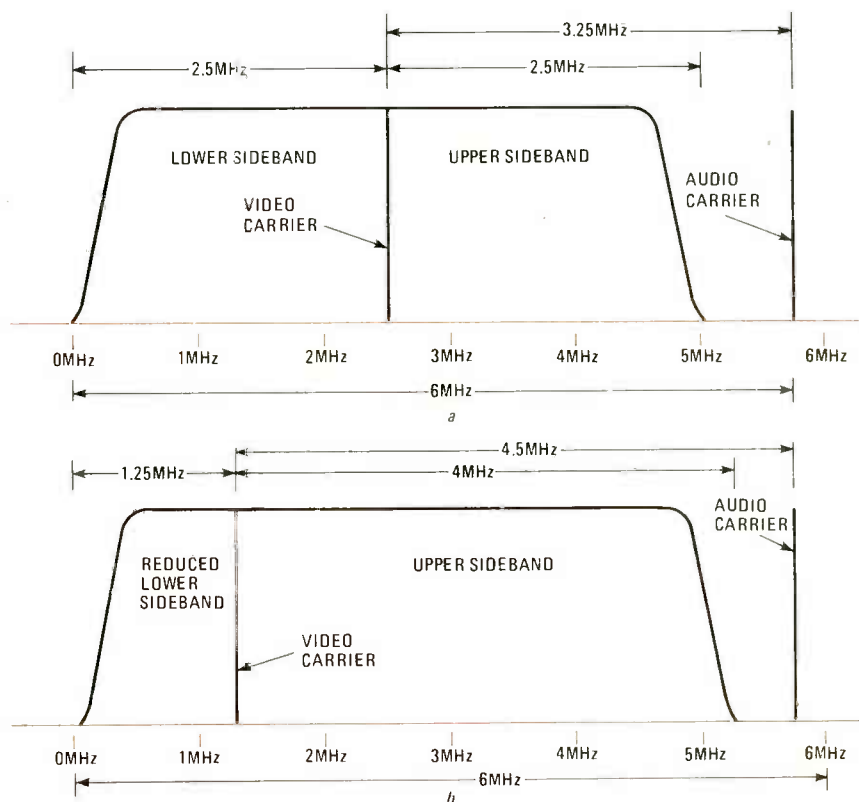


FIG. 3—THE FIRST STANDARDIZATION of a television signal, the system shown in a featured full upper and lower sidebands. A later revision, shown in b, featured a reduced lower sideband. That vestigial sideband technique is the one is use today.



TABLE 1

| Channel | Year      |           |           |              |
|---------|-----------|-----------|-----------|--------------|
|         | 1938-1940 | 1940-1946 | 1946-1948 | 1948-PRESENT |
| 1       | 44-50     | 50-56     | 44-50     | —            |
| 2       | 50-56     | 60-66     | 54-60     | 54-60        |
| 3       | 66-72     | 66-72     | 60-66     | 60-66        |
| 4       | 78-84     | 78-84     | 66-72     | 66-72        |
| 5       | 84-90     | 84-90     | 76-82     | 76-82        |
| 6       | 96-102    | 96-102    | 82-88     | 82-88        |
| 7       | 102-108   | 102-108   | 174-180   | 174-180      |
| 8       | 156-162   | 162-168   | 180-186   | 180-186      |
| 9       | 162-168   | 180-186   | 186-192   | 186-192      |
| 10      | 180-186   | 186-192   | 192-198   | 192-198      |
| 11      | 186-192   | 204-210   | 198-204   | 198-204      |
| 12      | 204-210   | 210-216   | 204-210   | 204-210      |
| 13      | 210-216   | 230-236   | 210-216   | 210-216      |
| 14      | 234-240   | 236-242   | —         | —            |
| 15      | 240-246   | 258-264   | —         | —            |
| 16      | 258-264   | 264-270   | —         | —            |
| 17      | 264-270   | 282-288   | —         | —            |
| 18      | 282-288   | 288-294   | —         | —            |
| 19      | 288-294   | —         | —         | —            |

after the allocations became effective, RCA announced that regular television programming would begin as a "public service" on April 30, 1939. That date coincided with the opening of the 1939 New York World's Fair. A number of manufacturers began producing television receivers, and by the opening of the fair they were in the stores and ready for sale. The opening ceremonies of the fair were broadcast on Channel 1 by RCA's W2XBS, and featured the President of the United States. After that event, broadcasts were scheduled on a regular basis.

By the end of May 1939, large department stores, such as Macy's in New York, offered as many as nine different models for sale; those were supplied by three manufacturers (Andrea, DuMont, and RCA). Screen sizes for those television sets ranged from 5 to 14 inches, and prices ranged from \$189.50 to \$600.00. Most of the early sets were complete receivers, but one, the *model TT-5* from RCA (shown in Fig. 4), had no audio section; if audio was desired, it had to be connected to a compatible RCA receiver. Unfortunately, sales of those early television sets were not very good, and by the end of 1939 fewer than 400 of them had been sold in the New York area.

All of the major television broadcasters (incidentally, the stations were still considered experimental) had adopted the RMA standards by the end of 1939. That included the stations in New York City, Chicago, Los Angeles, and Schenectady. The FCC was urged to adopt the RMA standards so that commercialization could begin. The FCC responded to the pressure from the TV industry by publishing rules for limited commercialization on December 22, 1939. It was a kind of Christmas present for the television industry.

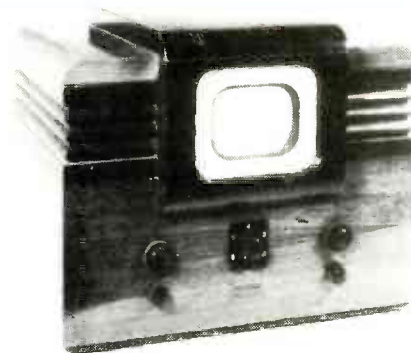


FIG. 4—THIS EARLY TELEVISION SET, the RCA *model TT-5*, was one of the first offered for sale to the general public. It featured a five-inch screen, five-channel coverage, but no audio section; it sold for \$199.50 in 1939.

At the time those rules were published, the FCC also announced that hearings would be held in January, before establishing a date for limited commercialization. At those hearings, it was made clear to the FCC that many of the broadcasters did not agree that the RMA standards were the best. Philco urged the FCC to adopt their system of television with 605 lines and 24 frames-per-second. DuMont wanted standards that included 625 lines and 15 frames-per-second. In addition, there was some vague talk about something called color television. Nevertheless, in an order issued on February 29, 1940, the FCC ruled that limited commercialization could begin on September 1, but warned that nothing should be done to encourage a large public investment in television receivers. They refused to adopt any standards, with the implication that each of the broadcasters could use whatever standards they liked best, with the public deciding who had the best system.

RCA responded to the authorization for limited commercialization with full-

page newspaper ads in early March announcing the "arrival of television," and ordered the immediate production of 25,000 television receivers. The FCC realized that limited commercialization wasn't going to work, as the sale of thousands of television sets would, in effect, "freeze" the standards, making a change to other standards almost impossible. Within a few days of the RCA newspaper ads, the FCC's permission for limited commercialization was withdrawn.

Television was also about to undergo some more changes. Frequency Modulation (FM) had been introduced by its developer, Major Edwin H. Armstrong, in 1935. Shortly after its introduction, FM was granted five experimental frequencies between 42.6 and 43.4 MHz. By 1940, the FCC had 150 applications for experimental FM stations on file that could not be processed because of lack of frequencies. As a result of hearings held on March 18, 1940, the FCC assigned FM a continuous band of frequencies (that was done to simplify tuner design), and expanded the FM allocation to include the frequencies from 42 to 50 MHz. The new allocation included the 44- to 50-MHz band that had previously been assigned to Channel 1.

But that is not what happened to Channel 1! The TV channels were renumbered with Channel 1 now assigned to 50-56 MHz band and the remaining channels were shifted around the spectrum. But when the smoke cleared, the television industry had lost one channel, leaving them with 18 allocations.

The new FM channels and the changes in the television allocations became effective on June 20, 1940; commercial FM broadcasting was authorized to begin on January 1, 1941.

#### 1940 to 1946

When the revised 18-channel TV allocations went into effect, the television industry was unhappy, to say the least. The limited commercialization plan was suspended; the FCC continued its refusal to set television standards; a television channel was lost to FM, and, because of the changes in the allocations, many of the experimental TV broadcasters had to go off the air to complete extensive transmitter changes. For example, the RCA experimental transmitter, W2XBS, had been operating on the old Channel 1 (44-50 MHz); because of the changes, they were forced to switch to the new Channel 1 (50-60 MHz).

However, soon after that things began to look up. A member of the RMA had met with the FCC to ask just what the television industry could do to win approval of a set of standards. The FCC replied that if the industry could agree on *one* set of standards, they would be

approved without delay. Quickly, the RMA organized the National Television Standards Committee (NTSC). The NTSC was open to all major interests in the television field whether they were associated with the RMA or not. Eventually, over 160 individuals became associated with the NTSC. On July 31, 1940, under the RMA's sponsorship and with the FCC's blessing, the NTSC held its first meeting.

With the opportunity to propose a set of standards to the FCC, you might have expected that the NTSC would simply have endorsed the existing RMA standards, but that is not what happened. Every aspect of the television-standards question was re-examined and discussed at length. On January 27, 1941, the NTSC met with the FCC and presented a progress report. The preliminary NTSC standard presented to the FCC at that meeting closely paralleled the RMA standards. That seemed to indicate that the RMA standards were essentially correct. There was one important difference, however: The audio carrier was to be FM. The FCC had one reservation about the proposed standard—they felt that the 441-line standard recommended by the NTSC was too low. That standard went way back to the first RMA standards of 1936, when both video sidebands were transmitted. It was common knowledge that the vestigial sideband system in use since 1938 allowed a much higher line count and, accordingly, a better television picture. The NTSC agreed to re-examine that question and said that it would present more information at hearings that were to be held in March, 1941.

Those hearings were held on March 20, 1941. The NTSC standard that was presented at the hearing was almost identical to the one proposed earlier, except that the number of lines was increased to 525 lines. (Although the number of lines seemed to be random, it was not. The line count had to be an odd number and to be related to few multiples of odd numbers, such as  $3 \times 3 \times 7 \times 7 = 441$  or  $3 \times 5 \times 5 \times 7 = 525$ , for example. That was necessary for generation of the synchronizing pulse.) The new standard was as follows:

|                |   |
|----------------|---|
| Lines:         | 525   |
| Frames:        | 30-per-second   |
| Scanning:      | interlaced (2:1)  |
| Bandwidth:     | 6 MHz   |
| Video carrier: | AM modulated, vestigial sideband                                    |
| Audio carrier: | FM modulated, $\pm 75$ kHz deviation (later $\pm 25$ kHz deviation) |

Virtually all of the participants in the hearings (they went on for four days) agreed that the NTSC Standards were correct and should be adopted quickly. The FCC was convinced that the indus-

try had finally agreed and the NTSC Standards were adopted as the national standard in April 1941. The effective date was July 1, 1941; commercial television could finally begin!

When that "Opening Day" for commercial television finally arrived, only two television stations were licensed and ready for operation; WNBT (NBC, old W2XBS) transmitting on Channel 1, and WCBW (CBS, old W2XAX) transmitting on Channel 2. Both of those stations were in New York City. Soon after (on September 1, 1941) WPTZ in Philadelphia, transmitting on Channel 3, came on the air. By the spring of 1942, a total of four commercial stations were in full operation and 10,000 television receivers had been sold.

Television's growth was halted by World War II, with the Defense Communications Board ordering the construction of new radio and television stations to end. Television programming was reduced to just four hours per week for the broadcasters already in operation (all devoted to war-related activities).

As the end of the war approached, the FCC was faced with a monumental task. The war effort had brought about an extraordinary leap in communications technology. Frequencies that had been thought to be useless were now in tremendous demand. The entire spectrum had to be re-examined, with new allocations made and old ones revised. The FCC began by holding hearings on September 28, 1944. They were promptly overwhelmed. The 18-channel television allocations in effect since 1940 were attacked by one group as being wasteful of the valuable VHF spectrum, yet another group urged an increase to 26 channels. Others urged the FCC to move all of the television allocations to UHF frequencies immediately. But the television industry argued that television had waited long enough and should develop now, using the existing allocations.

After hearings that were held on February 14, 1945, it became clear that no group was going to get everything it wanted. In the FCC's final decision, released on June 27, 1945, television's allocation was reduced to 13 channels, and FM was moved from the 42-50 MHz slot to 88-106 MHz (the band was later increased to 88-108 MHz). The television interests were very unhappy that they were left with only 13 channels, but the FM interests suffered a major blow because all of the existing stations had to go off the air and switch to new frequencies. In addition, 500,000 home-FM receivers were now obsolete.

The reduction to 13 television channels was accompanied by new and re-organized frequency allocations (see Table 1). Again the broadcasters had to go off the air to switch frequencies.

Our Channel 1 was still around, but it was moved back to the 44- to 50-MHz band that it had occupied from 1938 to 1940. In addition, there was a restriction for Channel 1: It could only be assigned as a community channel, and was limited to a maximum power of 1000 watts. Other TV channels were for metropolitan stations, with a maximum power of 50,000 watts permitted. All channels, except Channel 6, were shared with fixed and mobile services—a fact that left the television interests concerned about interference. The changes became effective March 1, 1946.

### 1946 to 1948

Even with the reduced number of channels, the boom was on! Manufacturers quickly began producing television receivers, transmitters, antennas, etc. New television stations were being built all over the United States. The FCC had identified the top 140 metropolitan cities and assigned each at least one channel; a total of 400 were to be allotted. The FCC received many more applications than it had available channels. In an effort to provide the public with as many channels as possible, the FCC routinely threw away the "safety factor" of mileage between licensed transmitters. Television-receiver sales were doing very well, with 175,000 sold by the end of 1947. Manufacturers were selling television sets as fast as they could be made, even though the sets were rather expensive. (A typical set with a 10-inch screen sold for \$375.)

But problems began to appear. Propagation theories at that time predicted that television signals would not be received over the horizon—but they were, quite readily. So, even with just 50 stations on the air, interference problems were beginning to appear. Meanwhile, the FCC had reduced the minimum distance between stations using the same channel to just 80 miles. An engineering study released by the FCC warned of interference problems if immediate action wasn't taken. That led to an FCC report, issued on May 5, 1948, that ruled that television could no longer share its frequencies with fixed and mobile services, and that the 72- to 76-MHz band could be used for fixed radio services only.

But where could the mobile services be located if they could no longer share the television allocations, and could no longer use the 72- to 76-MHz band? There was only one place to go—the television industry would have to give up another TV channel. But which channel would that be? The American Radio Relay League (an association of amateur radio operators) urged that Channel 2 be deleted so that the second harmonics of the 28-29.7-MHz amateur-radio band would not interfere with

*continued on page 89*



TRAFFIC BROADCAST ZONES  
IN WEST GERMANY (ARI)

## NEW USE FOR FM SCA AUTOMATIC ROAD INFORMATION SYSTEM

*Most people think of SCA as a means of piping mood music into stores and restaurants. West Germany has found a much more valuable way to use that service.*

LEN FELDMAN  
CONTRIBUTING HI-FI/VIDEO EDITOR

A FEW YEARS AFTER MAJOR ARMSTRONG FIRST DEMONSTRATED a workable system of wideband-FM radio broadcasting back in the 1930's, he demonstrated how a subcarrier could be used to modulate the main carrier of an FM station, and how that subcarrier could carry information that was totally different from what was being transmitted on the main carrier.

Many years later, in 1961, the basic techniques developed by Armstrong and modified by others resulted in the beginning of stereophonic broadcasting in the U.S., using subcarrier techniques which, though somewhat different from those first proposed by Armstrong, nevertheless fall into the general category for multiplexed FM.

### SCA

In 1954—several years before stereo broadcasting began—the Federal Communications Commission, concerned over

the increasing economic plight of struggling FM stations, authorized what came to be known as SCA transmissions. (SCA stands for Subsidiary Communications Authorization.) In those pre-stereo days, FM stations were permitted to transmit one or more subcarriers at frequencies between 25 kHz and 75 kHz above the main carrier, and to modulate those subcarriers with virtually any sort of useful information for use on a point-to-point basis. In other words, the station could lease its subcarriers to companies. The companies leasing the subcarriers could then charge a rental fee for receivers provided to subscribers who wanted to hear whatever was being transmitted on the subcarriers.

The best known use of those subscriber-oriented services is for commercial-free background music. Such music, brought to us by such familiar names as Muzak, has been the butt of jokes and disparaging remarks almost from the day that SCA service began. Less familiar is the fact that SCA transmissions do not always consist of background music. In many parts of the country, SCA channels are used to provide a "talking book" service for the blind. And, with the shortage of regular radio-channel space becoming acute, some enterprising broadcasters are turning to SCA to provide foreign-language or ethnic programming for audiences whose numbers are too small to justify the assignment of a station-frequency by the FCC.

With the advent of FM stereo in 1961, the space available for SCA channels was sharply reduced. Figure 1 shows the modulation spectrum of an FM-stereo transmitter. All of the frequencies given in the following discussion are referenced to the main-carrier frequency. The sum (L+R) of the two audio channels occupies spectrum space from 30 Hz to 15 kHz (the highest audio frequency permitted on FM), the stereo pilot-signal is found at 19 kHz, and the sidebands of the suppressed-carrier 38-kHz AM subcarrier signal containing the difference (L-R stereo information) occupy the space from 23 kHz to 53 kHz. That leaves only the spectrum space from 53 kHz to 75 kHz for SCA or private subcarrier use. Some guard-band space must be provided for, so the first practical subcarrier will have a frequency of around 57 kHz. Stations transmitting in stereo and also providing an

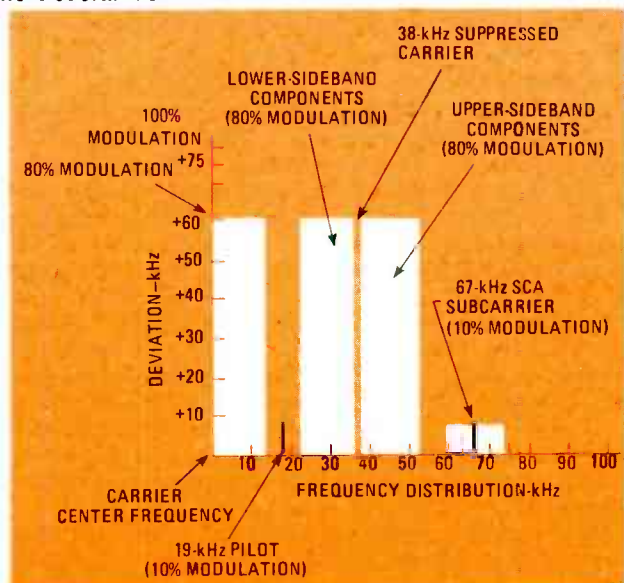


FIG. 1—AN FM-STEREO STATION that offers an SCA service does so at a frequency 67 kHz above the center frequency of its carrier.

SCA service generally select 67 kHz as their subcarrier frequency.

### Auto road information

We recently learned about a new use for SCA, which is currently in service in West Germany. The new service is helping to solve road problems in that country. As most drivers know, there are AM and FM radio stations in almost every part of this country that broadcast traffic information as part of their regular programming. The same is true in West Germany and in other European countries. But the high density of traffic in Europe has caused problems that did not exist even a few years ago.

The traffic problems, of course, are worst during rush hours, weekend peaks, vacation periods, etc. When the capacity of a road is exceeded, traffic jams occur, leading to road accidents—rear-end collisions and the like. The authorities in West Germany reasoned that information supplied promptly to drivers would help keep traffic problems to a minimum. Indeed, way back in the 1960's the government-controlled Radio Broadcast Network began giving traffic information at the end of hourly news broadcasts. It was quickly realized, however, that even such an expanded information service would be of little use unless the information were of a local nature (so that drivers in the immediate area of a problem were informed of it), and unless drivers could be readily alerted to the problem.

As early as 1969, West Germany's well known Blaupunkt radio company began working on the problem and came up with a system that made it possible to distinguish a station that broadcast traffic news and information from the many other stations on the FM broadcast band. Some time later, that system was elaborated upon and became known as ARI (Automatic Road Information). After extensive testing, the system was adopted in West Germany in 1974, and is in use today. Since then, the system has been submitted to the European Broadcasting Union (EBU) for adoption as a standard and, after practical tests in Switzerland, has been recommended to all European countries for the dissemination of traffic information. Austria introduced the system in 1976, and trials in other European countries have also been taking place to assess ARI's merits.

### The ARI system

The ARI system is used to identify stations that broadcast information about traffic conditions, as opposed to those that do not. That is especially useful to a driver who comes from another geographical area and is not familiar with local stations. Using a specially designed, ARI-equipped, radio, the driver can "tune out" stations that do not broadcast traffic information, leaving only the traffic-information stations audible.

One option in an ARI-equipped car radio automatically increases the volume to a predetermined level at the start of any traffic announcement, and returns it to its previous level at the conclusion of the announcement. Another option available in ARI-equipped radios provides a visual indication (similar to the familiar stereo-indicator light) when the driver tunes to a "traffic information" station. It is also possible to have traffic announcements override a cassette-tape program that the driver may be listening to while driving, with automatic return to the cassette when the announcement has been completed.

Still another version of the ARI-equipped radio provides an advance warning that a traffic announcement is about to be made, using a brief "signature tune" to avoid startling a driver whose radio had been muted before the announcement. A suitably equipped ARI car radio can even warn a driver when a station's signal strength falls below usable levels as he leaves the station's area of coverage. That is useful as it will allow him to tune to another ARI-equipped station in his new region of travel.

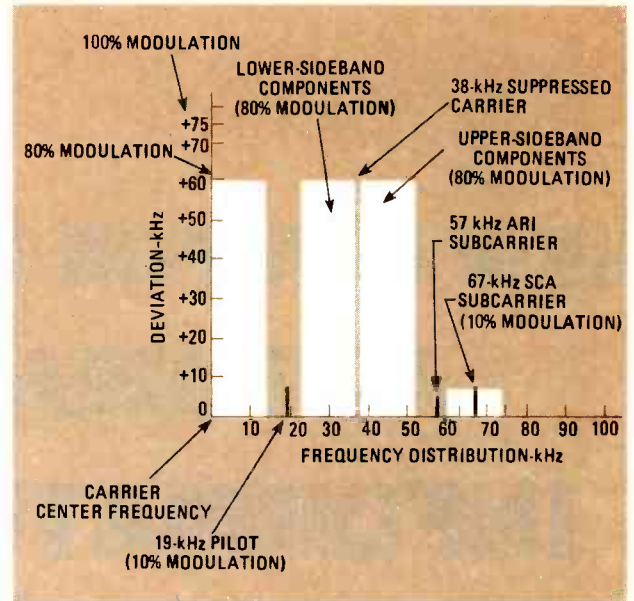


FIG. 2—THE ARI SYSTEM adds a 57-kHz subcarrier to indicate the presence of an ARI station.

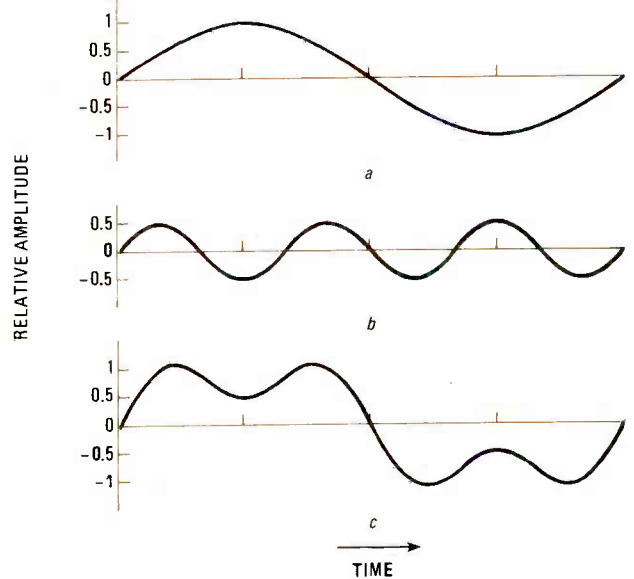


FIG. 3—THE PEAK AMPLITUDE of the 19-kHz stereo pilot-signal plus the 57-kHz ARI subcarrier does not exceed that of the pilot signal alone.

### How ARI works

An important characteristic of the ARI system is its ability to identify the station or stations in a given area that provide traffic information on a regular basis. Ordinarily, a driver would find it difficult and time consuming to single out a traffic-news station from all the others on the FM band in most metropolitan regions. With the ARI system, those stations that broadcast traffic information and are part of the ARI network transmit a continuous 57-kHz sub-carrier signal, known as the Station Identification signal (or "SK," from the German word "Senderkennung"). That signal, nestled between a normally used 67-kHz SCA subcarrier, and the upper frequency of 53 kHz that is present during FM-stereo broadcasts, is derived by tripling the 19-kHz pilot signal associated with stereo transmissions. The 57-kHz signal is therefore locked to the stereo pilot-signal both in phase and frequency relationship.

The complete modulation spectrum of an FM transmitter operating in both stereo and ARI is shown in Fig. 2. Figure 3 illustrates an important aspect of the ARI system. The 57-kHz subcarrier modulates the main carrier at half the level that the



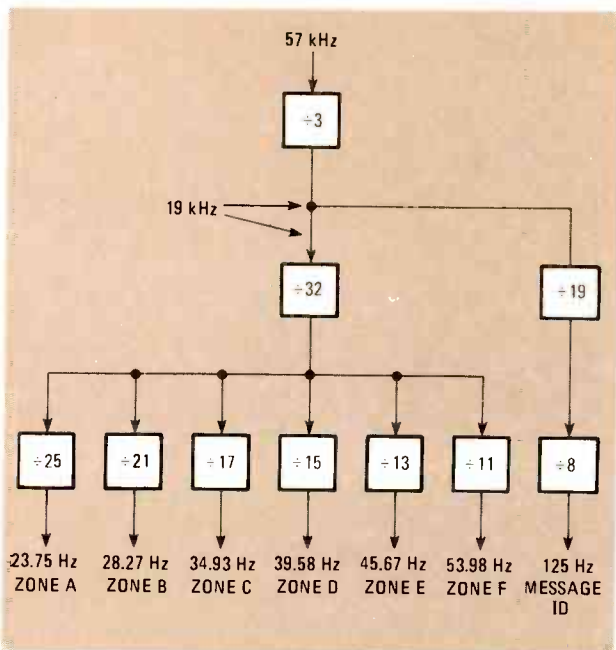


FIG. 4—ALL THE FREQUENCIES AND TONES used in the ARI signal are derived from the 19-kHz stereo pilot-tone.

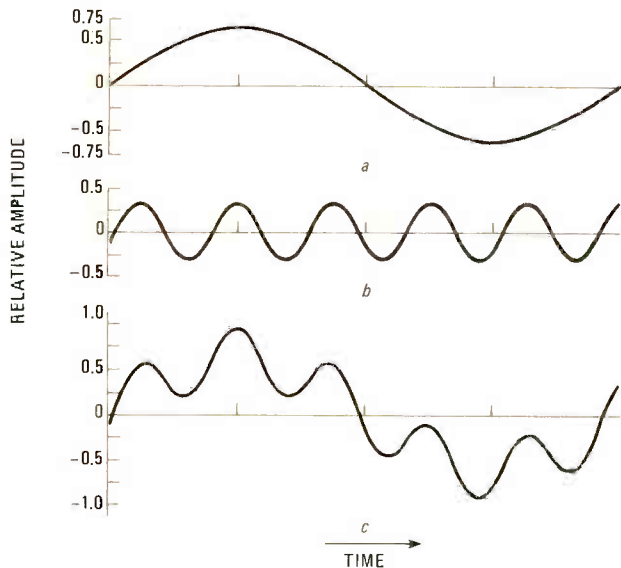


FIG. 5—ZONE-IDENTIFICATION TONE (a) is added to message-identification tone (b) to produce complex waveform (c).

19-kHz pilot signal modulates the main carrier, or between four and five percent of total modulation. The waveform shown in Fig. 3-a represents the amplitude of the 19-kHz pilot signal, while the one in Fig. 3-b is a representation of the 57-kHz ARI station-identification signal (the third harmonic of 19 kHz). Figure 3-c shows the algebraic addition of the two signals and it is clear that the peak amplitude of the resulting waveform is never greater than that of the original pilot signal. Thus, the combination of the pilot signal and the station-identification signal does not increase the frequency deviation of the main carrier. That also means that signal-to-noise ratios and station coverage-areas are not affected by the addition of the station identification signal.

#### Area identification

The limited range of FM transmissions presents both advantages and disadvantages in a traffic-information system such as that. On the one hand, drivers can be certain that the traffic information they receive applies to the region in which

they are. But it is also possible that, in certain areas, they would be able to receive more than one traffic-news station. A driver would want to be sure that he had selected the right station.

To solve that problem, Blaupunkt developed a special zone-indicating system for ARI. The total area to be covered is divided into traffic areas that correspond closely to areas covered by local radio stations. As many as six different zone identifications can be used, designated by the letters "A" through "F."

Each zone is assigned a very-low-frequency tone, which is used to modulate the 57-kHz ARI subcarrier, as shown in Fig. 4. Extensive measurements and field observations have shown that no audible interference occurs as a result of that added modulation. Zone or area identification frequencies are derived by dividing down the 19-kHz pilot tone; the values used in performing the division are also shown in Fig. 4. Depth of modulation of the 57-kHz ARI subcarrier signal is limited to just 60%.

#### Traffic message signals

While many drivers want to stay tuned to traffic-news stations throughout their travels, there are others who would prefer to hear only the traffic announcements but not the rest of the program material. For example, they might wish to converse with fellow passengers, preferring to keep the radio's volume level low, or to listen to a cassette tape for part of their trip, even though their car radio remained tuned to an ARI station.

For that reason, it was decided to use a seventh low-frequency tone, at a frequency of 125 Hz, to modulate the 57-kHz subcarrier and serve as a message-identification signal. The modulation level of that extra signal is set at half the value used for zone-identification tones and the tone is transmitted for the entire duration of the traffic message. Figure 5 shows how the modulating frequency of a zone or area identification adds to the 125 Hz "message identification" modulating frequency, with the latter having 50% of the amplitude of the former.

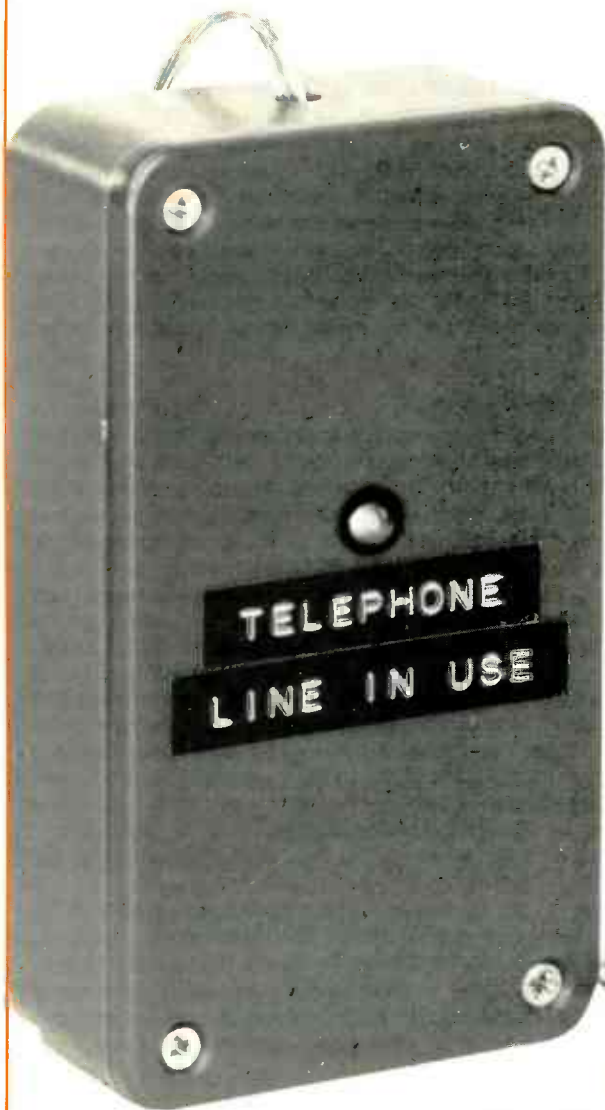
An important advantage of the ARI system is that all of the tones it uses, as well as the basic 57-kHz subcarrier itself, are derived from the stereo pilot-frequency through division or multiplication of the 19-kHz stereo pilot signal. Because of that relationship to the 19-kHz stereo pilot-signal, the design of the ARI radio receiver is greatly simplified.

#### What's available

The simplest and least expensive type of ARI receiver is one in which only traffic-news station-identification is used. In that type of receiver, an indicator light comes on when the driver tunes to a traffic-information station. If he wishes, he can push a button to mute all other stations, allowing only the ARI-equipped one(s) to come through. A somewhat more sophisticated receiver is one that combines station identification and message indication. Still another type can interrupt the playing of a tape cassette when a traffic message begins, switching to FM reception for the duration of the message, and then switch back to the cassette.

The ultimate ARI system uses a car radio with signal-search capability combined with an ARI circuit. The signal-search feature is designed to stop only at traffic-information stations and, when leaving the area of the local transmitter, it automatically searches for another traffic-information station. If, having left one zone and entered another, no other station with the same identification letter can be received, a warning tone informs the driver that a new zone-letter should be selected.

Reports from West Germany indicate that the ARI system has proven to be of great benefit. With all industrialized countries looking for unused communications channels, SCA frequencies offer a convenient means for providing new and innovative forms of point-to-point communications. R-E



CHRISTOPHER M. DUNN

EVER PICK UP THE EXTENSION PHONE IN your home, only to find out that the line is already in use, and have someone get upset because you're interrupting his (or her) call? (It's always my sister talking to one of her boyfriends.) Well, if you have that annoying situation, or would just like to know when the phone line is in use, this simple and inexpensive device will do the trick.

What the phone-line monitor does is to flash an LED whenever a telephone connected to that line is off its hook. Most of the parts needed to build it can most likely be found in your junk box, and construction is simple—the monitor can easily go on a piece of perforated board.

## TELEPHONE IN-USE MONITOR

*Do you embarrass easily? This phone line monitor will eliminate unintentional eavesdropping by indicating when a phone line's in use.*

### How it works

Let's look at what happens to the telephone line when someone takes a phone off the hook. Normally, with all phones hung up, a potential of approximately 48-volts DC exists across the two wires of the line. If any phone is picked up, it shunts across the line, and the voltage drops down to about six volts. That change is what is used to trip the monitor.

The circuit is shown in Fig 1. With the monitor connected across the phone line's red and green wires, and with all phones on-hook, a relatively strong potential is developed across resistor R2 (through R1 and R3—more about them later). That positive voltage keeps the base-emitter junction of transistor Q1 biased off. With Q1 off, there is no base current for transistor Q2; it is off, too. That keeps IC1 from flashing the LED because the return path back to the battery is not complete. This IC, an LM3909 is a low-power LED-flasher that needs only an electrolytic capacitor to flash an LED from

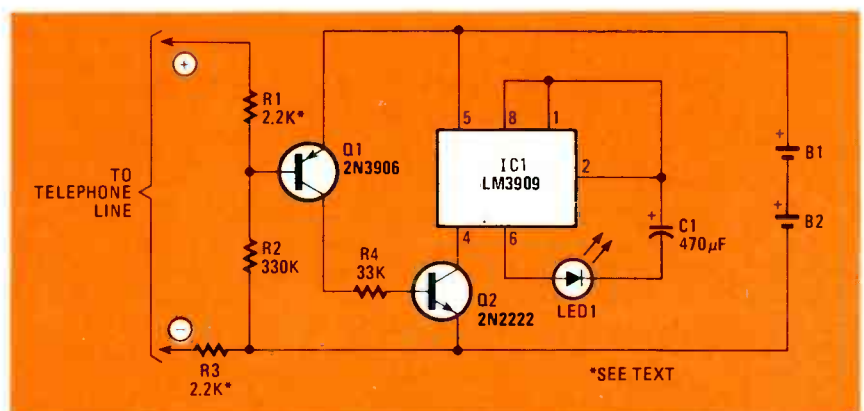


FIG. 1—BOTH POLARITY AND VOLTAGE at phone lines must be known in order for monitor to work. Use a voltmeter to determine them.



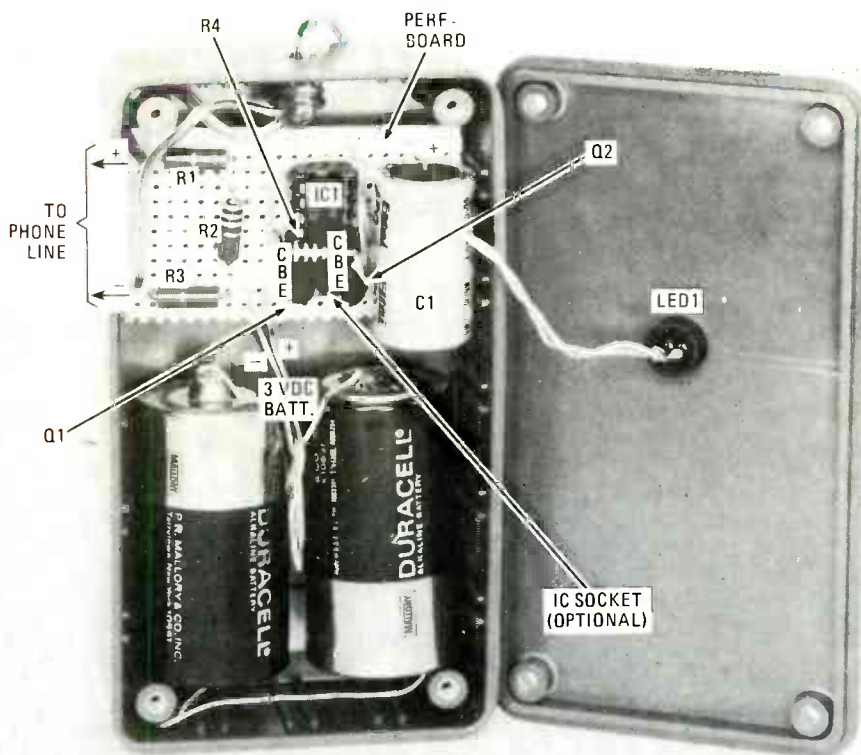


FIG. 2—COMPONENT PLACEMENT is not critical. Board and batteries are held in place by double-sided foam tape. If you wish, an IC socket can be used to hold the transistors as well as the IC. Keep the transistor leads as short as possible.

## PARTS LIST

### All resistors ½ watt, 10%

R1, R3—2.2 megohms\*  
 R2—330,000 ohms  
 R4—33,000 ohms

### Capacitors

C1—470  $\mu$ F, 10 volts, electrolytic

### Semiconductors

LED1—jumbo red LED  
 Q1—2N3906 or similar PNP-type  
 Q2—2N2222 or similar NPN-type  
 IC1—LM3909 LED flasher  
 B1, B2—1½-volt "C" cell

**Miscellaneous:** perforated construction board, case, 16-pin IC socket, double-sided foam tape, etc.

\*See text

## WARNING

Current FCC rules (Part 68) forbid direct connection of customer-owned equipment that is not FCC type-approved to telephone company lines. To use unapproved equipment, an approved protective coupler must be installed. Check with your local phone company for details.

1½ or 3 volts. I picked that arrangement for flashing the LED because the IC consumes so little power that, even if it were active continuously, the two "C" flashlight batteries would last well over a year.

When someone picks up a telephone, the phone-line voltage drops, and the potential across R2 practically disappears. That allows transistor Q1 to conduct, which, in turn, supplies base current to Q2, which also then conducts. When Q2 switches on, it provides the return path for IC1, and the LED starts flashing about three times a second. If all phones are hung up again, the voltage returns to 48 volts, shutting everything off.

Because the device connects directly to the phone line, I have taken precautions to insure that the line-monitor does not interfere with the normal operation of the phone system.

First, the unit is battery-operated, using two "C" cells. Under no circumstances should an external power supply be used. That insures that no hazardous voltages or earth grounds can be connected to the phone line.

Second, R1 and R3 provide 2.2 megohms of resistance on either side of the active circuit. (4.4 megohms total). While a single, large resistor could have been used in place of R1 and R3, I find it good practice to isolate as much as possible—again, as a safety precaution. Those resistors load down the line little, if at all.

## Construction

The circuit can be built on perforated construction board and mounted in any small box (Fig. 2). The "C" cells may be held by battery clips, or soldered directly to wires from the board. Everything is held in place by double-sided foam tape. The LED is mounted in the lid of the box. In Fig. 2, you will notice that a 16-pin IC socket is used to hold both the IC and the two transistors. While I found that to be the most convenient way to mount those components, the socket is optional.

Don't be surprised if the monitor starts blinking at you as soon as you apply power. Remember, it's a *high* voltage that turns it off. With nothing connected to it, the monitor thinks it's seeing a low voltage (in this case, *very* low), and turns on.

## Installation

The values given for resistors R1 and R3 (2.2 megohms) are for telephone systems using 48 volts, as measured with all the phones on the hook. In some parts of the country the voltage used may be different and, if you are uncertain about its value in your area, check it out with a voltmeter. Be careful when you make that measurement—that voltage can be dangerous!

If you obtain a reading that is considerably different from 48 volts, take that reading and divide it by 22. That will give you the correct value, in megohms, for R1 and R3.

The monitor will not work if it is hooked up backwards (R1 *must* go to the positive line), but it will not be harmed, either. Just reverse the leads to the phone, and you'll be in business.

With the monitor connected, before you pick up the phone, check to make sure the LED is not flashing. If it is, the line is in use. (It's probably my sister again.)

Also, check the November 1979 issue of **Radio-Electronics** for the Music-on-Hold adaptor. Build them in the same box for a super telephone add-on.

R-E

## HOW TO ALIGN VIDEO IF CIRCUITS

*Aligning video-IF strips isn't as difficult as you may think. Here are some helpful hints.*

**JACK DARR**  
SERVICE EDITOR

MANY TECHNICIANS CONSIDER VIDEO-IF alignment to be the most complex task they have to perform. But that's not true—the stages involved are not more complicated, it's just that there are more of them than in a radio! And, as the saying goes, "Complicated things are just a lot of simple ones strung together."

AM and FM radios have relatively narrow bandpasses—10 kHz in the case of AM; from 200 to 250 kHz in the case of FM. Generally, they use cascaded circuits (one circuit right after the other) operating on a single frequency. Video-IF stages have bandpasses as wide as 5 MHz—they're known as controlled-bandpass, wideband IF's—and in most respects are similar to the ones in radios, except that the tuned circuits are *not* all aligned on the same frequency.

The important thing in performing video IF-stage alignment is not gain, but rather the overall response of each stage. That is easy to adjust with a sweep generator, which we'll discuss shortly.

The video IF-strip consists of several cascaded amplifier stages, each with a tuned circuit at its input, output, or at both ends. Each stage has an ideal bell-shaped curve representing its response. The cartoon in Fig. 1 shows how the tuned circuits in an IF stage work. Each resonant circuit in the stage "pushes the curve up" at its resonant frequency. Using several circuits gives us the wide bandwidth we need. (The two figures sitting on the ends of the curve and holding it down will be discussed later.)

Figure 2-a shows the overall response of one IF-stage, with one of the tuned circuits peaked at the wrong frequency. The dip in the curve caused by this misalignment is obvious. In Fig. 2-b the

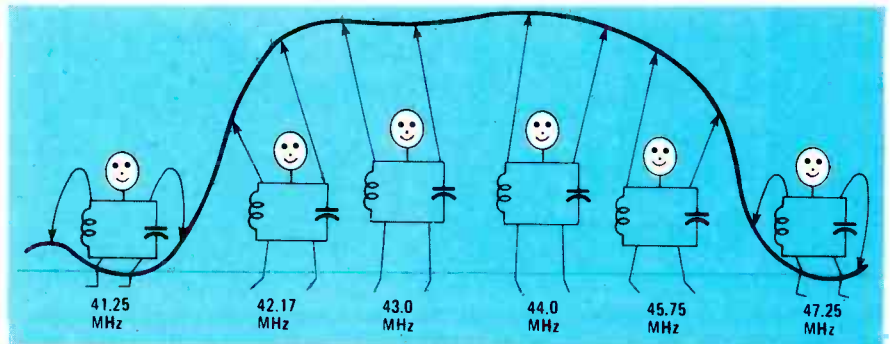


FIG. 1—EACH RESONANT CIRCUIT in the IF strip works to give the bandpass curve the correct shape.

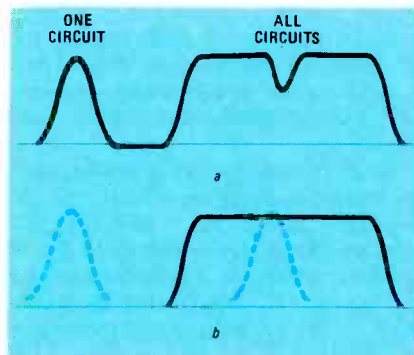


FIG. 2—AN OFF-FREQUENCY circuit will alter the shape of the curve. Retuning it will restore the curve to normal.

misaligned circuit has been retuned to the correct frequency and the overall response of the stage is now what was intended. That's how *all* the resonant circuits in an IF stage work—they alter both the height *and* the shape of the curve at the points they affect. When an IF stage is properly aligned, the resulting curve looks pretty much like the one in Fig. 2-b.

### Traps

Shaping the response of an IF stage means not only boosting certain frequencies, but also attenuating or eliminating some of them. That's what the two figures sitting on the ends of the curve in Fig. 1 are doing.

Figure 3 shows the two types of resonant circuits used in curve shaping. The parallel-resonant circuit at the right of Fig. 3-a boosts the response at the resonant frequency, as shown in Fig. 3-b. The series-resonant circuit at the left of Fig. 3-a does the opposite—it removes signals at its resonant frequency. (It has a very low impedance at resonance.)

Series-resonant circuits are used to reduce the strength of, or get rid of entirely, unwanted signals at specific frequencies. When they perform that function, they are called *traps*.

Traps are never used within the bandpass range; they are used to shape the slopes of the ends of the curve and to insure that signals from other channels do not get into the IF strip. The major



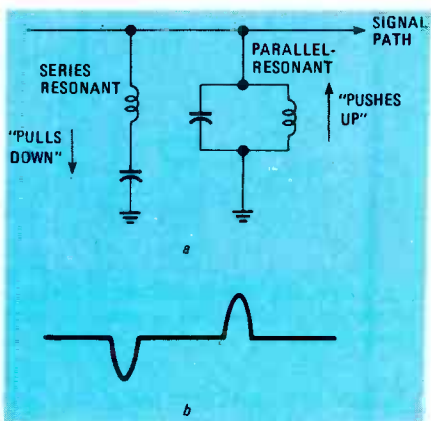
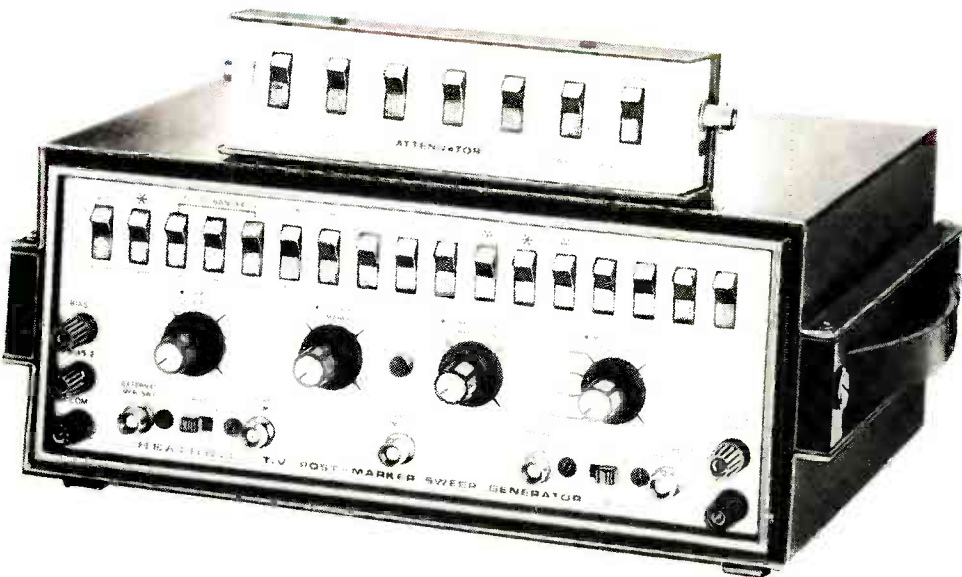


FIG. 3—A SERIES-RESONANT circuit has low impedance and acts as a trap. A parallel-resonant one reinforces the signal.

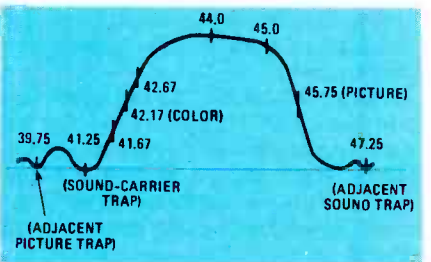


FIG. 4—A REPRESENTATIVE IF CURVE, showing all the key marker-frequencies.

difference between tuning traps and the other resonant circuits in the IF strip is that the traps are always adjusted to give *minimum* response. Because they determine the shape of the endpoints of the response curve, tuning the traps is always the first part of any TV-IF alignment procedure.

**Sweep alignment**

To align a TV-IF circuit properly, it is

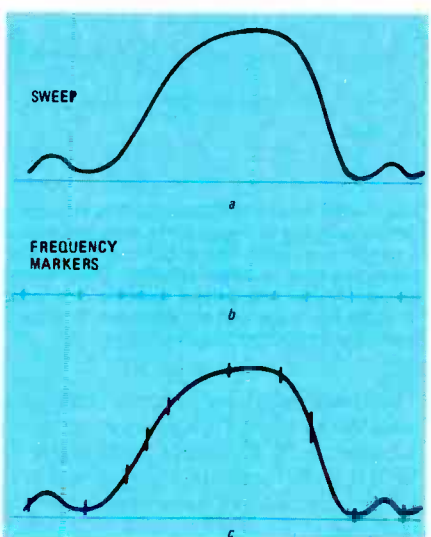


FIG. 5—SWEEP AND MARKER SIGNALS are mixed in the marker adder to create a marked-sweep curve to be fed to an oscilloscope.

important to be able to see the response of the entire curve. That way, the effect of any adjustment on the overall shape of the curve is instantly obvious. If you try using single-signal methods, and tuning each circuit for maximum, you can wind up with some *very* interesting results! Therefore, sweep-alignment equipment, which allows you to view the entire curve at once, is required.

The original sweep-frequency generators were called "wobblers" because they wobbled (swept) the signal back and forth; the response-curve of the IF strip was displayed on an oscilloscope. What they didn't do was to locate, or mark, the critical frequencies on that curve.

There are *nine* different frequencies (see Fig. 4) that are critical to IF-strip

alignment, and it is important that adjustments be made exactly at those frequencies. To locate them, a marker generator is used.

**Marker generators**

In the early days, markers were placed on the curve by a tunable RF signal-generator. The disadvantage of that was that only one marker could be seen at a time. The signal generator had to be retuned each time a new frequency was checked. (There was a way around that. The critical points could be marked, one by one, on the screen of the oscilloscope with a grease pencil. That system worked fairly well as long as the sweep generator was not retuned.)

Another disadvantage was that when the marker frequencies were fed through the video-IF-strip together with the sweep signal, the curve could be badly distorted if the level of the marker signal was too high. The marker generator also had to be *very* accurately calibrated.

**Current sweep-generators**

The current generation of sweep generators makes alignment a lot simpler. They have two very useful features. First, they have separate, crystal-controlled, markers for each key frequency. Any, or all, of the markers can be used at any time.

The other feature is a circuit called a post-injection marker-adder (or just "marker adder," for short). The marker adder is actually separate from the sweep generator and only the sweep signal goes through the circuits being aligned. A small portion of that signal is fed to the marker adder, and the markers are added electronically at that point. The marker-adder's output is then fed to the scope. Figure 5 will give you an idea of how that works.

The crystal-controlled markers are extremely accurate because each one is generated by a separate circuit. Furthermore the markers cannot cause curve distortion in the IF stage because they never pass through it.

With today's equipment, and a little knowledge of what's going on, video-IF-strip alignment turns out to be a lot less complicated than you may have thought it to be.

R-E

# DESIGNING CIRCUITS WITH OP-AMPS

Perhaps the most universal integrated circuit is the operational amplifier. Here's how to design your own op-amp circuits

JOSEPH J. CARR

THE INTEGRATED CIRCUIT WAS INVENTED in the early 60's, and has taken off like a rocket ever since. Devices have grown steadily in complexity. The early  $\mu$ A703, for example, contained only a few transistors and a couple of resistors, and was used extensively as an FM IF amplifier...and not much else. The  $\mu$ A703 was a real hit, but that device is now considered "low technology" and is no longer used.

We now have MSI and LSI (Medium Scale Integrated and Large Scale Integrated) devices that may contain hundreds or thousands of transistors and other components on a single chip. They are even developing VLSI (Very Large Scale Integrated) circuits.

The biggest portion of the IC market are the digital IC's, but don't count analog devices down and out quite yet; they are alive and kicking in many areas of technology and can out-perform devices made only a few years ago.

There are several technologies used for creating transistors and other components on a slab of semiconductor material. This slab is referred to as a substrate. There may be several layers of material in the integrated circuit of which the substrate is the bottom-most.

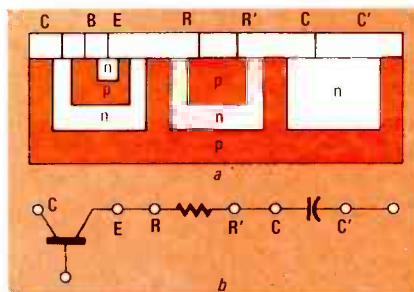


FIG. 1—AN INTEGRATED CIRCUIT is formed by diffusing layers of p-type and n-type material on a p-type substrate. The uppermost layer is an insulating layer of silicon dioxide. Connections to the n-type and p-type material are made through this layer and are indicated by vertical lines. The equivalent circuit is shown in b.

The usual substrate is approximately 6 mils thick, with a typical cross-sectional area being  $50 \times 50$  mils, with some up to  $160 \times 160$  mils. In Fig. 1-a, the substrate is shown as P-type semiconductor material.

The second layer is made of N-type material, and is grown as an extension of the P-type substrate crystal. In operation, that PN junction must be maintained at a reverse bias potential or the IC will be destroyed. That region is approximately 5 to 30 micrometers thick. The next region is P-type material, while the uppermost is again N-type material. Lastly, a layer of silicon dioxide is formed over the top of the silicon slab. The silicon dioxide is an insulating material and connections to the various regions are made through that layer, indicated in Fig. 1-a as vertical lines.

The equivalent circuit is shown in Fig. 1-b. In this case, a transistor is in series with a resistor and capacitor. The transistor is formed from elements of the second, third, and fourth layers of the substrate. Since the transistor is an NPN device, the collector and emitter terminals are connected to N-type (second and fourth) layers of the substrate. The series resistor is formed by the re-

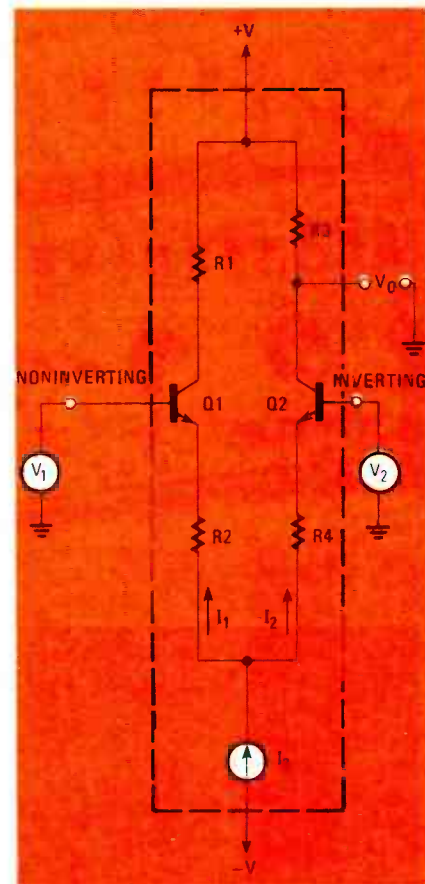


FIG. 2—OP-AMP INPUT CIRCUIT is actually a differential amplifier that requires a bipolar power supply.

sistance of a section of the N-type second layer. It is connected to the emitter section by depositing a metallized strip over the silicon dioxide.

The capacitor is formed by sandwiching the silicon dioxide between an N-type layer and a metalization layer. The dielectric of the capacitor is the silicon dioxide layer.

Integrated circuits do not often contain capacitors because of the size and cost. In general, only small-value (picofarad-range) capacitors can be integrated onto the substrate. Hybrid circuits, which use a combination of integrated-circuit technologies and discrete component techniques, often use small tiny capacitors called chip capacitors. Those capacitors are mounted on a ceramic substrate along with several unpackaged IC chips.

## The operational amplifier

The operational amplifier is a linear integrated circuit that has an immense variety of applications. The op-amp can be used in relatively complex circuits, yet the design rules are easy to master. The typical operational amplifier has two inputs, called inverting and non-inverting inputs. That is not a require-



ment in the definition of the operational amplifier, but it is true that almost all op-amps have two inputs: Only a few devices on the fringes of the linear IC market are op-amp-like, yet have but one input (the LM302 device, for example).

The operational amplifier was designed originally to perform mathematical operations in analog computers. That means that it had to operate on a variety of input-data values, and then be able to produce an output of either polarity depending upon the required answer.

As a result, operational amplifiers require a dual-polarity power supply. The positive (+V) power supply is positive with respect to ground, while the negative (-V) power supply is negative with respect to ground.

Figure 2 shows a typical input circuit for an operational amplifier. The two transistors (Q1 and Q2) of the differential pair are connected so that their emitters are fed from a single constant-current source ( $I_3$ ). The constant-current source will produce a constant current, despite changes in the load resistance. Most IC constant-current sources are bipolar transistors, biased in a particular manner. In Fig. 2, the two emitter currents ( $I_1$  and  $I_2$ ) are derived from the constant source  $I_3$ . We know from Kirchoff's current law that the following relationship holds true:

$$I_1 + I_2 - I_3 = 0 \quad (1)$$

$$\text{or} \quad (2)$$

$$I_1 + I_2 = I_3 \quad (2)$$

For the purposes of this discussion, we are going to assume that the emitter and collector currents of the two transistors are equal (i.e.,  $I_{C1} = I_{C2}$  and  $I_{E1} = I_{E2}$ ). In actual fact they are different by two to five percent, but that does not present a problem.

Let's assume that a voltage ( $V_1$ ) is applied to the base of transistor Q1. What happens? How does the circuit respond? When  $V_1$  is made positive, the collector and emitter current of Q1 ( $I_1$ ) will increase. That increase in current  $I_1$  must (by equations 1 and 2) cause a decrease in current  $I_2$ . Current  $I_2$  is the emitter current in the transistor Q2. Since  $I_2$  decreases, the voltage drop across resistor R3 also decreases (i.e.,  $I_2 \times R3$  decreases). The output voltage  $V_0$  is the difference between the collector potential and the voltage drop across resistor R3, so a reduction in  $I_2$  causes an increase in  $V_0$ . Here we have a positive increase in  $V_1$  causing an increase in output-potential  $V_0$ . The base of transistor Q1 is, therefore, the non-inverting input.

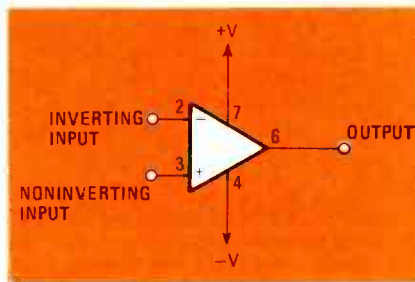


FIG. 3—SCHEMATIC SYMBOL and industry standard pinout of an operational amplifier.

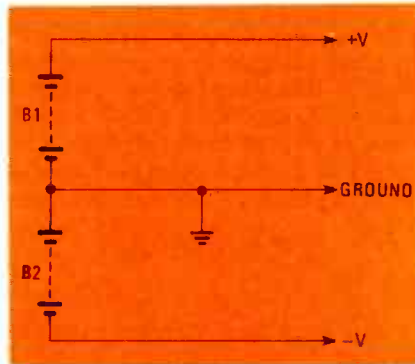


FIG. 4—BIPOLAR POWER SUPPLY can be built using batteries as shown.

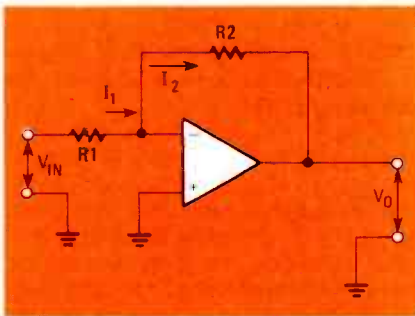


FIG. 5—BASIC INVERTING AMPLIFIER. The gain is determined by the ratio of R2 and R1. Point A is called a virtual ground.

TABLE 1

1. Infinite input impedance
2. Infinite open-loop (no feedback) gain
3. Zero output impedance
4. Infinite bandwidth
5. Zero noise contribution
6. Both input voltages track each other.

Now let's examine what happens when an input voltage ( $V_2$ ) is applied to the base of transistor Q2. When voltage  $V_2$  is positive, current  $I_2$  increases. When current  $I_2$  increases, the voltage drop across resistor R3 increases. The increased voltage drop across R3 causes a decrease in the output voltage. Therefore, the base of transistor Q2 is the

inverting input: a positive input voltage produces a decrease in the output voltage.

Output-voltage  $V_0$  is normally zero when both input voltages ( $V_1$  and  $V_2$ ) are equal.

### Operational amplifier symbol

The operational amplifier symbol used in circuit diagrams is shown in Fig. 3. It consists of a triangle with the output at one apex, usually oriented horizontally. Some texts follow the IEEE convention of using the straight-back symbol (as shown here) for linear amplifier IC devices, and a similar version with a curve back for the operational amplifier. In *Radio-Electronics*, however, we use the more common convention—as shown in Fig. 3.

The two inputs of the operational amplifier are labeled (-) for the inverting input and (+) for the noninverting input. The +V and -V power-supply terminals may or may not be shown in some schematics. Many people delete the power-supply terminals on their drawings for the sake of simplicity. Make no mistake about it, however: The power-supply terminals are still to be connected! The pin-out numbers shown in the illustration were originally for the 741 device only, but that particular arrangement is now considered the "industry standard." Most commercial integrated-circuit op-amps use that pinout.

The +V and -V power-supply terminals are not +V and ground, but two separate power supplies of opposite polarity with respect to ground. The +V power supply is positive with respect to ground, while the -V power supply is negative with respect to ground. A battery version of the typical operational amplifier power supply is shown in Fig. 4. Note that this power supply has a ground connection, but there is no ground terminal on the operational amplifier symbol! The input and output potentials are measured with respect to ground, so the ground must come from the power supply.

### Operational amplifier properties

A simple linear amplifier using an operational amplifier is shown in Fig. 5. We can analyze the operation of this circuit by using Kirchoff's current law and the basic properties of the operational amplifier. For purposes of discussion, we will consider the properties of an *ideal* operation amplifier. Table 1 lists the six basic properties of the ideal operational amplifier:

An infinite input impedance means that the input neither sinks nor sources current. The input impedance of any amplifier is given by  $V_{in}/I_{in}$ . If the input

will neither accept (sink) nor generate (source) current, then  $I_{in}$  is zero and the input impedance is infinite. In actual operational amplifiers, which are not ideal, the input impedance is not quite infinite; but it's extremely high. Some low-cost cheapie operational amplifiers are only able to offer input impedances of 100,000 ohms, but most devices can boast 1 megohm or more. A few devices, such as the RCA BiMOS devices (which have MOSFET input transistors) have input impedances of 1.5 teraohms ( $1.5 \times 10^{12}$  ohms)! That reflects input currents of picoamperes or nanoamperes.

Infinite open-loop gain means that the amplifier gain is infinite when there is no negative feedback present. In real operational amplifiers, the open-loop gain will be 20,000 for cheapies, and over 1,000,000 for some premium devices.

An ideal operational amplifier is said to have a zero output impedance. In real operational amplifiers, however, we find output impedances of less than 200 ohms, with most under 75 ohms.

Infinite bandwidth means that the device will amplify all signals applied to the input, regardless of frequency. But, that is not the case in real operational amplifiers. Many devices operate into the HF region and some devices operate into the low VHF region. Most common operational amplifiers, however, are severely limited in frequency response. The popular 741 device, for example, has a frequency response of only a few kilohertz.

Zero noise-contribution means that the op-amp adds no noise to the signal it amplifies. Unfortunately, most operational amplifiers fall far short of that ideal: Some premium (high cost) devices offer very good noise performance, but most common operational amplifiers do not perform well as low noise-amplifiers.

Both input voltages track each other. What does that mean? It means that applying a voltage to one input requires us to treat the other input mathematically as if it, too, were connected to the same voltage. That is not merely some theoretical device used in mathematical formulas; it is real. If you apply 4 volts to the noninverting input, then you can measure 4 volts at the inverting input also! That phenomenon is one of the most important of the ideal properties!

### Inverting-follower circuits

Figure 5 shows the circuit for the inverting-follower configuration. An inverting follower uses the inverting input of the operational amplifier. Note that the noninverting input is grounded in this circuit. That is the same as saying that the noninverting input is at zero potential. A result of ideal property No. 6 listed in Table 1 is that the inverting input must now be treated as if it were also at zero potential. The inverting input is essentially grounded, even though

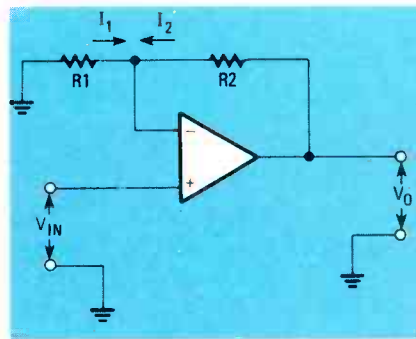


FIG. 6—BASIC NON-INVERTING amplifier. The input signal is fed to the non-inverting input terminal.

not physically connected to ground. That confusing state of affairs is not made too much clearer by the name usually given to the phenomenon: "virtual ground." The virtual ground is *treated* as a ground even though it is not actually grounded through a piece of wire.

What do we know about the circuit in Fig. 5? We know that the currents are as follows:

$$I_1 = V_{in}/R1 \quad (3)$$

and,

$$I_2 = V_o/R2 \quad (4)$$

we also know from Kirchoff's current law that:

$$I_1 = -I_2 \quad (5)$$

So, by substituting equations 3 and 4 into equation 5, we obtain:

$$V_{in}/R1 = -V_o/R2 \quad (6)$$

We can solve equation 6 for  $V_o$ , thereby obtaining the transfer equation for the inverting follower:

$$V_o = -V_{in} \times R2/R1 \quad (7)$$

The gain of any amplifier is the quotient  $V_o/V_{in}$ , which in this case is  $R2/R1$ . That relationship means that we can set the gain of the inverting-follower operational amplifier circuit by setting the ratio of two resistors! The absolute values of the resistors are not important, only their ratio. For example, if the feedback resistor ( $R2$ ) is 100,000 ohms, and the input resistor is 1000 ohms, then the gain  $R2/R1$  is 100,000/1,000, or 100.

There is a problem associated with the inverting follower. The input impedance is low, being limited to the value of input-resistor  $R1$ . That is because one end of  $R1$  is grounded as a result of the "virtual" ground. The apparent solution to the problem is to use an input resistor that has a sufficiently high value. But that is not always possible, due to gain problems (remember, the open-loop gain is not infinite), and because certain problems with real operational amplifiers are made worse by using high-value resistors in the feedback and input circuits. Unless phase inversion is needed in the circuit, there may be good reason to opt for the non-inverting follower.

### Non-inverting follower with gain

Figure 6 shows the circuit for the non-

inverting-follower configuration. In this circuit, the signal is applied directly to the non-inverting input of the operational amplifier. The feedback network is the same as in the inverting follower, except that  $R1$  is now grounded.

Recall ideal property No. 6 listed in Table 1: Applying voltage  $V_{in}$  to the noninverting input has the effect of placing the other (inverting) input at the same potential. Since there is no phase inversion in the circuit, the output signal has the same polarity as the input signal, so:

$$I_1 = I_2$$

By the same sort of reasoning as in the previous case:

$$I_1 = V_{in}/R1 \quad (9)$$

and:

$$I_2 = (V_o - V_{in})/R2 \quad (10)$$

We can obtain the transfer equation for the circuit by substituting equations 9 and 10 into equation 8, which yields:

$$V_{in}/R1 = (V_o - V_{in})/R2 \quad (11)$$

Algebraically rearranging equation 11 yields:

$$V_{in} \times [(R2/R1) + 1] = V_o \quad (12)$$

Equation 12 is the transfer equation for the non-inverting follower with gain circuit shown in Fig. 6. Note that the circuit will always have a gain of at least 1, since the gain factor is  $(R2/R1) + 1$ .

The input impedance of the non-inverting-follower circuit is very high, being limited by the input impedance of the operational amplifier. Recall that typical operational amplifiers have an input impedance greater than 1 megohm, with some models offering impedances as high as  $10^{12}$  ohms. The non-inverting follower, therefore, is best suited for use with high-impedance circuits. In the case of some oscillator and timer circuits, it also relieves us of the problem of considering the effects of the input impedance of the amplifier on R-C time constants.

### Unity gain non-inverting followers

In the non-inverting-follower circuit shown in Fig. 6, the feedback was only a fraction of the output signal and was set by a voltage divider consisting of  $R1$  and  $R2$ . Let's investigate what happens when we feed back all of the output signal. We can accomplish that by connecting the output of the operational amplifier to the inverting input directly, as

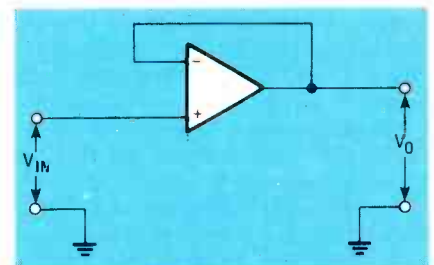


FIG. 7—UNITY-GAIN AMPLIFIER has high input impedance and low output impedance. This circuit is used as a buffer.



shown in Fig. 7.

Substituting  $R_f = 0$  in equation 12 yields:

$$V_o = V_{in} \quad (13)$$

Thus, the gain of the circuit shown in Fig. 7 is equal to 1. To understand why, recall ideal property No. 6. We know that if  $V_{in}$  is applied to the non-inverting input, then that same potential must also exist on the inverting input. But the inverting input is also connected to the output, so  $V_{in}$  must also exist on the output of the operational amplifier!

OK, but what's the use of a unity-gain amplifier? Aren't amplifiers supposed to amplify? The voltage amplification is nearly unity in that circuit (0.9999999), yet the output impedance is very low. Since the input impedance of the operational amplifier is very high, then it becomes obvious that the unity-gain follower can be used for impedance transformation without loss of amplitude between a high-impedance source and a low-impedance load. Also, the unity-gain non-inverting follower can be used as a buffer stage to provide some isolation without either a change of amplitude, or phase inversion.

### Differential amplifiers

The two input terminals of an operational amplifier are complementary; that is, they produce an equal but opposite effect on the output signal. If a voltage is applied to the non-inverting input, the output will have the same polarity as the input signal. But, if that same voltage is applied to the inverting input, then the output will have the opposite polarity. The gain of the amplifier in each case is the same, but the output polarity is opposite. The inputs of the operational amplifier are, therefore, differential. The actual input voltage seen by the op-amp is the difference between the potentials applied to the inverting and non-inverting inputs. We can, therefore, use the operational amplifier to make a differential amplifier.

An example of a simple operational differential amplifier (diff-amp) is shown in Fig. 8. This circuit is the simplest form of a diff-amp.

The gain of this circuit is:

$$\text{Gain} = R_3/R_1 \quad (14)$$

Provided that

$$R_1 = R_2 \quad (15)$$

$$R_3 = R_4 \quad (16)$$

The ideal differential amplifier will not respond to a common-mode voltage (that is, a signal voltage applied equally to both inputs simultaneously). The real differential amplifier, however, will respond somewhat to a common-mode voltage and produce a small output voltage, called the common-mode error voltage. The ratio of the common-mode voltage (a voltage applied equally to both input terminals) to the common-mode error voltage (resulting error voltage that appears at the output of the

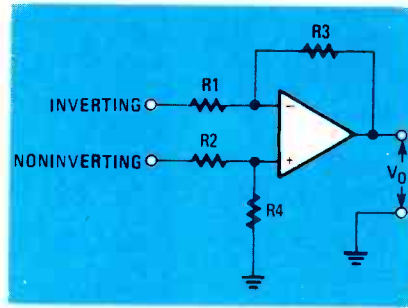


FIG. 8—DIFFERENTIAL AMPLIFIER circuit amplifies the difference between the two input signals.

op-amp) is called the common-mode rejection ratio (CMRR) and is expressed in dB. Some operational amplifiers have a CMRR of 120 dB (1,000,000:1), while even garbage-grade blister-pack op-amps have CMRR ratings in the range of 60 dB!

The differential amplifier is used extensively in circuits where noise pick-up is a factor. The human electrocardiogram signal, for example, is very weak (1 mV), yet interference from 60-Hz power lines can be several volts on an 8-foot cable leading to the patient being monitored. The result is that the signal is completely swamped by 60-Hz interference that is 1000 times greater! However, if we treat the electrocardiogram signal from the surface of a patient's body as a differential signal, we find that the 60-Hz signal will be seen by the differential amplifier as a common-mode signal, whereas the electrocardiogram signal is seen as a differential signal. The gain of the amplifier may be 1000 for the differential signal and the amplifier will significantly attenuate the 60-Hz components. The result is an electrocardiogram trace that is essentially free of 60-Hz interference.

### Operational amplifier problems

The properties of the ideal operational amplifier are never realized in practical devices. The ideal properties are closely approximated in some premium devices, but there is always some discrepancy. Those problems fall into several categories. We have already discussed the matter of frequency response and common-mode rejection ratios. We also find that there are several DC-offset problems that cause the output voltage to be non-zero at times when it should be zero.

There are several sources of offset voltage. One is the bias currents of the transistors used in the input circuit. Remember that the ideal operational amplifier has an infinite input impedance, which means that the input terminals will not sink any current. But real operational amplifiers are built from real transistors that require bias current. The bias current for some premium grade devices may be nanoamperes, or

even picoamperes, but in some cheapies the bias current may be a fraction of a milliamperes! The error voltage generated at the output of the operational amplifier by this bias current is equal to:

$$I_{\text{bias}} \times R_f$$

where  $R_f$  is the resistance of the feedback resistor. Also, the bias current will cause a voltage drop to appear at the input terminal that is equal to the product of the bias current and the parallel combination of the feedback and input resistances [ $R_f \times R_2 / (R_f + R_2)$ ].

One method for reducing the error voltage caused by the input-bias current is shown in Fig. 9. That circuit works because the operational amplifier input circuit is symmetrical, meaning that identical currents will flow in both input terminals. If the value of resistor  $R_3$  is equal to the parallel combination of  $R_1$  and  $R_2$ , then both input terminals see an equal resistance to ground. The bias current at each input terminal will then generate an equal error voltage at each input terminal and the common-mode rejection ratio will cancel the effect at the output terminal.

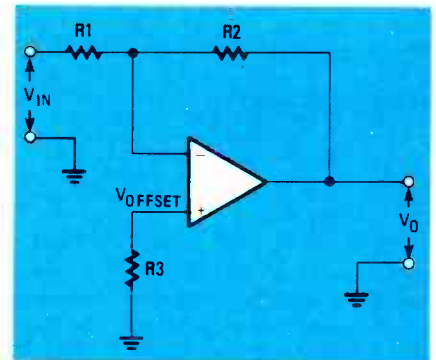


FIG. 9—INPUT BIAS CURRENT causes an error voltage to appear at the output of the op-amp. The voltage drop across resistor  $R_3$  (caused by the input bias current) cancels the output error voltage.

Unfortunately, input-bias currents are not the only source of offset voltages on the output line. There are actually several causes, some of them inside of the operational amplifier and others from outside sources (for example, the power supply). The circuits shown in Figs. 10 and 11 will allow us to cancel any type of offset voltage, including the offset voltage caused by the input-bias current.

The circuit shown in Fig. 10 is used with operational amplifiers that have offset compensation terminals. Those terminals allow us to balance the emitter currents of the input amplifier transistors to allow for offset variations.

Another, more universal, method for cancelling the offset voltage is shown in Fig. 11. In this circuit, which can be used whether or not the operational amplifier has offset-compensation terminals, we add a current to the input sum-

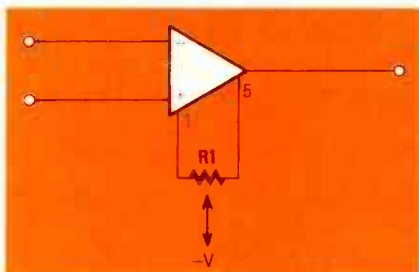


FIG. 10—OFFSET COMPENSATION terminals are provided on some op-amps. Potentiometer R1 is adjusted to eliminate offset errors that appear at the output.

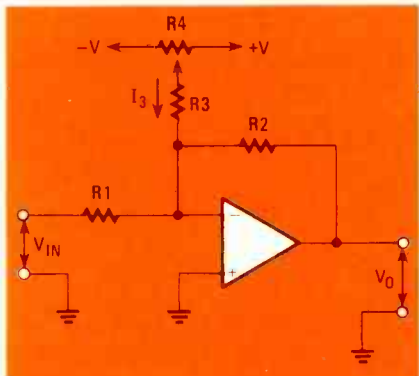


FIG. 11—SIMPLE CIRCUIT for eliminating offset errors with op-amps that do not provide offset compensation terminals.

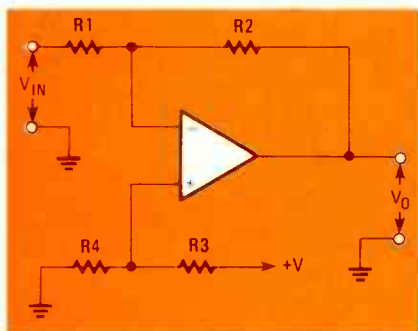


FIG. 12—SINGLE-POLARITY POWER SUPPLY can be used with an op-amp by biasing the non-inverting input at half the power-supply voltage. In this case, resistors R3 and R4 are equal.

mation junction of the inverting follower (or the non-inverting follower, if desired) that exactly cancels the output offset voltage. Resistors R1 and R2 are the normal input and feedback resistors used in the amplifier, while R3 and R4 are part of the offset cancellation circuit. Potentiometer R4 is adjusted so that current  $I_3$  exactly cancels the normal offset voltage and no more (otherwise, the offset-cancellation voltage becomes an offset in its own right.)

The operational amplifier is designed to operate from bipolar power supplies.

During normal operation, the  $-V$  and  $+V$  power supply contributions to the output voltage depend upon the polarity of the input signal. When the input signal is zero, the respective contributions are zero. But what happens when the operational amplifier must be operated from a single-polarity power supply? In that case we must bias one input (usually the non-inverting input) to some potential between zero and the power-supply voltage. The output voltage will be equal to that potential when the input signal is zero, and will swing about the bias potential when the input signal is non-zero. In most cases (see Fig. 12) the non-inverting input is biased at one-half  $+V$  by making resistors R2 and R3 equal to each other. R-E



"NO! NO! NO! That's not what I meant by trouble-shooting!"

## SERVICE QUESTIONS

### HALF RED-BLUE, HALF GREEN

I've got a Philco C7261TMA-1 whose screen is red-blue on the left and green on the right. I changed the picture tube (the old one was bad, anyhow), but that didn't help. Where do I go from here?—L.B., Salt Lake City, UT

I've seen almost the same thing—also in a Philco. The left half was gold and the other blue. Try scoping all the B+ lines around the bandpass-amplifier stages—any point that has a bypass capacitor on it. You should see no signals at all. If you do, one of the bypasses isn't working and you will get feedback that upsets the color.

(Feedback: Thanks for the idea. The scope showed all kinds of signals on the B+ lines. I replaced both of the big filter capacitors and that cured the color problem and some others in the horizontal and vertical circuits.)

### TOP-STRETCH CURE

My good buddy Bill Stiles, of Hollsboro, MO, has sent me another of his jewels. He had asked about top-stretch in an Admiral 12H10 and I suggested checking the .039  $\mu$ F capacitors in the vertical-output grid circuit.

He did, and although they checked out OK, he decided to replace C74 and C76 anyway. That cured the stretch!

(And showed up another problem. The vertical-centering control wouldn't work properly. A new one set everything right.)

If you run into this sort of problem in this or similar chassis, try new capacitors, even if the old ones look OK.

### HOT RESISTOR

This RCA CTC-31A burns up R163 (the plate load-resistor from the horizontal-oscillator plate to B+) and then loses drive. A new resistor brings back the HV for about two minutes and then the resistor burns up again. The tubes, etc. all seem to check out. What's going on here?—B.C., Kent, OH

This sounds familiar—we ran into almost the same thing in a CTC-22 some time ago. The horizontal-oscillator plate in this set is fed by a "parallel path." At turn-on, voltage is fed through R163 from B+; after the set warms up, the oscillator is fed through a pair of 220K resistors in series from boost and R163 doesn't have to carry so much current.

Check to see whether one or both of the 220K units are bad and replace what's necessary. If they were bad, R163 would have had to carry the full load, and it's only a 1/2-watt type. Replace it with a 1-watt just for luck.

### ODD PICTURE

I've got a TS941 Quasar. I get a couple of black patches near the top of the raster—they come and go, as well as writhe. Even-

tually the picture goes dark and narrow and compresses in the center, making a bright vertical streak. This is weird!—J.G., Oak Park, IL

It certainly is. I've heard of something like this before. The cause of the problem is usually a big 500  $\mu$ F filter capacitor, Q508, located under the power-supply chassis. The negative connection breaks loose or becomes intermittent. Make sure the ground lead is good, and well soldered.

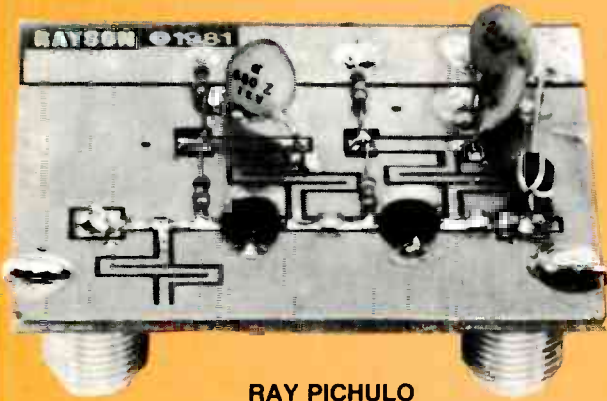
### LOSS OF VIDEO

I've got good sound but no video in this RCA KCS-169B. The base of the video amplifier (Q3) is OK with no signal (+2 volts), but goes to -5.5 volts when signal is applied, cutting off that stage. Replacing the transistor did no good. The video signal to the base is too high (5.5 volts); it should be 2 volts. Any suggestions?—W.M., Springville, NY

Yes! You should recheck the Q3's base circuit; that is L8, R22, R24, and R3 to ground. Apparently there is some positive voltage being fed into the control circuit from the detector-return circuit and R21 to ground. I'd say that this should go more positive with increasing signal strength since it comes off the detector cathode. That should prevent the base of Q3 from being driven into cutoff. Check the video-bias control to see if it does anything; it should. I'd also check the little choke for an open circuit, etc. Also check for bad solder joints. R-E



# UHF-TV PREAMPLIFIER



RAY PICHULO

*This inexpensive antenna-mounted UHF-TV preamplifier can add more than 25 dB of gain to your system and pull in signals you never knew were there. You'll also learn how to optimize your UHF reception through other means.*

UNTIL RECENTLY, NOBODY SEEMED TO care too much about good UHF-TV reception, and most people were content to take whatever quality they could get. The situation became serious enough to warrant an investigation by a committee made up of FCC and industry representatives. They published their findings late in 1980, and their major conclusion was that the most direct way to improve UHF-TV reception was through effective receiving-antenna systems.

### Adding more gain

Antenna selection and feedline considerations were discussed in the July, 1981 issue of *Radio-Electronics*, and we'll take a closer look at them in Part 2 of this article, but what happens if the proper antenna and feedline are used and we still don't get the results we want. What then? The next step is to consider a mast-mounted preamplifier.

First, let's clear up a common misconception about preamplifiers. Many people believe that a preamplifier aids reception by boosting the signal level; that's only partly true. What is more

important is that a preamplifier reduces the system noise-figure, which is the overall limiting factor to any receiving system's sensitivity.

There are two sources of noise—external and internal. External noise may be either atmospheric noise or man-made noise from electrical discharges. At UHF frequencies, external noise is very low, so the major noise source is internal—circuit noise. There is a great deal of room for improvement here, since a typical UHF tuner has a noise-figure of approximately 12 dB. The amount of noise introduced by the front end of a receiver plays a major part in establishing the overall receiver noise-figure, because each successive stage amplifies the noise introduced in the preceding stages.

The effect of gain on overall-system noise-figure can be calculated using the following formula:

$$N_T = N_1 + \frac{N_2 - 1}{G_1} + \frac{N_3 - 1}{G_1 G_2}$$

Where:

$N_T$  = overall-system noise-factor

$N_1$  = noise-factor of the first stage

$N_2$  = noise-factor of the second stage

$N_3$  = noise-factor of the third stage

$G_1$  = power gain of the first stage

$G_2$  = power gain of the second stage

Note that all numbers must be in terms of power gain, because the use of dB will result in large errors—especially when low noise-figures are involved. Noise-factor can be converted to noise-figure using the following formula:

$$Nf (g) = 10 \log_{10} N$$

Where:

$g$  = gain in dB

$N$  = noise factor

$Nf$  = noise figure

Noise-figure can be converted to noise-factor by using the formula:

$$N = \frac{\log^{-1} Nf (g)}{10}$$

In the same way, power gain ( $G$ ) can be calculated from gain ( $g$ ) as follows:

$$G = \frac{\log^{-1} (g)}{10}$$

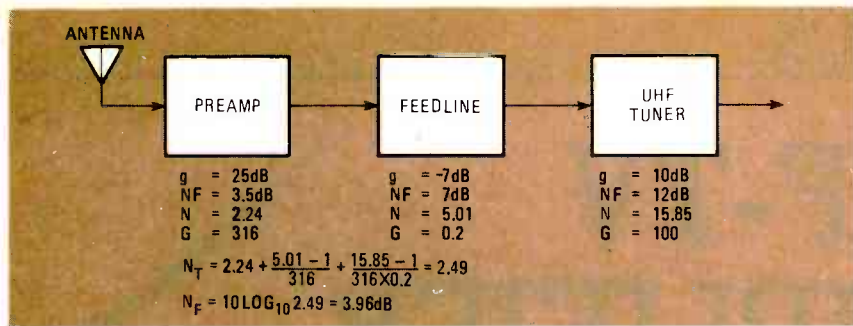


FIG. 1—PLACING A PREAMPLIFIER with a gain of 25 dB and a noise-figure of 3.5 dB at the antenna-end of a UHF receiving-system gives a total noise-figure of 3.96 dB.

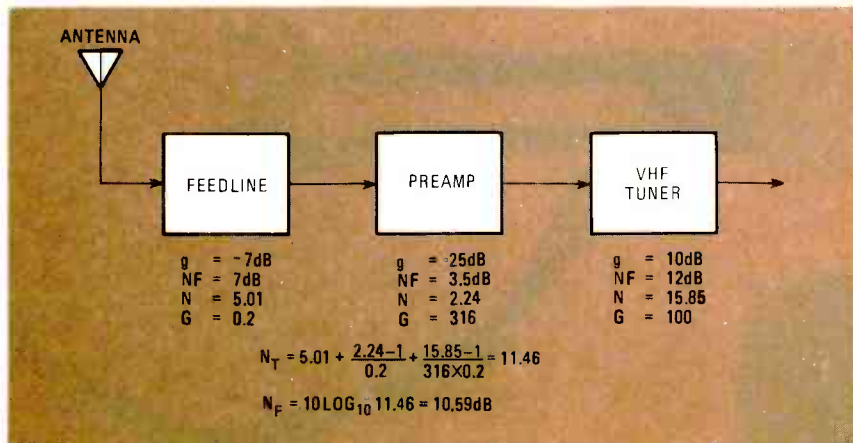


FIG. 2—PLACING THE SAME PREAMP at the receiver-end of the system increases the noise-figure to 10.59 dB.

Now that we've introduced those relationships, let's look at a model of a typical receiving system. Figure 1 shows a block diagram in which we consider the feedline to be the first stage. (That is valid in our calculations, as you will see.) Gain can be negative as well as positive; in the case of the feedline, we consider the insertion loss to be negative gain. The noise-figure of the feedline is essentially equal to the loss.

Let's see what happens when we add a preamplifier with a gain of 25 dB and a noise-figure of 3.5 dB, first at the antenna as shown in Fig. 1, then with the amplifier at the input of the receiver as in Fig. 2.

With the preamp at the antenna, the total calculated noise-figure for the three elements shown in Fig. 1 is 3.96 dB. By putting the feedline ahead of the preamplifier, as shown in Fig. 2, the noise-figure increases to 10.59 dB. As you can see, the noise-figure is improved by 6.6 dB by putting the element with the lowest noise-figure (the preamp) first. A general rule of thumb in receiver design is that each stage should have at least 10 dB more gain than the noise-figure (in dB) of the subsequent stages of the receiver. By placing the preamp first we eliminate the noise-factor and attenuation effects of the feedline, because the preamp has a gain of more than 10 dB over the losses induced by the feedline.

Another benefit of having the pre-amplifier located at the antenna is improved flatness of the transmission line's VSWR (Voltage Standing Wave Ratio); even the best antenna designs do not have a constant feedpoint impedance over their frequency range. The result is that the VSWR of the feedline varies with frequency. Two adverse effects of a high VSWR are increased losses, and reflections that degrade picture quality—especially in the case of color. With the preamp, however, it is easy to design a broadband output-circuit, thus making the match to the line better and lowering the VSWR on the longest part of the feedline. The antenna will still exhibit whatever mismatch characteristics it has, but the resulting mismatch will occur only on the portion of the line between the antenna and preamplifier. That will be of little consequence, because of the short line-length involved, and the pre-amplifier will effectively buffer the remaining feedline to the set or distribution system.

Commercially available UHF preamps have gains ranging from 12 to 22 dB with noise-figures in the range of 3 to 8 dB. (You can perform gain and noise calculations as shown above using the appropriate figures).

#### A preamp you can build

You can improve your UHF reception for less than \$35.00. The preamp

#### PARTS LIST—PREAMP

All resistors 1/8 watt, 5%

R1—82,000 ohms

R2—820 ohms

R3—39,000 ohms

R4—390 ohms

**Capacitors**

C1, C2—3.3 pF chip capacitor

C3, C4—2.7 pF chip capacitor

C5, C6—680 pF, ceramic disc

C7—0.01 μF, ceramic disc

**Semiconductors**

Q1, Q2—BFQ85 or BFR90

L1—L3—See text

L4—10 μH choke (3½ turns No. 30 wire-wrap wire through 1/8-inch ferrite bead)

J1, J2—bulkhead-mount female "F" connectors

**Miscellaneous:** Double-sided PC board (etched one side), enclosure, solder, etc.

A kit of all parts for the UHF preamp, including power supply and balun (the balun will be discussed next month), is available for \$34.50 plus \$2.00 for shipping and handling. An assembled version is available for \$47.50 plus \$2.00 for shipping and handling. Both are available from:

RaySon Electronics Corp.

1010 12th St., Suite 5

Sparks, NV 89431

Micromart

508 Central Avenue

Westfield, NJ 07090

(201) 654-6008

Quest Electronics

P.O. Box 4430

Santa Clara, CA 95054

(800) 538-8196 (except CA)

(408) 988-1640

All suppliers accept MC and Visa. Please add sales tax where applicable.

that will do the job is unusual because, for its price, it provides exceptional gain (25 dB typically) with an exceptionally low noise-figure (only 3.5 dB, maximum). Its performance exceeds that of any of the under-\$100 commercial preamps tested by the FCC. While the device is intended to be used outdoors as an antenna-mounted unit, it can also deliver reasonable performance if used indoors at the TV receiver.

Several factors contribute to its high performance, the primary one being use of two microwave-type transistors. Those devices are useful up to 1.5 GHz and have a noise-figure of less than 2 dB over the entire UHF-TV spectrum. Figure 3 shows gain vs. frequency and noise-figure vs. frequency plots for the transistors. (They are actually integrated circuits that have broadband impedance-matching networks right on the chip.) The devices have nominal input and output impedances of 75 ohms, so no tuning is required and circuits built around them are extremely stable.



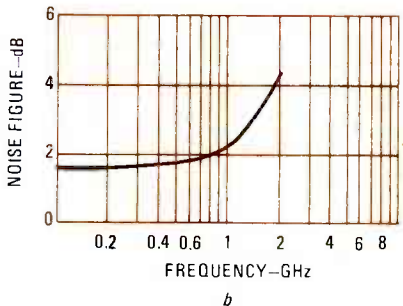
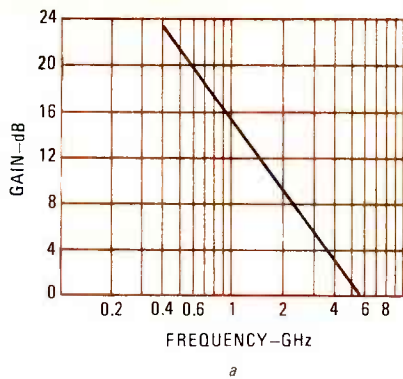


FIG. 3—TRANSISTORS USED IN PREAMP show excellent gain-vs.-frequency (a) and noise-figure-vs.-frequency (b) responses.

The second contributing factor to that preamp's performance is the PC board's design; the RF path on the board is actually a 75-ohm transmission-line section, or *stripline*. The use of stripline construction continues the 75-ohm transmission line right to the input and output terminals of the transistors, thus insuring proper impedance-matching to the devices for optimum performance. To take maximum advantage of the stripline construction, the RF coupling-capacitors are micro-wave chip-capacitors, which are designed to be integrated into the stripline with a minimum of disturbance in the line's characteristics. Stripline construction is used almost exclusively in microwave equipment and this preamp makes an ideal project for experimenters to gain experience with microwave-equipment construction techniques.

Figure 4 shows a schematic of the circuit. The input and output circuits are both 75 ohms. (Since we discussed the differences in losses between wet 300-ohm twinlead and wet 75-ohm coax earlier, there should be no doubt as to why the output cable to the TV set should be coaxial cable).

The first stage of the preamp is biased for a collector current of approximately 4 mA for the best noise-figure, and the second stage is biased for a collector current of approximately 10 mA for optimum gain. The input filter, consisting of C1, C2, and L1, is a high-pass filter that rejects anything below about 500 MHz. While that frequency falls

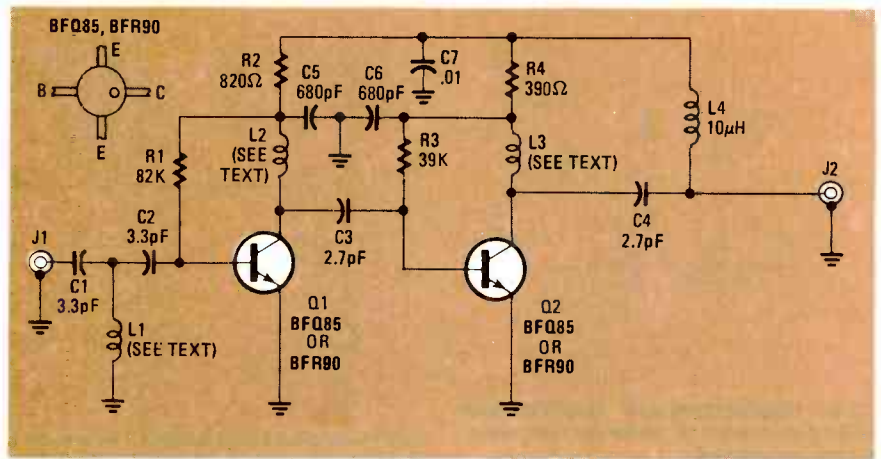


FIG. 4—FIRST STAGE OF PREAMP is biased for optimum noise-figure; second stage for optimum gain.

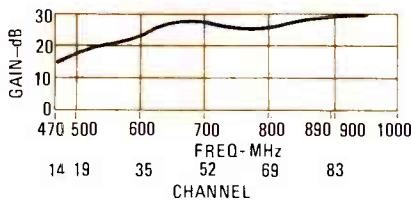


FIG. 5—HIGH-END RESPONSE of preamp is in excess of 25 dB.

around channel 20, the rolloff characteristics are sufficiently broad for the amplifier to have a gain of 15 to 18 dB at the low end of the UHF band. Considering the overall response of a typical antenna, feedline and TV tuner, the low-end rolloff of the amplifier is more than offset by the higher response of the other system components. The amplifier's frequency response is shown in Fig. 5, a normalized response-curve for three prototypes tested. It should be noted that the high-end response is better than 25 dB even at channel 70, a feature that is not found in many commercially-available amplifiers; many of them roll off sharply before channel 60.

### Preamp construction

Figure 6 is a foil pattern for the stripline preamplifier. For the stripline section to exhibit the desired characteristics, the board material must be glass-epoxy *double sided* material, 1/16-inch thick.

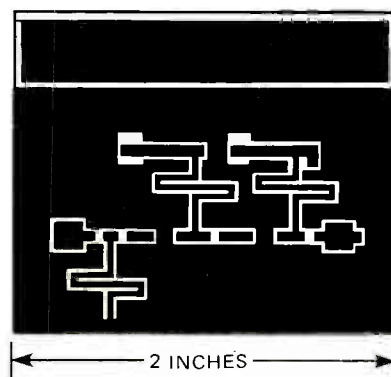


FIG. 6—PREAMP IS CONSTRUCTED on double-sided PC board, only one side of which is etched.

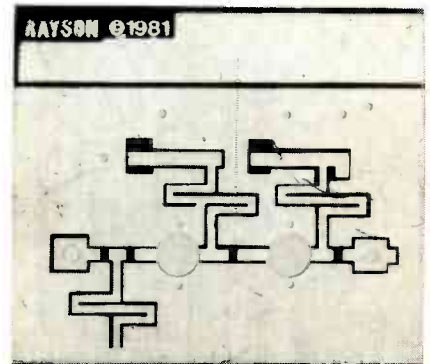


FIG. 7—BARE PC BOARD shows where holes for "F" connectors, transistors and disc capacitors are drilled.

The three elongated "S"-shaped sections are inductors L1, L2, and L3; L4 is made by winding 3½ turns of No. 30 wire-wrap wire through a small (1/8-inch) ferrite bead. The bead should be located as close to J2 as possible.

The input and output connectors are F-type connectors that are soldered to the rear (unetched side) of the board, with the center pins passing through the board directly into the stripline sections. The copper around the two center-conductor holes on the rear must be removed so the pin will not short out against it. That is easily done by hand with a 1/8-inch or larger drill bit. Apply pressure gently while twisting it in the hole—the foil will be removed and the insulating glass-epoxy board exposed. Stop there—you don't want to weaken the material. Figure 7 shows the large and small holes that have to be drilled for the jacks, transistors, and disc capacitors.

Assembly is reasonably straightforward; Fig. 8 shows the component placement. The two emitter leads on the transistors are bent at right angles just beyond the point where they narrow. The base and collector leads are cut short at the same point. The transistors are inserted into the holes in the board from its etched side with the collector lead (marked by a dot on the case) facing down and toward the out-

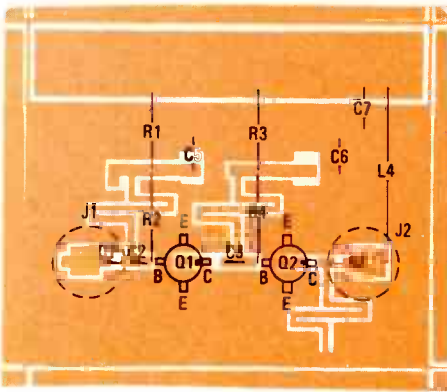


FIG. 8—TRANSISTORS ARE MOUNTED from etched side of board. "F" connectors are mounted from unetched side.

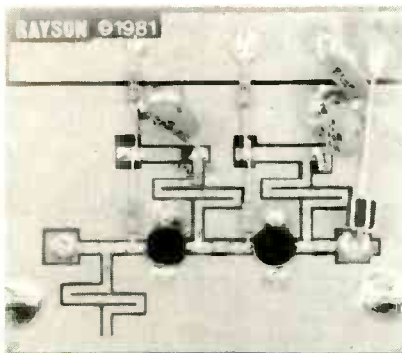


FIG. 9—MOST COMPONENTS are tack-soldered to etched side of board. Exceptions are disc capacitors, transistors, and connectors.

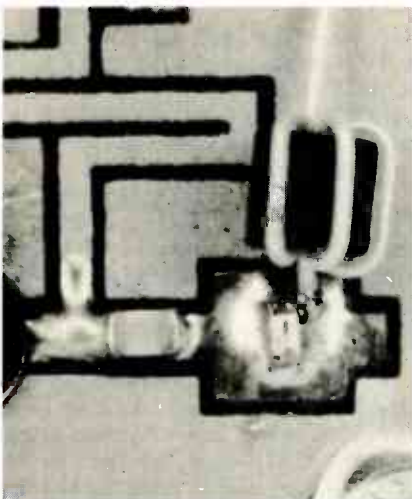


FIG. 10—CLOSE UP OF BOARD shows choke L4 and small chip capacitor to its right. See text for details on soldering chip capacitors.

put connector (J2). The emitter leads must be passed through the board and soldered on both sides of it. The other transistor-leads should lie flat against the stripline section.

While it is possible to use ¼-watt resistors, ½-watt units have been found to give better performance. Keep all leads as short as you can.

The chip capacitors have to be very carefully installed. They are extremely small and light, and the surface tension of molten solder will cause them to

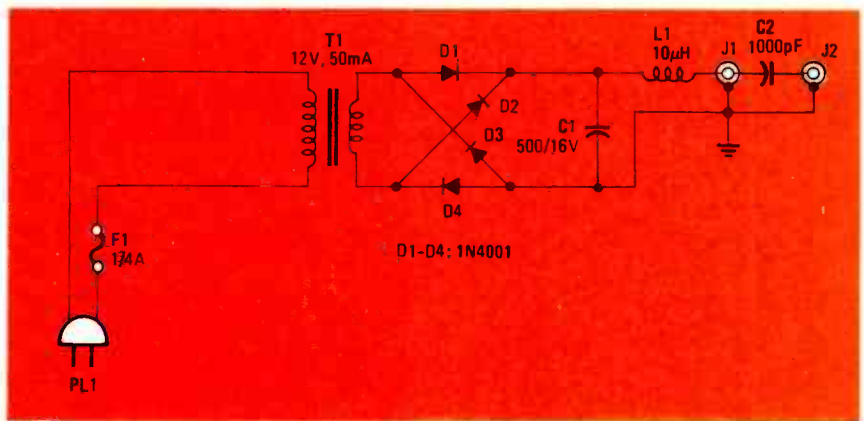


FIG. 11—SIMPLE POWER SUPPLY for preamp. If desired, an off-the-shelf 9-volt wall-plug DC supply can be used, or 12-volts taken from TV set providing it is not "hot chassis" type.

### PARTS LIST—POWER SUPPLY

#### Capacitors

- C1—500 µF, 16 volts, electrolytic
- C2—1000 pF, ceramic disc

#### Semiconductors

- D1—D4—1N4001
- L1—10 µH choke (3 ½ turns No. 30 wire-wrap wire through ⅛-inch ferrite bead)
- T1—12 volts, 50 mA or greater
- F1—¼ amp fuse

J1, J2—female "F" connectors

Miscellaneous: baluns (see text), wire, solder, etc.

stick to the tip of the iron. To mount them on the board, you should work slowly and carefully with a fine tip on the iron and fine-gauge solder. Apply a very small amount of solder to the PC board first, and then, with a pair of tweezers, carefully position one end of the capacitor against it. Heat the solder momentarily with the iron until the solder flows, and hold the capacitor in position with the tweezers while you remove the iron. That will tack one end of the capacitor to the board and then you can go ahead and solder the other end.

The two sides of the board have to be connected for best operation. That is easily done by forming two short lengths of wire (resistor leads, for example) into "U"s, slipping them onto the board with one leg of the "U" on each side of it, and soldering. The "U"s should be located as close as possible to the input and output jacks.

The circuit can be assembled in less than an hour, and once it's together, it's ready to use. The completed board is shown in Fig. 9. (Note that two of the holes shown in Fig. 7 are not used.) A close-up view of coil L4 and one of the chip capacitors is shown in Fig. 10.

Since the preamp is a broadband device, there is no tuning or alignment required. It should be mounted in an enclosure; the two coaxial connectors secure it to that enclosure. The box can be either metal or plastic, and the

preamp can be used either indoors or outdoors. Best results are obtained when the preamp is mounted right at the antenna, but in many instances, good results can still be obtained with the preamp mounted indoors near the TV set. An interesting combination for indoor use has the stripline pre-amplifier with the \$6.95 Radio Shack 15-623 antenna. Georgia Tech engineers rated that antenna as "...significantly superior to other indoor antennas evaluated."

### Power supply

The preamp requires approximately 12-volts DC for operation. The voltage is not especially critical, and the pre-amp will operate reasonably well at any voltage between 9 and 15 volts; however, the best noise-figure is attained at 12 volts. The power is run up the feed-line. Choke L4 on the preamp board prevents the output signal from flowing into the power bus, while C4 blocks the DC from being short circuited by Q2.

The preamp requires only 15 mA for operation. Figure 11 shows the circuit for a power supply that can be used to power the unit, and a means for connecting the 12-volts to the set end of the cable. J1 connects to the preamp and J2 connects to the set.

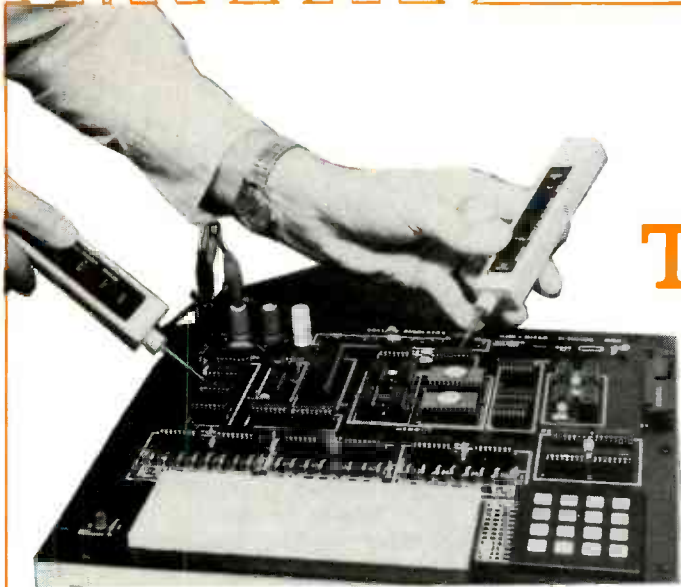
If you do not want to build your own supply, you can use a small wall-plug DC supply. A 9-volt, 100-mA supply will deliver between 12 and 14 volts when lightly loaded. Surprisingly, 200-mA supplies provided only 11 to 12 volts under the same conditions. However, either would be adequate—there is little difference in performance apparent with supply voltages between 9 and 15 volts.

If you're careful, power can also be "stolen" from the TV set itself if it is not of the hot-chassis type.

You'll need to modify a commercially available balun for use with the preamp. We'll show you how to do that, and some things to consider when selecting an antenna and feedline, when we continue this article.

R-E





## Troubleshooting DIGITAL CIRCUITS

*Troubleshooting procedures and tools for digital logic-circuits are quite different from those used in analog work. Here's an introduction to working with digital IC's.*

ROBERT L. GOODMAN

THE DIGITAL INTEGRATED-CIRCUIT HAS revolutionized the electronics industry and, in many areas, now dominates it. Because of the digital explosion, you will find more compact, complex, and powerful troubleshooting instruments and devices. Unfortunately, the digital-IC boom has given a big headache to the analog-circuit troubleshooter. Because of the fundamental differences between analog and digital circuits, the troubleshooting techniques and the types of instruments that must be used differ greatly from those required in analog work. One of the first, and most useful, tools you will encounter in troubleshooting digital-logic circuits is the logic probe.

### About logic probes

Digital logic works using two voltage levels to express either an "on" or an "off" state. "On" is usually in the neighborhood of +5 volts, and is referred to as a *logic-high* state or "1." "Off" is at or near 0 volts, and is called a *logic-low* state or "0." We'll go into more detail on the workings of digital logic later.

Logic probes quickly tell you how—or whether—a digital circuit is operating at the point being tested by indicating what logic state is present. Suppose, for example, that a test point is supposed to go to a logic-high state under certain conditions. A logic probe will indicate whether or not the line actually does go high when it's supposed to, or whether

it is, perhaps, permanently at a logic-high level.

Some probes have a memory function and can be used to monitor a line for intermittent pulses, or noise spikes ("glitches") that can upset logic-circuit operation.

Logic probes are powerful troubleshooting tools because of their portability, low price, and simple operation.

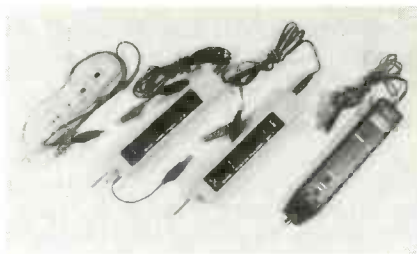


FIG. 1—SOME OF THE logic probes and pulsers used for digital troubleshooting.

Most logic probes provide the following features:

- High or low pulse-indication
- Pulse-train indication
- Stretching capability for short pulses
- 10 nanosecond pulse-response
- Pulse memory
- Undefined logic-state indication
- Ability to test different logic-families

Figure 1 shows a few of the various logic probes that are available. From left to right they are the Global Specialties Corp. model *LP-1* and *LP-2* logic probes, the *DP-1* pulser, and B&K-Precision's model *DP-50* logic probe.

### Using a logic probe

Logic probes indicate logic states with lamps or LED's. Some use colored LED's in various patterns to show logic states. The LED's show whether a logic state is high, low, or alternating (pulsing); or whether an open circuit exists.



FIG. 2—GLOBAL SPECIALTIES' *LP-2* logic probe, like most others, derives its power from the circuit under test through clip leads (top).

The Global Specialties *LP-2* logic probe shown in Fig. 2 is protected against over-voltage and reverse voltage that might be applied to its power leads. To use the probe, connect its black-clip lead to the power-supply common (–) and the red-clip lead to  $V_{cc}$  of the system under test. In order to minimize the possibility of power-supply spikes or other spurious signals

from affecting the operation of the probe, connect the power leads as close to the point being tested as possible.

The B&K-Precision DP-50 digital probe (shown in Fig. 3) is designed for quick analysis of digital circuits, and is compatible with TTL, DTL, RTL, CMOS and high-noise-immunity logic. Three LED's at the probe-tip indicate the presence of digital pulses, and high and low logic-states. Two switches allow you to select TTL or CMOS logic-thresholds, and PULSE STRETCH or MEMORY modes. In the PULSE STRETCH mode, short-duration pulses are stretched for a clear visual indication. In the MEMORY mode, a single digital pulse will cause an LED to remain lit until the memory circuit is reset. The probe thus has the ability to "freeze" an indication of digital-logic action.

### Pulse stretching

Probably one of the most important features of a logic probe is its ability to "stretch" a 10-nanosecond (ten-billionths of a second) pulse to 100 milliseconds so that the LED will stay illuminated long enough to be observed. That pulse stretching is accomplished by using the leading edge of the short pulse detected to trigger a flip-flop whose time delay is 100 ms. Single pulses flash the probe's LED's once, while trains of pulses will usually cause them to blink at a 10-Hz rate, regardless of pulse-frequency. Generally, just knowing that pulse activity is present is enough. (If the pulse-frequency is important, use a frequency counter or oscilloscope.)

### Digital vs. analog troubleshooting

When troubleshooting circuits containing analog devices, you usually need only test resistance, capacitance, or voltages. The total circuit may be quite complex, but each component in the circuit performs a simple task and its operation can usually be checked out easily. If necessary, each resistor, capacitor, diode, and transistor can be tested individually by using a signal generator, VTVM or DMM, diode checker, or scope, together with conventional troubleshooting techniques. With integrated circuits, though, it is impossible to check the individual components on the chip; you must troubleshoot the device as a whole.

A significant difference between circuitry made up of discrete components and digital IC's lies in the complexity of the functions performed by the latter. Instead of measuring simple characteristics, you need to observe complex and rapidly occurring digital signals and to determine whether they're correct.

Verifying proper digital-IC operation requires observing several inputs while simultaneously observing two or more outputs. Thus another difference between analog circuitry built from discrete components and digital IC's is the



FIG. 3—SWITCH-SELECTABLE threshold levels (TTL/CMOS) are common on logic probes such as B&K-Precision's DP-50.

number of inputs and outputs for each component and the need to check them simultaneously.

Digital IC's contain many complex circuits. Should any portion of such an IC fail, it would be difficult to pinpoint the area of failure—and impossible to repair or replace it (you can rebuild picture tubes, but not IC's). Consequently, to troubleshoot circuits made up of digital IC's involves locating not a portion of an IC that's gone bad, but, rather, just the IC itself. Replacing it usually restores the circuit to working order.

For effective troubleshooting of digital circuits, it is necessary to take advantage of the digital nature of the signals involved. Tests and techniques to troubleshoot analog circuits do not do that and are inefficient when used for digital circuits.

### TTL logic-signals

A typical TTL (Transistor-Transistor Logic—the most common digital-logic family) logic signal is shown in Fig. 4. The appearance of a similar pulse-train on the screen of an oscilloscope is shown in Fig. 5. The scope displays voltage with respect to time, but for digital pulses, exact values are not important. A digital signal exists in one of two or three states—high, low, or undefined (in-between states)—each determined by a threshold voltage. It is the value of the signal voltage *with respect*

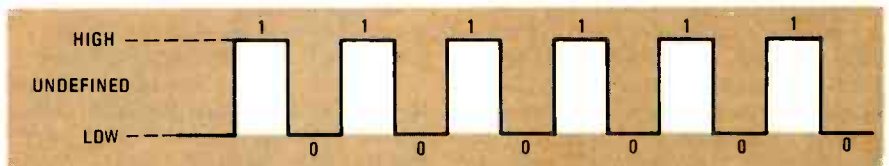


FIG. 4—TRAIN OF DIGITAL PULSES consists of a square wave whose values alternate between (approximately) 5-volts and 0-volts.

to those thresholds that determines the logic-state of a digital signal.

As Fig. 6 shows, if the signal level is greater than 2.4 volts, it is considered to be a logic "high." For a logic "low" the voltage must be below 0.8 volts. The precise value is not important as long as it is above or below the threshold, and not in the "undefined" area. When using a scope, you must always determine whether the signal meets the threshold requirement for the desired digital state; a logic probe will tell you that.

Each gate in a TTL logic family has a certain propagation-delay time, rise time, and fall time. Those times rarely change, so scope checks of timing parameters contribute very little to the troubleshooting process.

The circuit in Fig. 7, showing a simple TTL totem-pole device (the output transistors are "stacked" like a totem pole, hence the name), illustrates a problem created by the TTL logic-family. In either state—high or low—it has a low output-impedance. In the low state that is about 5 or 10 ohms to ground.

That presents a problem for in-circuit pulse injection (used to determine how the device is operating by "force-feeding" it a pulse). A device used to inject a pulse at a point that is driven by a TTL output must have sufficient power to override the low-impedance output state. Most signal sources used for troubleshooting do not have that capability. Thus the troubleshooter is forced either to cut the printed-circuit runs or lift IC leads in order to pulse the circuit to be tested; that is time consuming and also can damage other circuits.

For those reasons a scope and traditional signal-sources are not very useful. And, since many diodes and transistors are packaged in the IC, diode checkers are largely useless. With the complexity of today's electronic circuits, it makes good sense to find the most efficient troubleshooting method. In most cases, oscilloscopes, diode checkers, and voltmeters are best suited for use with analog circuits, where they really shine. Special-purpose equipment, such as logic probes and pulsers (see below), should be used when working on digital equipment.

Logic probes provide a quick way not only to detect, but also locate, breaks in a PC run. Since an open signal-path may allow IC inputs at the break to "float" to an undefined state, a logic probe can be used to test the input of each IC for such a state. Once a floating input is detected, the logic



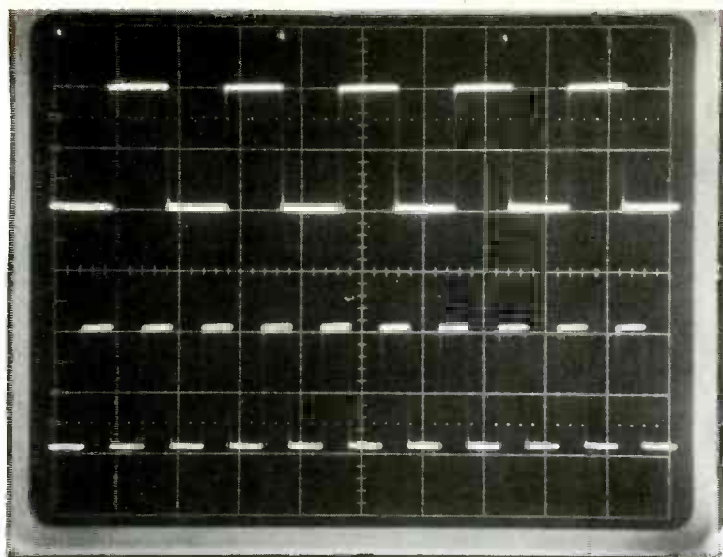


FIG. 5—DUAL-TRACE SCOPE shows two trains of pulses. Vertical lines in square wave are nearly invisible because transition between states is extremely fast.

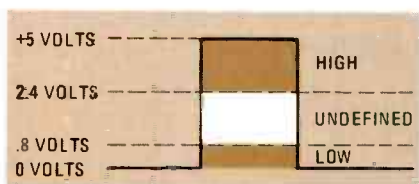


FIG. 6—VOLTAGE THRESHOLDS determining logic states. Contrary to popular belief, a logic "high" is not always 5-volts.

in the internal circuitry (often called the steering circuitry) of the IC.

In addition to those four internal failures, there are four types of faults that can take place in the circuitry external to the IC. They are: (1) a short between a signal path and  $V_{CC}$  or ground, (2) a short between signal paths, (3) an open signal path, and (4) a failure of an

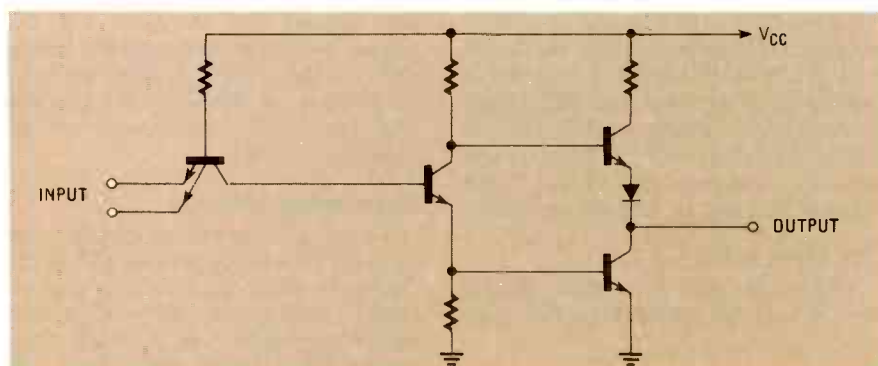


FIG. 7—TWO-INPUT NAND GATE. Totem-pole configuration at output results in low impedance, making some conventional tests difficult to perform.

probe can be used to follow the circuit back from the input searching for the break. That can be done because the circuit before the break will show valid logic levels (either high, low, or pulsing) while the circuit after the break will probably show undefined levels.

#### IC failures

To troubleshoot digital-IC circuits, it is important to know what types of faults to expect. They can be divided into two main classes—those caused by failures inside the IC, and those caused by circuit failures outside the IC.

There are four types of internal IC-failure: (1) an open bond at either an input or output, (2) a short between an input or output and  $V_{CC}$  or ground, (3) a short between two pins, and (4) a failure

analog component, such as a resistor, capacitor, or semiconductor device.

#### Logic pulsers

Logic pulsers inject a single pulse of the proper amplitude and polarity into a circuit. If a point was at a logic-"low," it will automatically be pulsed high, and if it was high it will be pulsed low. Pulsers are useful for forcing the inputs of digital IC's to change state so that the resulting outputs can be observed. Pulsers have a high current-output, but use a low duty-cycle to protect the IC's from damage.

In their many applications, digital IC's have certainly made our lives easier. Knowing how they work and how to troubleshoot them should make *your* life easier, too.

R-E

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## ALL ABOUT PULSE GENERATORS



Once found only in sophisticated design labs, the tremendous growth in the use of digital circuits and devices has made the pulse generator a valuable instrument for any service shop or experimenter's workbench.

CHARLES GILMORE

NOT TOO LONG AGO THERE WERE FEW pulse generators outside of sophisticated design laboratories. Today, they are found in service shops, on experimenters' benches, and anywhere else that electronics testing is done. Two factors have influenced the wider use of those instruments: need and lower prices. The dramatic growth in the use of logic circuits caused the need; the price-drop soon followed, and pulse generators are now truly low-cost signal sources.

Not long ago, few pulse generators were available for under \$1000. Now, there are many available for under \$400. Although many sophisticated, and expensive, pulse generators are still available, the lower-priced units have enough features to make them extremely useful.

Currently, the need for a pulse generator arises mostly from the extensive use of many different varieties of digital logic in industrial, laboratory, and consumer applications (although a pulse generator is also useful when working with analog circuits). It is not possible to service or design logic-based electronic systems using only a sine-wave generator or a square-wave generator. A sine-wave generator or square-wave generator cannot vary the pulse width of its output signal; it also cannot generate a wide enough range of frequencies. In addition, frequently the output impedance of a sine-wave generator or a square-wave generator is not low enough to drive logic circuits.

A more elaborate function generator with DC offset, variable symmetry control, and a wide frequency range may fulfill the need for a pulse generator

partially, if the requirements are simple. When extensive use of logic circuits is involved, however, a function generator is not adequate. Function generators cannot produce pulses of less than 5% duty cycle, and low-cost or reasonably priced units do not provide the 10-MHz to 20-MHz capability required of pulse generators used with TTL (Transistor-Transistor Logic) or ECL (Emitter-Coupled Logic) systems. Of course, the function generator contains many other features that may or may not be needed.

### The basic pulse

Before discussing the pulse generator, it may help to review the basic

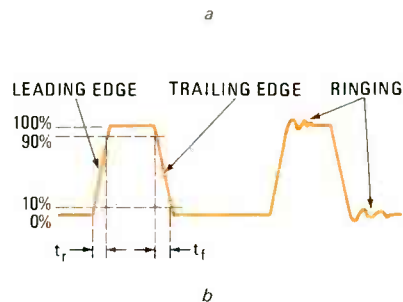
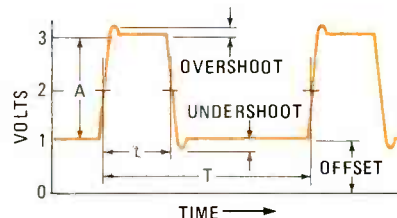


FIG. 1—THE TIMING AND AMPLITUDE relationships of a basic pulse are shown in a. A pulse with exaggerated leading and trailing edges is shown in b.

characteristics of a pulse. Figure 1 shows the basic timing and amplitude relationships of a pulse. In Fig. 1-a, the period between the start of each pulse is a length of time,  $T$ , that is considerably greater than the pulse width,  $t$ . Figure 1-b shows exaggerated leading and trailing edges to illustrate such parameters as rise-time and fall-time. The basic pulse parameters are explained in Table 1.

### Basic pulse generator

Figure 2 shows a simplified block diagram of a pulse generator. The circuitry for each block is fairly conventional. Numerous outputs, special buffer amplifiers, and power supplies can be added to each stage to reach the level of sophistication needed for a particular application.

The basic pulse repetition rate is controlled by the *repetition-rate generator*—a free-running astable multivibrator capable of covering the frequency range required by the pulse generator.

Pulse generators offer a switch-selected alternate source for rate generation called the *external trigger*. Signals applied to the external trigger input pass through triggering circuitry much like that found in an oscilloscope. Those circuits establish the triggering amplitude and polarity. Additional inputs to the trigger amplifier may include a line-frequency source and a manual pushbutton for one-shot operation.

A second external amplifier can be used to gate the main repetition-rate generator in a manner similar to the gated mode of function generators. Signals from the gating amplifier permit



TABLE 1

**Pulse period**—pulse period  $T$  is the time between two pulses. It is measured between either the leading or trailing edges.

**Repetition rate**—indicates the number of pulses over a fixed period of time, usually 1 second. The repetition rate depends on the pulse period  $T$ : Repetition rate =  $1/T$ .

**Pulse width**—the time between the 50% amplitude points of any single pulse is defined as the pulse width  $t$ .

**Pulse amplitude**—pulse amplitude  $A$  is the voltage to which the pulse rises above its own baseline, measured after any overshoot has been reduced to zero.

**Pulse offset**—the value and polarity of the difference between the pulse baseline and 0 volts.

**Overshoot**—that portion of a pulse at the end of the leading edge, where the leading edge extends above the normal pulse amplitude. Overshoot is usually expressed as a percent of total amplitude.

**Undershoot**—that portion at the end of the trailing edge where the trailing edge extends below the baseline. That is usually expressed as a percent of pulse amplitude.

**Leading edge**—the portion of the pulse where a negative-to-positive transition occurs.

**Trailing edge**—that portion of the pulse in which the positive-to-negative transition occurs.

**Rise time**—the time required for the pulse to pass from 10% of total amplitude to 90% of total amplitude ( $T_r$ ).

**Fall time**—the time required at the trailing edge for the pulse to pass from 90% of full amplitude to 10% of full amplitude ( $T_f$ ). Rise time and fall time are not necessarily equal.

**Ringling**—damped oscillation at the end of the leading or trailing edge of the pulse.

**Duty cycle**—the ratio of pulse width to the pulse period, expressed in percent. Sometimes that is referred to as the duty factor.

**Pulse polarity**—indicates whether the desired pulse extends positively or negatively with respect to the baseline. Pulse polarity is independent of the absolute DC-value of the baseline.

the repetition-rate generator to output pulses only when a gating signal is applied; otherwise no pulses are generated. A burst of pulses can be produced in that mode.

Signals from the repetition-rate generator or from the trigger circuits are applied to the delay generator (if the pulse generator has one). The delay generator is a wide-range monostable multivibrator.

Once the delay generator has completed its cycle, the main pulse generator is triggered. The pulse generator is also a monostable multivibrator with a wide dynamic range to generate the necessary pulse widths. That monostable multivibrator can be quite sophisticated.

It must cover an extremely wide range of pulse widths (typically 7 to 8 decades) and operate at fairly high duty-cycles. Some generators need to operate at duty cycles that are greater than 100%. The output stages of the monostable multivibrator may include independent charge and discharge switches so that independently variable rate times and fall times can be generated. That feature is usually found only on more expensive pulse generators.

The output of the monostable multivibrator is applied to one or two output amplifiers. Those amplifiers must be DC-coupled, variable-gain wideband amplifiers. On more sophisticated generators, where extremely close control

of pulse characteristics is desired, two amplifiers are used. One of the amplifiers handles the positive pulses; the other handles the negative pulses. In that manner, each amplifier can be tailored to its particular function. In other pulse generators, a single amplifier is used. In either case, extremely wide-band amplifiers must be used to reproduce faithfully pulses whose rise times lie in the nanosecond range, without ringing or other aberrations.

Pulse amplitude is usually regulated solely by a variable-gain control that is part of the output amplifier. A few of the higher-priced pulse generators include a step attenuator at the output. As the output amplifier is DC-coupled, a DC offset signal can be applied to the amplifier, along with the pulses, so that the pulse baseline can be changed with reference to 0 volts. Normally, the offset voltage is unaffected by adjustments of the continuously variable output attenuator.

Pulse generators that include a delay-generator frequently have a specialized mode referred to as a double- or twin-pulse mode. In a double-pulse mode, the main pulse generator is triggered not only by the delay-generator output, but also by the signal directly, at the same time that the signal triggers the delay generator. The result is two pulses, the first, generated at the time of triggering, and the second, at the time the delay generator has completed its cycle.

There are many special applications that require a capability other than those offered by a standard pulse-generator. For such applications, certain portions of the basic pulse generator can be adapted to accommodate those special requirements.

**Word generators**

The word generator is one of those specialized versions. Its function is to generate a series of pulses that form a serial digital word. Usually, those generators are operated in either a one-shot or a repetitive mode. The pulse-generator circuitry (a simple monostable multivibrator) is replaced by a more sophisticated circuit that is capable of producing a series of pulses. Usually 8, 16, or 32 pulses-per-trigger-signal are produced.

**High-speed pulse generators**

Two types of pulse generators fall into the high-speed category. Pulse generators whose repetition rates are in the 100-MHz to 250-MHz range are designed especially for working with extremely high-speed ECL circuitry.

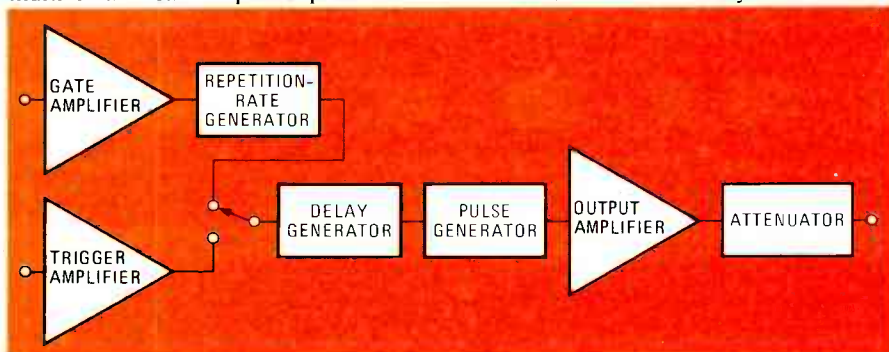


FIG. 2—SIMPLIFIED BLOCK DIAGRAM of a basic pulse generator is shown here. Many outputs, special buffer amplifiers, and power supplies can be added to each stage to make a more sophisticated instrument.

They are particularly useful when designing or servicing complicated portions of high-speed computers and some instruments. Because of their high repetition rates, high-speed pulse generators require that all circuitry within the pulse generator perform many times better than the circuitry of a conventional pulse generator.

Pulse generators may also be required to produce pulses with extremely fast rise-times. The conventional pulse generator has typical rise times in the range of 5 to 7 nanoseconds. Rise times that are measured in hundreds of picoseconds are available with specialized pulse-generators. Pulse generators with those fast rise times generally do not have variable rise-time and fall-time capability.

### Pulse-burst mode

The pulse-burst option permits you to select the number of pulses that are generated when a trigger signal is received. That mode differs from the word generator in that the logic state of each pulse is not controlled individually. However, you can trigger from 1 to 10,000 pulses in a single burst. The pulse-burst mode is particularly convenient when you are working with counters or other circuits where response to the wave-shape and repetition rate, as well as to a particular number of pulses, is important.

### High-voltage generators

High-voltage outputs on pulse generators are becoming less and less common. However, pulse generators designed for certain communications, biological, or physiological applications, and those to be used with tube-type circuits, may have very high voltage-signals. Usually, such pulse generators are severely limited in terms of rise time, pulse-repetition rate, and output impedance.

### Pulse-repetition rate

The controls that vary the pulse-repetition rate on most generators consist of a decade switch combined with a continuously variable control. Repetition-rate specifications include the minimum and maximum frequency capability, and the number of decades involved. Maximum repetition rates of 10 to 20 MHz are typical of low-cost generators. A few of those generators have maximum repetition rates that extend to 50 MHz. The minimum repetition rates of pulse generators vary widely. Some low-cost generators can have a minimum repetition rate of as little as 0.1 Hz, while others have minimum repetition rates that are as high as 10 Hz.

The selection of a repetition rate must be made with the application in mind. If the generator is to be used for

TTL or ECL logic analysis or servicing, a maximum repetition rate of at least 10 MHz is a must; 20 MHz is certainly more desirable. Minimum repetition rates are not tied to any particular logic-family type, but depend on the application. For most applications, a minimum repetition rate of 5 to 10 Hz is sufficient. For special applications, however, lower repetition rates may be needed. Extremely low repetition rates can be obtained by triggering the pulse generator from an external low-frequency source, such as a function generator.

The repetition-rate specification is not always given as the frequency. Some manufacturers list it as a repetition rate or frequency; others supply the information as a pulse period or time specification. The conversion between pulse period  $T$  and frequency  $f$  is easily made by the relationship:

$$T = 1/f$$

Repetition-rate accuracy is rarely specified on low-cost pulse generators. Where it is specified, it is indicated as a percentage of the maximum range. The accuracy of the repetition-rate setting is very unreliable, and whenever an accurate pulse-repetition rate is needed, it should be obtained either by triggering the pulse generator from a known frequency source, such as a signal generator, or by measuring the repetition rate at the trigger output, using a digital frequency meter or oscilloscope. Extremely low repetition rates may require using a digital period meter.

Repetition-rate jitter refers to the consistency of the period from one set of pulses to another. Jitter is caused by noise in the pulse-repetition-rate generator, and is specified as a percentage of the repetition rate or period. Although not specified on many low-cost pulse generators, repetition-rate jitter is typically 0.1% to 0.5%. That specification may include a fixed minimum amount of jitter in addition to the percentage of repetition-rate setting. Repetition-rate jitter does not decrease dramatically with the increased price of a generator.

### Pulse characteristics

The most important pulse characteristic in most applications is the pulse-width range, which is usually controlled in the same way as a repetition-rate generator—that is, in decade steps with a continuously variable control covering the range between each step. Pulse-width controls frequently do not have accuracy specifications, and when such specifications are given, an accuracy of pulse-width settings on the order of 10% to 15% can be expected. Once again, like the pulse-repetition rate, the pulse width must be closely monitored by a digital period-meter, or by an oscilloscope, to achieve more precise settings. Pulse-width characteristics of generators cover a

fairly wide range.

The narrowest pulse obtainable varies between 10 and 15 nanoseconds. Almost all low-cost generators have the same minimum pulse width but the maximum pulse width varies widely from manufacturer to manufacturer. Typically, the maximum pulse width varies from 10 milliseconds to 10 seconds. In most cases, narrow pulses are needed, and generators that produce pulses with minimum widths of 10 to 15 nanoseconds are suitable for use in most TTL (and some ECL) systems. For most general applications, a pulse generator is suitable if it can generate pulses with widths of at least 100 milliseconds. Pulses that are wider than that (from 100 milliseconds to 10 seconds) may be convenient for certain applications, but in general, they are not widely used.

Some manufacturers provide a pulse-width jitter specification that is fairly similar to that of the pulse-repetition rate, and indicates the maximum variation in width from pulse to pulse that can be expected. Pulse-width jitter specifications normally range from 0.1% to 0.5%.

Pulse rise-time is an important specification. To be suitable for high-speed logic operation, pulse rise times and fall times must be less than 10 nanoseconds, with 5 to 7 nanoseconds being a typical specification.

The maximum duty cycle is usually listed as a pulse specification. Most pulse generators are limited to duty cycles of 70%. Some special-purpose pulse generators offer duty cycles of up to 100%. The maximum duty cycle usually decreases at the high repetition-rate settings.

Leading-edge and trailing-edge overshoot and undershoot are specified as a percentage of the maximum permissible output-amplitude. Those, like many other specifications, are only valid when the pulse generator output is terminated into its characteristic impedance.

### Delay generator

Specifications for a delay generator are nearly similar to those for the main pulse generator. That is, they specify delay width, although the range of that width is usually much more limited than that of the main pulse generator itself. Jitter specifications can also be applied to the delay generator. Adjustments to the delay generator's operating parameters are made the same way as those that are made for the main-pulse generator. The controls for both parameters (pulse width and jitter) are not interactive.

Next month, we'll continue our look at pulse-generator characteristics, and begin to look at some applications for those devices.

R-E



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# HOBBY CORNER

## Put that old calculator to good use

EARL "DOC" SAVAGE, K4SDS, HOBBY EDITOR

HOW WOULD YOU LIKE TO OWN, FOR only \$30, a digital capacitance meter that will measure from a few picofarads to the largest value you are likely to encounter? Or, for the same price, a digital ohmmeter with an upper range that you can measure well into the multi-megohms? How about a digital stopwatch/timer, a shutter-speed tester, a tachometer, a light meter, or a speedometer?

Some of those devices sound all but impossible for the price. You probably wouldn't believe it if I told you that you could have all of them for about \$30 total! Well, believe it because it's true. Let's see how you can do it.

First of all, I'm allowing \$10 to buy a basic "four-banger" calculator. Even if you go out and buy a new one, that's more than enough money. When I started looking recently, I found five of the little things scattered around my home. You probably have several, yourself. Further, I saw an ad offering six manufacturers' rejects for one buck.

The only absolute restriction on the type of calculator is that it must have a "constant add" function: that is, each consecutive time the EQUALS key is pressed, the total is increased by one of the earlier entered digits (probably the last one entered).

Also, it is desirable that the calculator have a fast internal clock oscillator. That is more likely to be found in the cheaper models. The faster the clock, the shorter are the intervals between calculations.

Back to the cost, five dollars is allowed for the purchase of a few common capacitors, resistors, and switches. Of course, you'll only need the full \$5 in the unlikely event that you don't even own a junk box.

The final \$15 of your allotment will have to be spent. It is for a nifty little RC-111 module from Kaltek (Box 7462, Rochester, NY 14615). This amazing device measures approx.  $\frac{3}{4} \times \frac{3}{4} \times \frac{3}{8}$  inch, and it makes the whole thing possible. The RC-111, plus a very few additional components will convert your four-banger into any of the instruments listed above plus a few others. Because of the small size and parts count, often everything will fit right into the calculator case.

Of course, you *can* build separate instruments, but with suitable switching or plug-in arrangements, you can have a multi-purpose instrument. And, by the way, whatever you build, the calculator will still have its original functions. Here's how the RC-111 does its magic.

Before I start, though, let me say that the manual that comes with the RC-111 is quite complete. It gives plenty of diagrams and information for building the instruments. If I miss a point in this brief account, you can bet that the manual didn't.

Two of the eight pins on the module are connected to the calculator (or other) battery. It will operate on any voltage from 3- to 15-volts DC, and that range takes in the battery voltage of almost all calculators.

Two of the module pins are connected across the constant add key of the calculator. That is usually the one marked "=", but all you have to do is to punch a little addition problem to determine which it is on yours.

Let's look at a simple circuit application for the RC-111, and then a few variations. Figure 1 is about as simple as they come. It is a timer or stopwatch. As you can see, the  $\pm$  and D/K pins are connected to the calculator battery and key, respectively.

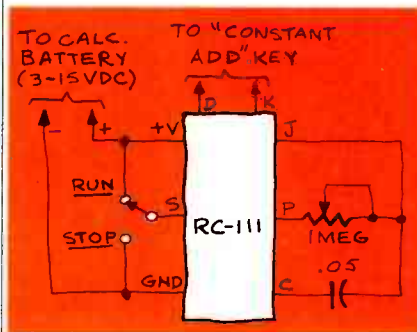


FIG. 1

The capacitor and pot connected to pins J, P, and C are adjusted to give a count rate appropriate to any given use. For the present application, you will want to adjust the rate to an interval of 1, 0.1, or 0.01 second. In fact, you can increase the accuracy to maximum (decrease the interval to minimum) by making the rate just as fast as the cal-

culator will count—that's why the internal clock rate of the calculator can become important.

The switch can be of the push, slide, or toggle variety as you prefer. When pin S is positive, the RC-111 counts; when negative, it stops. All you have to do is enter "1" or "1 + 1", depending upon the calculator model, then operate the switch during the period to be timed. The readout shows units, tenths, or hundredths of seconds. Note that you will have to subtract one from the readout if you use a "1+1" calculator, but most of us can do that in our heads!

A .05 µF polystyrene-type capacitor located at pin C will provide very good accuracy. For the highest accuracy, you can eliminate the capacitor and pot, and feed pulses from a crystal timebase oscillator into pin J.

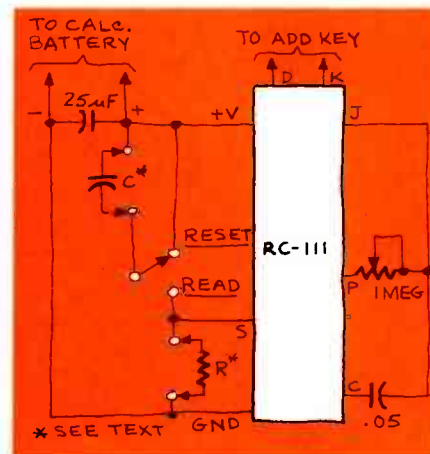


FIG. 2

There you have a neat and simple timer. If you keep in mind the functioning of pin S, the circuit in Fig. 2 is easy to understand. With the switch in the RESET position, pin S is negative and nothing happens. When placed in the READ position, pin S goes positive and the calculator counts until capacitor C charges. At that time, pin S goes low, the counting stops, and the time can be read from the display.

Now, you don't care how many tenths or hundredths of a second it takes a capacitor to charge. What you *do* want to know is the value of the capacitor in micro- or picofarads. That's easy to arrange: Just adjust resistor R, or the

*continued on page 72*



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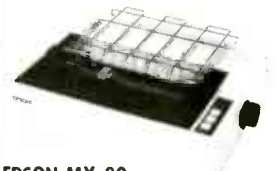
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### HOBBY CORNER

continued from page 70

capacitor connected to pin C, or the pot connected to pin P, so the calculator counts in microfarads or picofarads! Of course, you do that by using a known capacitor for C to calibrate your capacitance meter.

You are probably way ahead of me—yes, the circuit in Fig. 2 is also an ohmmeter. Using a known capacitor C, the readout can be calibrated in the same manner as before to show the value of resistor R. The reading can be in ohms, kilohms, or megohms, depending upon your calibration scale.

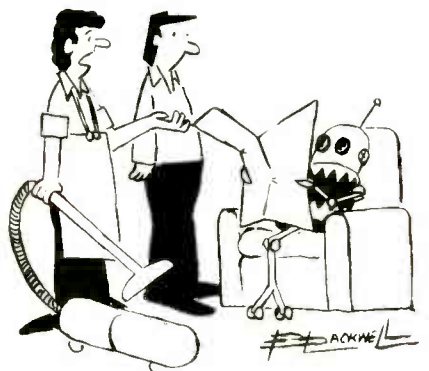
Now you are well on your way. By controlling the module rate and the on-time with the polarity of pin S, you can measure all kinds of things. As you see, there is no problem in adjusting the module rate to your needs.

Pin S can be "switched" from minus to plus in a variety of ways. Two are shown in the examples above. Of course, a transistor switch can be used. Another way is with a magnetically operated reed switch. Then, too, the common photocell and the photo-transistor can be used to change the potential on pin S.

By using different switching methods on pin S, and having the actual switching controlled by various actions, you can have any of the instruments mentioned earlier. For example, you can see that a magnet on a bike wheel activating a reed switch will count the rotations of the wheel and you can calibrate that into miles-per-hour, feet-per-minute, or whatever strikes your fancy. Several of those applications are illustrated in the *RC-111* manual.

It should be obvious to you at this point that an old calculator and an *RC-111* module can team up to do a variety of jobs. If you come up with any unusual applications, I would be glad to hear of them.

R-E



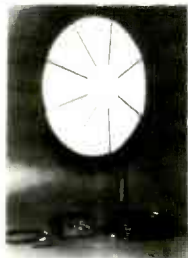
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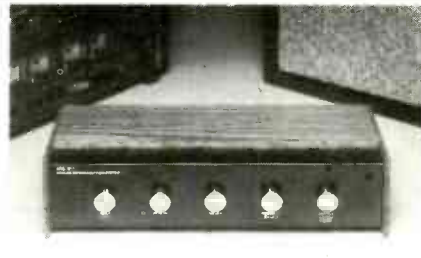
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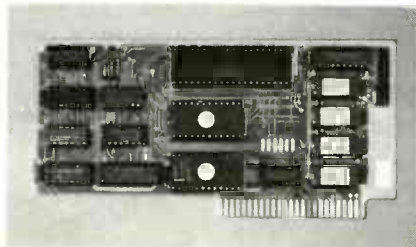
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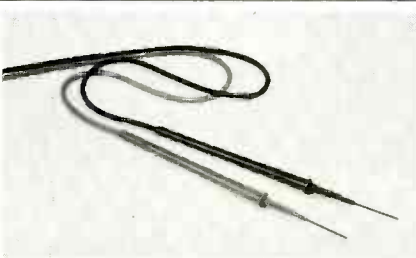
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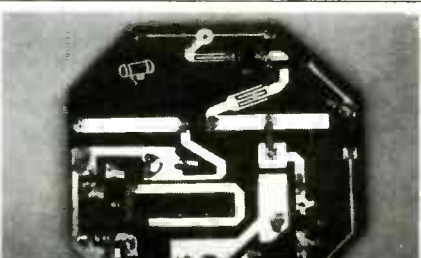
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# COMMUNICATIONS CORNER

## Speech-scrambling techniques

HERB FRIEDMAN, COMMUNICATIONS EDITOR

ONE OF THE REAL THRILLS OF SHORT-wave listening is hearing the news before it's seen on TV or the headlines of the major newspapers (whatever "major" is supposed to imply). I can remember using a surplus BC-348 receiver to "read the mail" on the overseas phone circuits and government transmitters, and "astounding" my friends and family when I told them of some new war or scandal that hadn't yet made the local papers or the "on-the-hour" newscast of the local radio stations. Today, it's somewhat more difficult to get the facts first-hand because much of what you'd like to know about is sent by radio teletype—called RTTY—or scrambled radio telephone, but it is still possible to monitor many of those transmissions.

To monitor RTTY you need to know the operating times and frequencies of the various transmissions; and if you don't want to spend most of your time fiddling with the dials, you also need to know the station's baud rate (speed of transmission) and shift frequency. I could take up this whole issue of **Radio-Electronics** and still not give you enough information to get any enjoyment out of RTTY.

A better introduction to RTTY is an excellent handbook that I recently received in the mail: *World Press Services Frequencies*. That little gem is not only a handbook on how RTTY works, and the equipment that you'll need to receive it; it also lists the frequencies, times, baud rates, shift frequencies, etc. of the commercial press services such as UPI, XINHUA (China), Reuters, Tass (Russia), and so forth. It's a thorough job and the work was obviously a time consuming labor of love by the author, Thomas Harrington, W8OMV.

Just keep in mind that while there's no law to stop you from reading the mail, you cannot divulge anything you hear to another party. The book is priced at \$5.95 and is published by Universal Electronics, Inc.; they are located at 1280 Aida Drive, Reynoldsburg, OH 43068.

### Scrambled communications

Not all scrambled communications systems use sophisticated computer circuits, and many of the ones that don't can be easily monitored. That is particularly true of some of the systems that are commonly used on the UHF

frequencies.

Among the earliest, and still effective means of scrambling communications so that the "average" SWL (ShortWave Listener) cannot monitor them is speech inversion. That system makes a transmitted signal sound like the "Donald Duck" chatter of SSB. In speech inversion, all that is done is to mix the voice frequencies and a steady carrier in a ring modulator.

To get a better idea of how speech inversion works, let's look at a simplified example. Assume that the voice frequencies are 300-2500 Hz, and that the carrier is 3000 Hz, as shown in Fig. 1-a. When the voice signal and the carrier are mixed in a ring modulator, what comes out is the sum and difference frequencies. (A ring modulator is a balanced modulator. A four-quadrant multiplier IC can be used as a ring modulator.) When the sum is removed, you are left with the difference, which is an exact inversion of the original speech frequencies. When the speech is inverted, 300 Hz becomes 2700 Hz, and 2500 Hz becomes 500 Hz, as shown in Fig. 1-b. Anyone monitoring a signal that has been inverted in that manner will hear "garbage."

At the receiver, the scrambled signal is decoded by once again mixing the signal with a carrier in a ring modulator. That will re-invert the signal. If the carrier is 3000 Hz as before, the original 300-2500-Hz input signal is recovered, as shown in Fig. 2. One problem with that scrambling system is that if someone assumes that the transmission is SSB and adjusts the BFO to "tune in" the signal, he may be able to decode the scrambling since one BFO setting will re-invert the signal in exactly the same manner as is done by the descrambler or decoder.

Several years ago, before the "age of the microprocessor," I experimented with an "unbreakable" scrambler. (At least, I thought it was unbreakable at the time.) In those experiments, I used a signal from a national radio network as the "carrier." The "receiving" station—rather than broadcasting the signal, a telephone hook-up was used—picked up the same signal from a local radio station and used it for decoding a transmission.

Fortunately, I knew little about

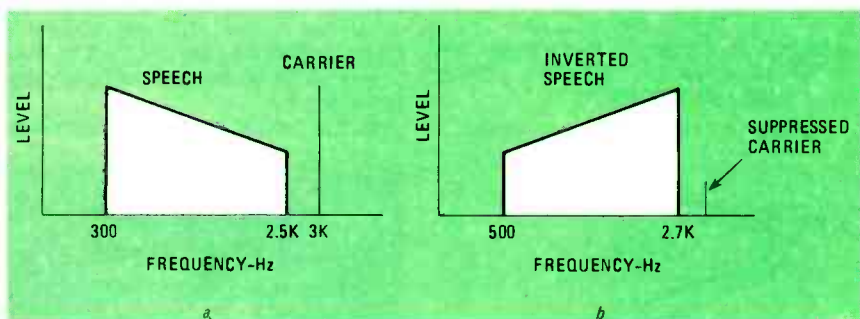


FIG. 1

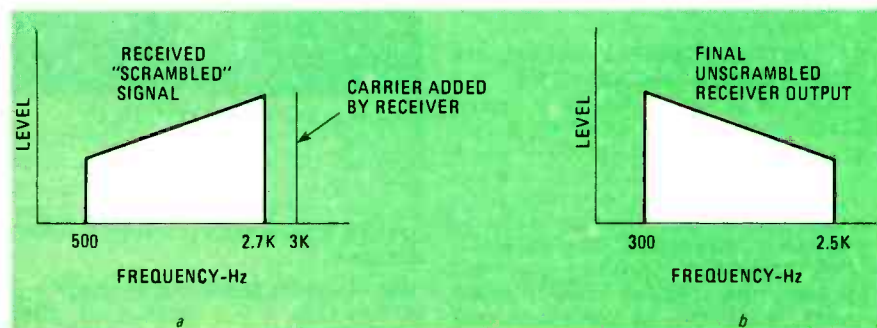


FIG. 2



scrambling at the time (which isn't all that much more than I know now) so I did not know that there were at least ten good reasons why the idea should not work. Of course the darned thing worked! The sound was somewhat garbled, but a message using some non-technical, simply constructed phrases could be understood. Had I known more about filters, and had the time to work on the thing, it probably would have proved commercially viable. But I was doing my experimentation just for fun, and once satisfied that my idea would more or less work, packed everything into a box and simply forgot about it.

Today, much scrambling is done using a microprocessor. Instead of the steady tone of a carrier, or the radio-station signal of my "Friedman Special," a constantly changing sampling rate is used to digitize a speech signal. The digital transmission also serves to program the microprocessor at the receiving station to decode the signal. When total security is required, the digitized transmission only serves to synchronize the microprocessor at the receiver. Since no key to the sampling sequence is transmitted, the scrambling is almost unbreakable. (I say "almost" because in electronics nothing is any better than "almost." By the time you read this, someone may very well be selling a 50-cent IC that is capable of "breaking" all of the digital scramblers currently in use.)

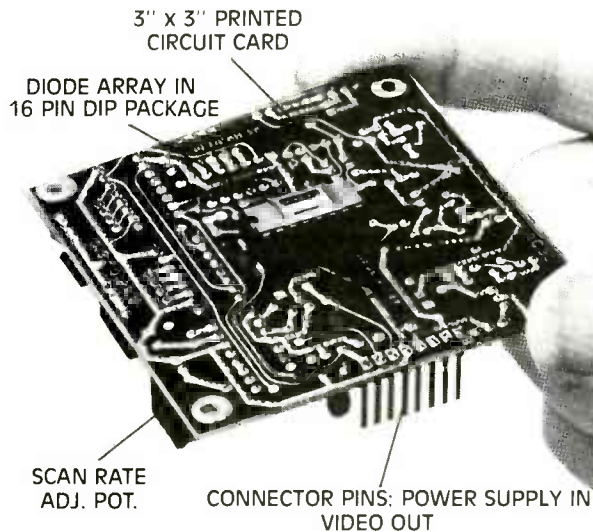
Though the digital scramblers are essentially unbreakable, many scrambler users make things simple, to keep overall costs down and receiving problems at a minimum. They are not as interested in absolute security as in making their copy unintelligible to the general public. After all, anyone that really wants to break a scrambler code can probably do so.

One major problem for the SWL is that HF-circuit scramblers are usually used with SSB. That means that you need a second local oscillator, because the receiver's regular BFO is being used to receive the SSB signal. You can either mix the received audio in a ring modulator with a variable-frequency/variable-level audio oscillator, or radiate a small tunable "IF frequency" into the antenna input, as was done in the early days of CB SSB. The whole thing is a lot of fun to try, although it is rather time-consuming when you're trying to establish the best "carrier" level in the descrambler.

If any of you give it a try, please drop me a line, in care of **Radio-Electronics**, and let me know how you make out. Perhaps some other readers will be interested in your results; we'll run the highlights of your experiments in future issues.

R-E

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MARCH 1982

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# COMPUTER CORNER

Games (computer) people play.

LES SPINDLE\*

DESPITE THE OFTEN-HEARD PHRASE "personal computer," microcomputers today are largely used as serious devices for practical business applications; the "computer-in-every-home" era still seems to be a considerable time away. To fuel the fires of home-computer sales, manufacturers and vendors try to impress upon consumers the image of the home computer as a practical device; but the largest percentage of software purchased by home users falls into the same category that predominated five years ago—fun and entertainment applications.

That should come as no surprise. The widespread use of some of the most sophisticated electronic developments of the last hundred years—television, radio, and the telephone—can still be attributed at least as much to their capabilities for providing amusement as to their use for communications.

Because of that, the computer-game industry is a booming business, with millions of dollars worth of game cassettes and disks being sold annually. Hundreds of software companies, large and small, release new offerings every month. Some examples of game software are shown in Fig. 1.

## Electronic-game history

The computer-game scramble began in 1966, when Ralph Baer sold the rights to his video-game invention, *Odyssey*, to Magnavox. The game reached the market in 1972, and the phenomenon was on its way.

The early games were simple, ping-pong-type diversions with little challenge or variety. The next phase offered more options for players by using switches to select various modes of operation. In 1977, with Fairchild's *Video Entertainment Center*, programmability was added.

Most modern games are sophisticated and challenging, because they offer the possibility for the player not only to alter the existing games, but also to devise new ones. That's made possible by a microprocessor in each game console, and by the availability of ROM (Read-Only Memory) cartridges containing the game elements.

All the games discussed so far have

been "dedicated" devices—all they can do is play games. The next step is a microcomputer system that permits you to expand your game-playing horizons beyond the limitations imposed by the dedicated game-machines. You can write your own games if you wish, and save the game results on cassette to determine your errors, or continue a game that had been started previously. And—perhaps the most important thing—after you've had your fill of game-playing, you can turn the computer to more practical applications.

Some manufacturers are turning out game consoles that are actually complete microcomputer systems, complete with keyboards and memory. The *Interact*, from Microelectronic Systems Corp., for instance, uses an 8080 microprocessor and offers some software in addition to games, including home and business applications-programs.

One popular computer that is especially suited for game-playing is the *Apple II*. While its capabilities extend far beyond that, it offers superb game-potential for the computer enthusiast who appreciates the computer's entertainment value as well as its practical side. With a keyboard, game paddles,

excellent graphics capabilities, and a sound generator, the computer is the ideal choice for creating games and playing those created by others. Needless to say, there is a wealth of game software available for the *Apple*.

## Game types

What kind of games can you expect to find for computers? There is a wide variety available, but a few popular formats tend to dominate the market. If you consider television to be a "sitcom factory" where one hit series spawns dozens of spinoffs, ripoffs, and imitations, you haven't seen anything until you've played the hundred-and-first version of a *Space Invaders* or *Star Trek* computer game. That doesn't seem to bother buyers, though; the formats that sell are the familiar ones.

At the simplest level, board-type games continue to be popular. Games such as tic-tac-toe, checkers, chess, and backgammon, hardly make extensive use of color graphics or other dazzling effects, but are formidable brain-teasers and entertain players for hours at a stretch. Several computer-chess competitions are held by computer clubs and other organizations

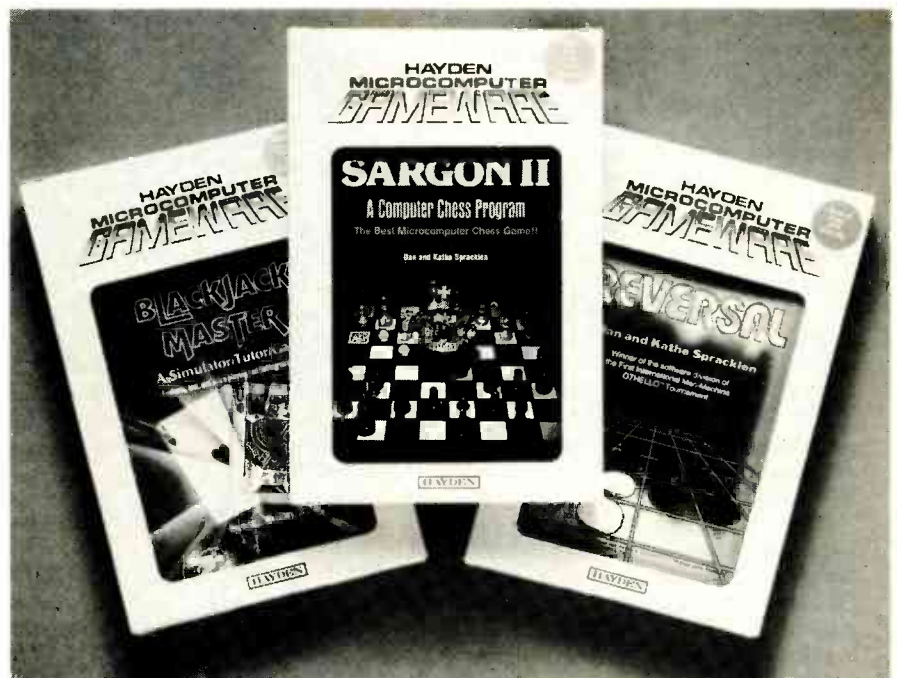


FIG. 1

\*Managing Editor, *Interface Age* magazine



here and in other parts of the world.

Guessing games provide some intellectual stimulation and, in some cases, are educational. Arithmetic calculations and problems in logic expand the programs into truly stimulating exercises. For example, one game challenges the player to search a grid of dots to locate a hidden object. Clues and hints are provided along the way to bring the astute player, step-by-step, closer to solving the puzzle.

Casino games satisfy the gambling instinct in computer buffs, creating exciting situations with poker, roulette, and blackjack competitions. While you can't win any money, you can't lose it, either.

### Simulations

Computers are widely used to perform simulations—programs that mimic real-life events, and whose outcome can be changed by changing the values of the data used.

Simulations are used in business to make long-range financial decisions by posing hypothetical situations to the computer. The armed forces frequently make use of computer simulations, and medical schools often depend on simulations for training purposes—electrons are more expendable than lives.

Simulations are also widely used in games. The Star Trek games cast the player as captain of the starship *Enterprise*; the object is to seek out and destroy Klingon battle cruisers without being destroyed yourself.

Another popular simulation is Adventure, a game in which you explore a vast, complex, underground world filled with treasures, magic, and menaces. The game is highly addictive and, when you've exhausted one version of Adventure—if that's possible—there are many more waiting.

Still another simulation puts you in the position of an air-traffic controller, guiding over 20 planes into, out of, and around your airport.

Home-computer versions of popular arcade games are also available. There are Space Invaders games to run on almost any machine. Missile Command and Pac-Man are two other games that have been adapted for microcomputers.

How do you select the best version of a game? Ask the man who plays one. Frequent your local computer club, follow the software reviews in computer magazines, and ask fellow computer owners whether you can try their games before investing in your own. You'll find the world of computer hobbyists—game enthusiasts, in particular—to be a friendly and cooperative brotherhood.

There's a saying: "You can tell the man from the boy by the price of his toy." Whoever coined that phrase must have been a computer buff. R-E

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# STATE OF SOLID STATE

## Play a tune with these new IC's

ROBERT F. SCOTT, SEMICONDUCTOR EDITOR

HARDLY A DAY PASSES THAT I DON'T read about some interesting new or improved semiconductor device, or of an innovative application for a more familiar one. But all too often, some of the most exciting devices are available only to equipment manufacturers, or are priced beyond the range of the average hobbyist.

That is not the case with a series of IC's available from Epson America. It has released a series of 24 melody-generator CMOS LSI devices. They are programmed to play selected melodies and to produce chime and alarm tones. They can be used in musical toys, to replace doorbells and chimes, as replacements for the mechanical devices

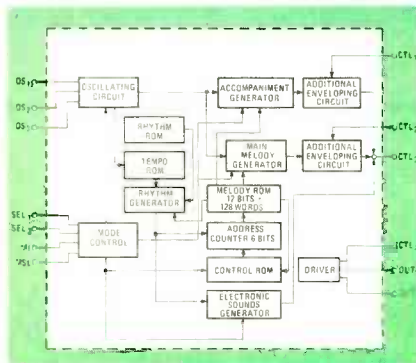


FIG. 1

in music boxes, and to produce musical tones that are a pleasant change from the strident clanging of a gong or the rasping sounds of a buzzer used in many applications. The devices are nearly complete in themselves, requiring only a speaker, 1.5-volt battery, and a few external parts for operation.

The 7910 series of IC's provides a selection of two preprogrammed tunes plus a chime and an alarm tone. The melody arrangements are diphonic—two notes sound at once. The 7930 series of IC's play only a single tune. The 7920's are simple 8-pin DIP devices, made by omitting the audio preamp/

driver from the 7930.

Figure 1 is a block diagram of a 7910 and Fig. 2 is a circuit that can be used to drive the IC. The built-in oscillator—two series-connected inverters connected between pins 1, 2, and 3 (terminals OS<sub>1</sub>, OS<sub>2</sub> and OS<sub>3</sub>) and tuned by R<sub>01</sub>, R<sub>02</sub>, and C<sub>0</sub>—generates a nominal frequency of 47.5 kHz. That signal is processed by the various internal circuits to develop the notes, tempo, keying, shaping, and other controls needed to produce a specific melody, chime, or alarm.

Pin 4 (terminal MI) is the on-off control point. The tune starts at the beginning of the melody when that terminal is switched HIGH (connected to V<sub>DD</sub>) and continues until the circuit to terminal MI is opened (switched to LOW). If the terminal is still switched HIGH when the tune ends, the tune is simply played over.

Control terminals CTL<sub>1</sub> and CTL<sub>2</sub> (pins 10 and 11), when connected to R1-C1 and R2-C2, regulate the time constant of the envelope. The overall tone can be changed by varying C1, C2, R1, and R2. Terminal CTL<sub>3</sub> (pin 12) is the unamplified output of the melody-generator section of the IC. Terminal CTL<sub>4</sub> (pin 13) is the input to the built-in audio preamplifier. In Fig. 2, R4 is the volume control. Terminals OUT<sub>1</sub> and OUT<sub>2</sub> (pins 14 and 15) are the preamp outputs used to drive the complementary bipolar output-transistors.

Terminals SEL<sub>1</sub>, SEL<sub>2</sub>, and MSL (pins 5, 6, and 9) are used to control the output of the IC. The terminals are connected to switches (S1-S3) that are used to select melodies, chimes, or alarm, depending on their setting. Table 1 shows

TABLE 1

| FUNCTION            | S1 | S2  | S3  | S4 |
|---------------------|----|-----|-----|----|
| Melody 1            | on | off | off | on |
| Melody 2            | on | off | off | on |
| Buzzer              | —  | on  | off | on |
| Chime               | —  | off | on  | on |
| Test mode/melody 1  | on | on  | on  | on |
| Test model/melody 2 | on | on  | on  | on |

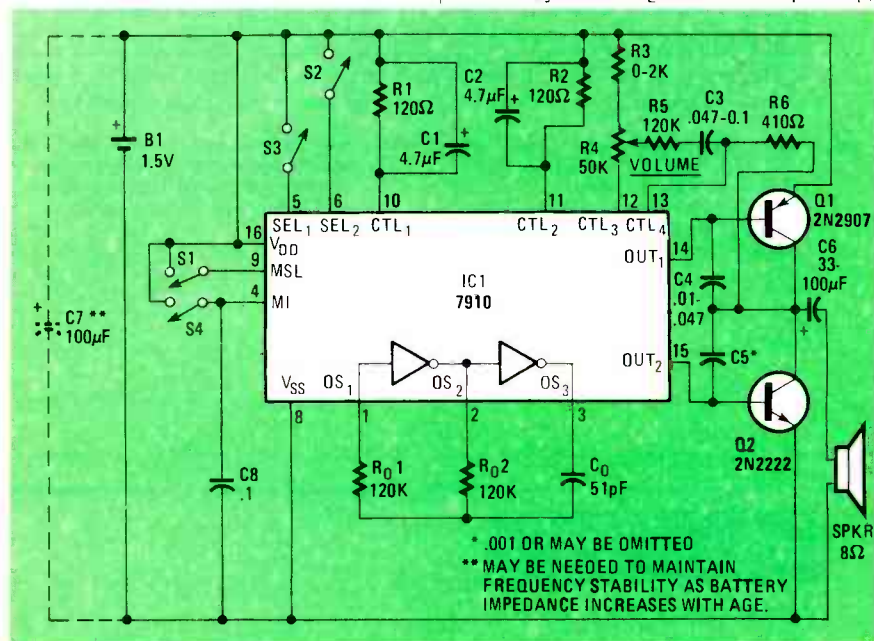


FIG. 2

\* .001 OR MAY BE OMITTED  
 \*\* MAY BE NEEDED TO MAINTAIN FREQUENCY STABILITY AS BATTERY IMPEDANCE INCREASES WITH AGE.



the switch settings for a 7910 programmed for two melodies and two alarm sounds. In the MELODY TEST modes, the tempo of the selected melody is stepped up eight times. The switch settings for 7910's that have two melodies and no alarm, or no melodies and two alarm sounds, are similar to those in the table.

I've mentioned the possibility of using a melody generator as a replacement for a doorbell. For that application, I suggest the 7910-O, P, X, or CH versions. Those are different 16-note arrangements of Westminster chimes; the devices are suitable for use as doorbells since they are programmed to play through just once and then stop.

At present, there are fifteen different IC's in the 7910 series, seven in the 7930 series, and two in the 7920 series. The melodies available are too numerous to list here, but, to give you some idea of what is available, they range from "Jingle Bells" and "Silent Night" in the 7910-CU to a Chopin nocturne and a Mozart minuet in the 7910-CE.

Sample quantities (1 to 9) of the 7910, 7930, and 7920 cost \$10, \$8, and \$7 each, respectively. Circuit boards are available and cost \$15 for the 7910; boards for the 7930 and 7920 cost \$10. If you order the IC and circuit board together (\$25 for the 7910, \$18 for the 7930 and 7920), you get an evaluation kit that includes all parts; all you have to add are an 8-ohm speaker and a 1.5-volt AA cell. To order any of those items, write to Epson America, 3415 Kashiwa St., Torrance, CA 90505. When ordering, include \$1 for shipping and handling. (California and New York residents, add appropriate sales tax.) Incidentally, tune lists and data sheets for the IC's are also available.

R-E



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| MS-215 | 15MHz              | 10mV to 50V/div.<br>12 Ranges | 0.1µ Sec to 0.5 Sec.<br>21 Ranges      |
| MS-15  | 15MHz              | 10mV to 50V/div.<br>12 Ranges | 0.1µ Sec to 0.5 Sec.<br>21 Ranges      |

MS 230



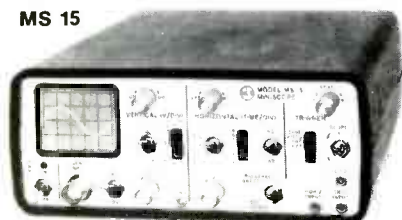
MS 215



Non-Linear Systems' trio of mini-oscilloscopes are accurate, affordable, portable. And there's one to match nearly every budget and need. Standard features on all models include an input impedance of 1 megohm with 50 pF; maximum input voltage of 350 V; trigger modes in auto, internal, external and line; slope that's + or - selectable; graticule (4x5 division of 0.25" each); dual power sources operating either internally from rechargeable lead acid batteries or externally from 115 VAC or 230 VAC (50-60 Hz) via plug-in transformer; handy size (2.9"H x 6.4"W x 8.0"D) and weighs just 3 lbs.\*

Check the chart below for details of model features and specifications.

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# SERVICE CLINIC

## Vertical-retrace-line problems

JACK DARR, SERVICE EDITOR

OVER THE YEARS I'VE RECEIVED A LOT of letters concerning vertical-retrace-line problems. That used to be one of the most "popular" complaints. The problem is easy to identify—there are four or five bright lines at the top of the screen, and they always start at the upper right corner and slant down toward the left. In the early 1950's, TV sets suffered a lot from that complaint, and it was frequently said that the sets came with built-in retrace lines. I've had quite a few letters about the problem recently, and the last one said, "Why don't you write a 'Service Clinic' column about it?" Always happy to receive inspiration, I accepted, and here it is.

Vertical blanking is simple. You feed a vertical-frequency pulse into one of the video circuits, or directly to the picture tube (see Fig. 1). That pulse must be exactly as long as the vertical-blanking interval, and with enough amplitude, and the right polarity, to cause the electron beam in the picture tube to be cut off.

Naturally, the pulse must be present during the vertical-blanking interval (which is the black horizontal bar between frames, as if you didn't know!)

A lot of different vertical-blanking circuits have been used. Early sets fed positive-going pulses to the cathode of the picture tube, or negative-going pulses to the grid. The important thing is

that the polarity of the pulse has to be in the direction of cutoff, and the amplitude high enough to cause full cutoff. One oddball circuit I remember fed rather-high-voltage negative pulses to the picture tube's screen grid! That was on a black-and-white tube set, of course. If you're restoring antiques, watch for it; usually pulses were fed in through capacitors, with shunt resistors. Check for leaky or open capacitors, or resistors whose values have drifted.

Later-model sets, especially solid-state ones, feed blanking pulses into one of the early video-amplifier stages. Very often the first video-stage is used. Popular circuits feed vertical-blanking pulses either into the base or emitter of that transistor. For NPN transistors, the pulse applied to the base is negative-going (reverse biased) while a pulse to the emitter is positive-going. The pulses are often fed through series or shunt diodes; more about them later.

The actual vertical-blanking pulses can be picked off the vertical oscillator-output circuit at quite a few points. What's needed is a point that has a pulse of the proper polarity and amplitude. Sometimes the pulse is shaped by R-C networks. One of the older sets even took the pulse from the vertical yoke! Some solid-state sets use a vertical-blanking amplifier-transistor, for a higher-amplitude pulse, wave-shaping etc. You can find the pickoff point by

looking for a line that isn't used in the vertical circuitry, but goes out and away, usually toward the top of the schematic.

### Other trouble sources

There are a few other things—not in the vertical circuits—that can cause retrace lines to show up. In older sets, if the brightness or contrast is too high, you may see retrace lines. That can be fixed by readjusting the controls. Also, if the AGC is set too far toward "white-out," that can cause the lines to appear. Reset the AGC control and see if that helps.

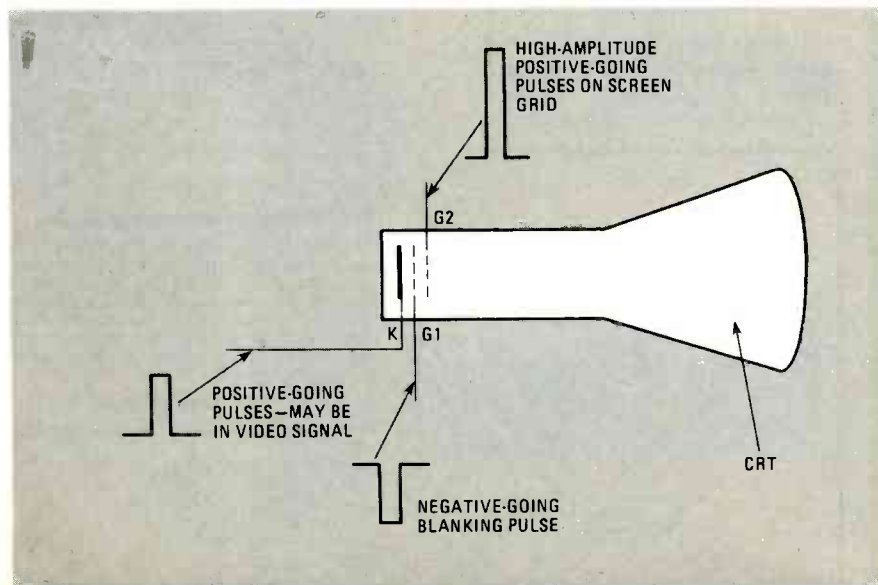
In the cases just mentioned, the lines show up because the picture tube is simply being driven too hard for the normal blanking-pulse to cause it to be cut off. In recent sets, automatic brightness-limiter circuits have contributed a lot to curing the problem. But they can also be the cause of the lines: If you see retrace lines in a set with an ABL, make sure that the circuit's working.

Check the schematic to see if a vertical-blanking amplifier-transistor is used. If so, and you see retrace lines, use a scope on that stage to make sure it is working. An open transistor could be the source of your trouble. If the transistor is leaky, it can do strange things to the blanking pulse—make it wider, distort its shape, etc., which causes really odd symptoms on the screen.

### Blanking diodes

Here's some more about the blanking diodes. Any defect in them causes problems. If a series diode is open, you'll lose the pulse entirely. A series diode that is shorted also causes odd problems. And leakage in those diodes really causes some oddball ones! One is "window-shading:" when the brightness is turned down, the raster goes dark from top to bottom just as though someone were pulling a shade down over it. That would be caused by the vertical-blanking diode. If the raster goes out from left to right, as if someone were pulling a drape across it, that usually means a leaky horizontal-blanking diode.

A shorted horizontal-blanking diode often produces the "jail bars" symptom—there will be five or six black ver-





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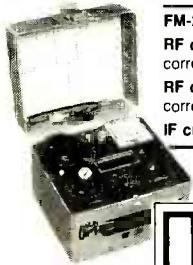
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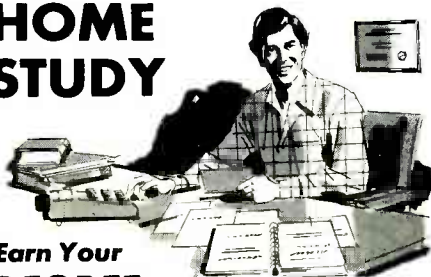


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tical bars in the picture: the picture will be seen between the bars. Those bars are due to the normally-present series of "ringing pulses" present on the horizontal part of the HV pulse: the shorted diode lets them get through. (It's supposed to clip them off and leave only the spike.)

There are even stranger problems, too. In one old set, we had what looked like retrace lines; closer examination showed that they didn't slant but were almost horizontal, and had flashes of color and bright points in them. After quite a bit of checking, the cause turned out to be a bad integrator circuit in the feedback loop. It was one of the ceramic-types, which looks like a ceramic capacitor with three leads. It was causing a very narrow and sharp top-foldover of the raster; the odd things seen, including the color, were the VITS signals, which are in the vertical-blanking interval.

An oscilloscope is the best piece of test equipment to use with that type of problem, or with any sync problem—you can follow the blanking pulses from their point of origin all the way to their destination, to make sure they get there, or to find the point where they drop out. When you find that point check voltages, components, etc. **R-E**

# SERVICE QUESTIONS

## THIS CAN'T HAPPEN!

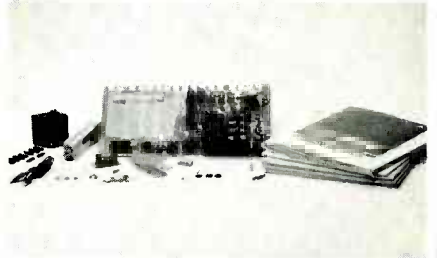
This happened with a Magnavox T920 chassis: There was no vertical sync. The set worked fine on the test jig, but not in its cabinet. I tried a new yoke and convergence board with no luck. That left only the picture tube. I had another picture tube in a cabinet with the chassis out, so I used the Magnavox yoke and convergence assembly, slipped the chassis in, and it worked fine. So I replaced the picture tube and now everything's back to normal. I know this isn't supposed to happen, but it did!—*W.S., Houston, TX*  
*I'm sure glad you didn't ask me why!*

## HOT FOLDOVER

*I have a Sylvania EO-9 that develops a bad foldover after it has been run for a while. I've replaced the IC-300 V/H divider and checked many of the resistors and capacitors around it without any luck. I tried cooling things down and found that if I cooled the IC, the picture would straighten out and stay normal for five or ten minutes. I put the original IC back and found that the same thing happens. The schematic shows a voltage regulator, SC310, but I can't find it. Any help would be appreciated.—R.H. Susquehanna, PA*

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It sounds as if your problem is in the voltages at the IC. You indicated that you measured +5.97 volts at pin three, the  $V_{CC}$  input. That's too high! The correct voltage should be +4.3 volts.

From the parts list, SC310 is a 4.3-volt Zener diode. I'd say that it's either open or missing. Get a 4.3- or 4.7-volt Zener and tie it directly from pin three to ground. That should do the job, and the original IC may still be usable.

### BAD PICTURE TUBE?

*We've got a GE 25YM that was damaged by lightning. We replaced some parts that obviously needed replacing. That didn't work—you turn the set on and the circuit breaker trips. Our old tester told us that the picture tube (25-EKP22) was shorted even though an ohmmeter didn't indicate anything was wrong. What's your opinion?—J.P., Cortez, CO*

I think your picture-tube tester is right. I've run into several sets with the picture tubes shorted so badly that they kill the HV and trip the breaker. (I didn't believe it the first time—the set would run with the HV lead disconnected. On a test jig it gave a perfect picture. So, we changed the picture tube and that was that.)

### NO VIDEO, LOW VOLTAGE

*I have no picture, only a raster with colored horizontal lines, on a Zenith*

*K1908C. Checking, I found only +50 volts on the supply to the video-output module, instead of the +238 volts shown on the schematic. The boost is a bit high, but the HV is normal. The +238 volts is derived from the flyback. Do you think the flyback is bad?—E.M., N. Olmsted, OH*

No, not the flyback. Note that many other voltages that are derived from the flyback are OK: the boost, HV, etc. Your problem is either an open rectifier on that +238-volt source, or something of that sort. Check any resistors that are in series with that supply, between it and the video-output module. The symptoms are not those of a short; that leaves only a bad diode or an open series-resistor as the likely cause.

### HORIZONTAL RIPPLE

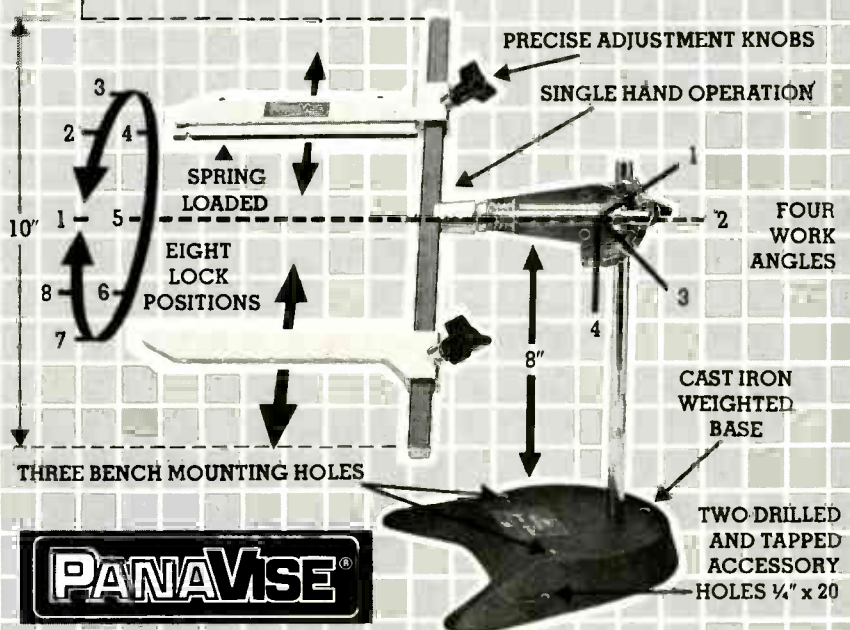
*I've got a bad case of what looks like full-wave horizontal ripple in a Sylvania E01-9. I replaced the main filter capacitors, but it's still there. If I disconnect the degaussing coil, the ripple just gets worse. That shouldn't have anything to do with the filtering, should it?—J.T., Memphis, TN.*

No—the degaussing coil isn't involved. I ran into that situation some time back and the problem turned out to be an open diode in the full-wave bridge rectifier. You have a similar case, so check all of the diodes and the solder joints.

R-E

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**USING MICROCOMPUTERS IN BUSINESS. A Guide for the Perplexed**, by Stanley S. Veit. Hayden Book Company, Inc., 50 Essex Street, Rochelle Park, NJ 07662. 142 pp including appendices and index; 6 x 9 inches; softcover. \$9.95.

This book, written by the man who opened the "second-oldest computer store in the world," is an essential background reference for any purchaser of computer systems or software for a business. It describes the advantage of "computerization" and provides the potential user with the data necessary to make intelligent choices.

Chapters 1 and 2 cover various types of businesses and the programs they need, with reference to the ability of small computers to handle those needs. They are followed by chapters on word processing; data-base management systems; how to install a computer without disrupting your business; buying your system; computer languages; the limitations of the microcomputer; software; where to find it and how to judge it, and what to do when the system goes down. The two final chapters deal with how a microcomputer works and microcomputer memory.

The book has many photos and easy-to-follow diagrams, and is written in plain language, without technical jargon. It answers the most-often-asked questions about computers and offers advice, information, and warnings which have been proved valid.

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**WHY DO YOU NEED A PERSONAL COMPUTER?** by Lance A. Leventhal and Irvin Stafford. John Wiley & Sons, Inc., One Wiley Drive, Somerset, NJ 08873. 278 pp including appendices and index; 6 3/4 x 10 inches; softcover; \$8.95.

This is a non-technical, fully illustrated, down-to-earth introduction to the world of personal computers. It offers detailed guidelines on the advantages and drawbacks of every type of personal computer; gives sources of equipment and information; provides a step-by-step introduction to the BASIC language, along with an easy-to-follow course in writing programs; information on how to maintain a computer and what to do if it breaks down; a user-directed discussion of peripherals and interfacing, and an extended glossary.

The reader will learn how versatile personal computers are and the many everyday applications they can perform, as well as what will be needed for a useful system and how to select a system that meets the user's personal requirements. Innumerable low-cost personal computers are widely advertised; this book will help the reader to choose among the many offerings and understand what the advertisements really mean.

**CIRCLE 151 ON FREE INFORMATION CARD**

**THE COMPLETE HANDBOOK OF MAGNETIC RECORDING**, by Finn Jorgensen. TAB Books, Inc., Blue Ridge Summit, PA 17214. 448 pp including appendix, additional reading list, and index; 5 1/2 x 8 3/4 inches; softcover; \$10.95.

This textbook of "know-how" and reference, covering all aspects of magnetic recording, is written both for the technically inclined person working in the field and for the equipment user who wants to get in-depth knowledge of magnetic recording equipment and principles.

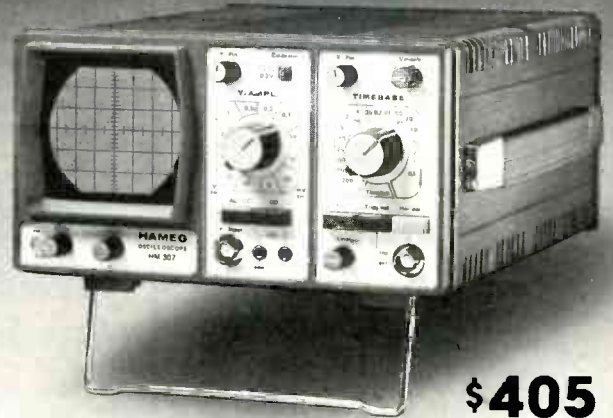
Chapter 1 gives a brief history, followed by an introduction to recording equipment (chapter 2). The rest of the book falls into three main sections: Fundamentals; Heads, Tapes, and Discs, and Equipment and Application.

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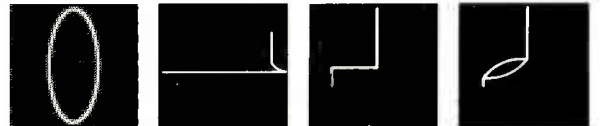
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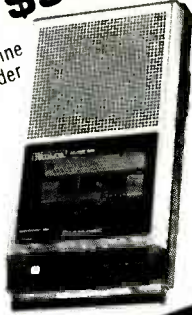
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**GRAPHIC EQUALIZER**, model EQ2400, is a stereo frequency equalizer for the home recordist or music listener. The user can listen to music "flat" while making and monitoring an equalized recording, or



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**CASSETTE DECK**, model ND-1000, is a two-motor, direct-drive system that assures accurate tape travel. Its three tape heads also add to tape-transport accuracy, while permitting off-the-tape monitoring as well. The transport also features full IC logic control, permitting smooth tape-function switching without

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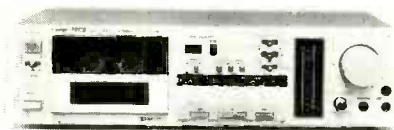
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The model ND-1000 accepts metal, normal, and CrO<sub>2</sub> tapes, and applies accurate equalization with each. Other features include two 12-section LED peak-level displays for accurate monitoring, separate left and right level controls, and a front-panel output-level control. Its standard *Dolby B* noise-reduction system is augmented by an MPX filter for interference-free off-the-air recording. There are also an automatic rewind function, a timer-activated record/playback function, and an automatic memory-stop/memory-play function.

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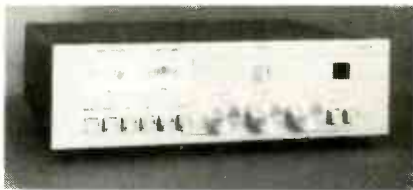
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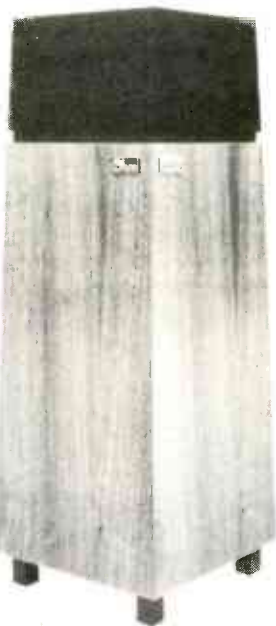
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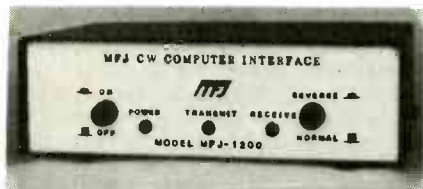
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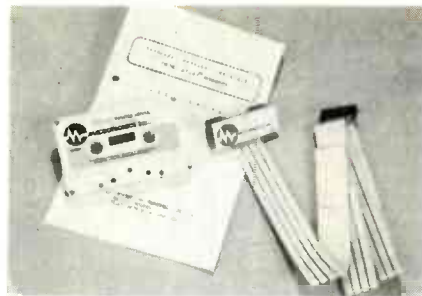
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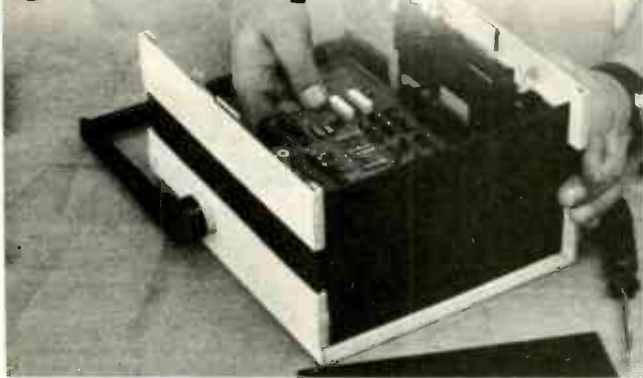
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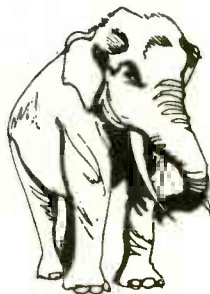
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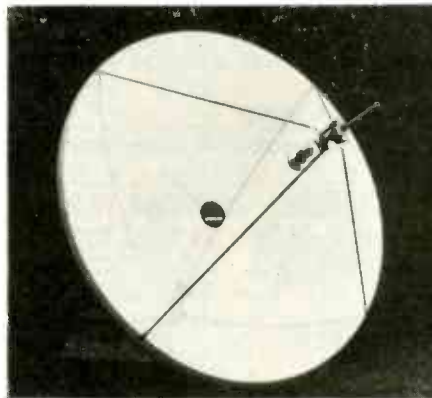
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## CHANNEL 1?

*continued from page 46*

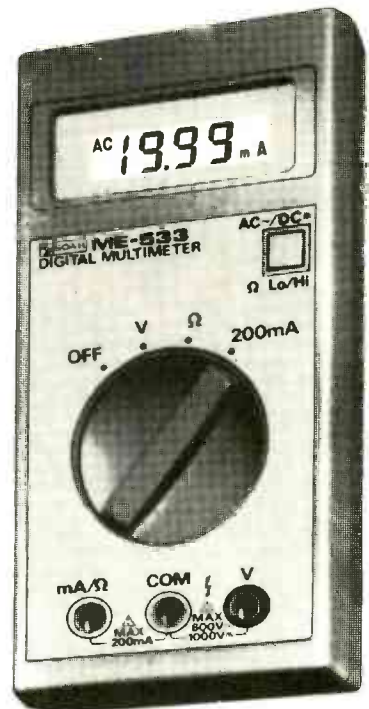
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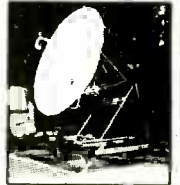
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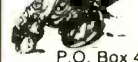
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Kit comes with regulated power supply, all you need is a 48V C.T. transformer @ 0.5A.

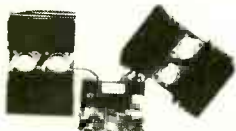
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- One channel, needs two for stereo



**TA-1000KIT**  
**\$51.95**  
Power transformer  
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**50 WATTS AUTO STEREO BOOSTER BY VERTRONIX**

Specifications: • 50 watts RMS total (25W + 25W)



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- Frequency Response:  $\pm 0.5dB$ , 20Hz ~ 20KHz
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**Super Buy**  
**Only \$18.50**

Kit includes 2 pcs. Fisher PA 301 Hybrid IC all electronic parts with PC Board. Power supply  $\pm 16V$  DC (not included). Power band with (KF 1%  $\pm 3dB$ ) Voltage gain 33dB. 20Hz-20KHz.

**5W AUDIO AMP KIT**



2 LM 380 with Volume Control  
Power Supply 6 ~ 18V DC  
**ONLY \$6.00 EACH**

**2 WATT AUDIO AMP**

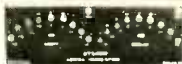
Pre assembled units. All you need is to hook up the speaker and the volume control. Supply voltage from 9~15V D.C. measures only 2" x 3 1/2", making it good for portable or discrete applications. Comes with hook up data.



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Stereo level indicator kit with arc-shape display panel!!! This Mark III LED level indicator is a new design PC board with an arc-shape 4 colors LED display (change color from red, yellow, green and the peak output indicated by rose). The power range is very large from -30dB to +5dB. The Mark III indicator is applicable to 1 watt - 200 watts amplifier operating voltage is 3V-9V DC at max 400 MA. The circuit uses 10 LEDs per channel. It is very easy to connect to the amplifier. Just hook up with the speaker output!

**IN KIT FORM \$18.50**

**MARK IV 15 STEPS LED POWER LEVEL INDICATOR KIT**

This new stereo level indicator kit consists of 36 4-color LED (15 per channel) to indicate the sound level output of your amplifier from -36dB +3dB. Comes with a well-designed silk screen printed plastic panel and has a selector switch to allow floating or gradual output indicating. Power supply is 6 ~ 12V D.C. with THG on board input sensitivity controls. This unit can work with any amplifier from 1W to 200W! Kit includes 70 pcs. driver transistors, 38 pcs. matched 4-color LED, all other electronic components, PC board and front panel.



**MARK IV KIT \$31.50**

**MARK V 15 STEPS LED POWER OUTPUT INDICATOR KIT**

All functions same as Mark IV but this is with heavy duty aluminum front plate and case. Can be easily slot into the front panel of your auto, truck or boat. Operates on 12V DC.



**\$41.50 EACH KIT**

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• Power Supply: 117 VAC  
Kit comes with all electronic components, transformer, instructions and a 19" rack mount type metal cabinet.



**MODEL TA-2500 \$119.00 PER KIT**

**ELECTRONIC DUAL SPEAKER PROTECTOR**

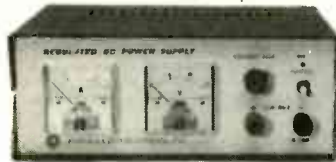


Cut off when circuit is shorted or over load to protect your amplifier as well as your speakers. A must for OCL circuits.

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$\pm 4$  ~ 30V DC 800 MA adjustable, fully regulated by Fairchild 78MG and 79MG voltage regulator I.C. Kit includes all electronic parts, filter capacitors, I.C. heat sinks and P.C. board.



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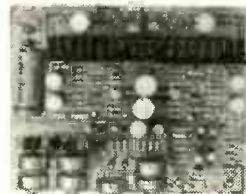
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**EXCELLENT PRICE!**

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We sell you all the above components in a package for **\$125.00** and you will receive a free predrilled P.C. board and instructions at no charge!

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For UHF CH 14 83  
Tuning voltage +1V~+28V D.C. Input impedance 75 OHM. I.F. band width 7~16 MHz. Noise figure 11.5dB MAX. Size 2 3/4" x 1 1/4" x 3/4". Supply voltage 15V D.C. Sound I.F. = 58.0 MHz. Video I.F. = 62.5 MHz.



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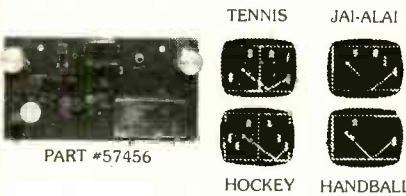
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**DIGITAL TIMER/CLOCK**

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- Displays month, date and day of the week
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- Back light by touch of the switch

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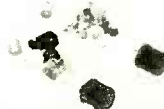
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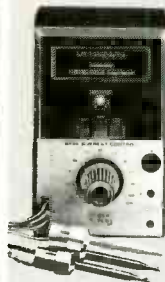


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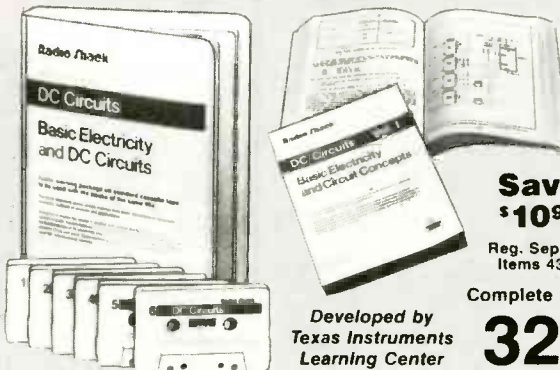
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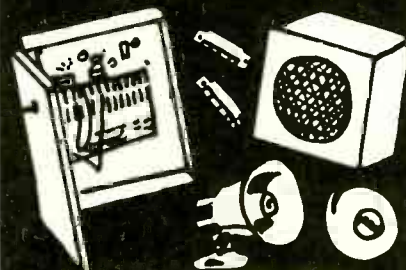
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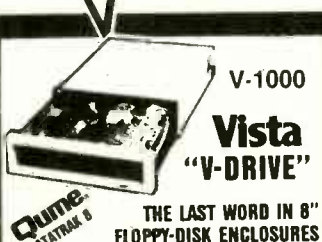


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| 8088-18014398919808MHz             | 19.95    |
| 8088-36028797839616MHz             | 14.95    |
| 8088-72057595679232MHz             | 19.95    |
| 8088-144115191384448MHz            | 14.95    |
| 8088-288230382768896MHz            | 19.95    |
| 8088-576460765537792MHz            | 14.95    |
| 8088-1152921531075584MHz           | 19.95    |
| 8088-2305843062151168MHz           | 14.95    |
| 8088-4611686124302336MHz           | 19.95    |
| 8088-9223372248604672MHz           | 14.95    |
| 8088-18446744737211344MHz          | 19.95    |
| 8088-36893489474422688MHz          | 14.95    |
| 8088-73786978948845376MHz          | 19.95    |
| 8088-14757397797770752MHz          | 14.95    |
| 8088-29514795595541504MHz          | 19.95    |
| 8088-59029591190893008MHz          | 14.95    |
| 8088-11805918237817600MHz          | 19.95    |
| 8088-23611836475635200MHz          | 14.95    |
| 8088-472236729512664000MHz         | 19.95    |
| 8088-94447345903328000MHz          | 14.95    |
| 8088-188894691806560000MHz         | 19.95    |
| 8088-377789383613120000MHz         | 14.95    |
| 8088-755578767226240000MHz         | 19.95    |
| 8088-1511157534452800000MHz        | 14.95    |
| 8088-3022315068905600000MHz        | 19.95    |
| 8088-60446301378112000000MHz       | 14.95    |
| 8088-120892602763224000000MHz      | 19.95    |
| 8088-241785205526448000000MHz      | 14.95    |
| 8088-483570411052976000000MHz      | 19.95    |
| 8088-9671408221059520000000MHz     | 14.95    |
| 8088-19342964442118400000000MHz    | 19.95    |
| 8088-38685928884236800000000MHz    | 14.95    |
| 8088-77371857768473600000000MHz    | 19.95    |
| 8088-1547437155376953600000000MHz  | 14.95    |
| 8088-3094874310753907200000000MHz  | 19.95    |
| 8088-6189748621507814400000000MHz  | 14.95    |
| 8088-12379497243156288000000000MHz | 19.95    |
| 8088-24758994486312576000000000MHz | 14.95    |
| 8088-49517988972625152000000000MHz | 19.95    |
| 8088-99035977945250304000000000MHz | 1        |



# 7400

|         |     |          |      |          |      |          |      |
|---------|-----|----------|------|----------|------|----------|------|
| SN7400N | .19 | SN74123N | .59  | SN74150N | .26  | SN74156N | 1.19 |
| SN7401N | .22 | SN74125N | .39  | SN74151N | 2.19 | SN74157N | .89  |
| SN7402N | .22 | SN74126N | .44  | SN74152N | .28  | SN74158N | 2.48 |
| SN7403N | .22 | SN74128N | .59  | SN74153N | .28  | SN74159N | 1.15 |
| SN7404N | .22 | SN74132N | .69  | SN74154N | .35  | SN74160N | 1.15 |
| SN7405N | .22 | SN74136N | .75  | SN74155N | .35  | SN74161N | 1.15 |
| SN7406N | .23 | SN74139N | .85  | SN74156N | .35  | SN74162N | 1.15 |
| SN7407N | .23 | SN74141N | .79  | SN74157N | .35  | SN74163N | 1.15 |
| SN7408N | .26 | SN74142N | 2.95 | SN74158N | .35  | SN74164N | 1.15 |
| SN7409N | .23 | SN74143N | 2.95 | SN74159N | .35  | SN74165N | 1.15 |
| SN7410N | .22 | SN74144N | 2.95 | SN74160N | .35  | SN74166N | 1.15 |
| SN7411N | .22 | SN74145N | 1.95 | SN74161N | .35  | SN74167N | 1.15 |
| SN7412N | .29 | SN74147N | 1.95 | SN74162N | .35  | SN74168N | 1.15 |
| SN7413N | .39 | SN74148N | 1.20 | SN74163N | .35  | SN74169N | 1.15 |
| SN7414N | .59 | SN74150N | 1.09 | SN74164N | .35  | SN74170N | 1.15 |
| SN7415N | .29 | SN74151N | .67  | SN74165N | .35  | SN74171N | 1.15 |
| SN7416N | .22 | SN74152N | .67  | SN74166N | .35  | SN74172N | 1.15 |
| SN7417N | .22 | SN74153N | .87  | SN74167N | .35  | SN74173N | 1.15 |
| SN7418N | .35 | SN74154N | 1.19 | SN74168N | .35  | SN74174N | 1.15 |
| SN7419N | .29 | SN74155N | .78  | SN74169N | .35  | SN74175N | 1.15 |
| SN7420N | .29 | SN74156N | .69  | SN74170N | .35  | SN74176N | 1.15 |
| SN7421N | .29 | SN74157N | .69  | SN74171N | .35  | SN74177N | 1.15 |
| SN7422N | .29 | SN74158N | 1.65 | SN74172N | .35  | SN74178N | 1.15 |
| SN7423N | .25 | SN74159N | .88  | SN74173N | .35  | SN74179N | 1.15 |
| SN7424N | .25 | SN74160N | .88  | SN74174N | .35  | SN74180N | 1.15 |
| SN7425N | .25 | SN74161N | .88  | SN74175N | .35  | SN74181N | 1.15 |
| SN7426N | .25 | SN74162N | .89  | SN74176N | .35  | SN74182N | 1.15 |
| SN7427N | .25 | SN74163N | .89  | SN74177N | .35  | SN74183N | 1.15 |
| SN7428N | .25 | SN74164N | .89  | SN74178N | .35  | SN74184N | 1.15 |
| SN7429N | .25 | SN74165N | .89  | SN74179N | .35  | SN74185N | 1.15 |
| SN7430N | .23 | SN74166N | .87  | SN74180N | .35  | SN74186N | 1.15 |
| SN7431N | .23 | SN74167N | .95  | SN74181N | .35  | SN74187N | 1.15 |
| SN7432N | .23 | SN74168N | 1.99 | SN74182N | .35  | SN74188N | 1.15 |
| SN7433N | .23 | SN74169N | 1.65 | SN74183N | .35  | SN74189N | 1.15 |
| SN7434N | .23 | SN74170N | 1.65 | SN74184N | .35  | SN74190N | 1.15 |
| SN7435N | .23 | SN74171N | 1.65 | SN74185N | .35  | SN74191N | 1.15 |
| SN7436N | .23 | SN74172N | 1.65 | SN74186N | .35  | SN74192N | 1.15 |
| SN7437N | .23 | SN74173N | 1.65 | SN74187N | .35  | SN74193N | 1.15 |
| SN7438N | .23 | SN74174N | 1.65 | SN74188N | .35  | SN74194N | 1.15 |
| SN7439N | .23 | SN74175N | 1.65 | SN74189N | .35  | SN74195N | 1.15 |
| SN7440N | .19 | SN74176N | 1.99 | SN74190N | .35  | SN74196N | 1.15 |
| SN7441N | .79 | SN74177N | 1.65 | SN74191N | .35  | SN74197N | 1.15 |
| SN7442N | .57 | SN74178N | 4.75 | SN74192N | .35  | SN74198N | 1.15 |
| SN7443N | .95 | SN74179N | 7.75 | SN74193N | .35  | SN74199N | 1.15 |
| SN7444N | .95 | SN74180N | 7.75 | SN74194N | .35  | SN74200N | 1.15 |
| SN7445N | .79 | SN74181N | 8.9  | SN74195N | .35  | SN74201N | 1.15 |
| SN7446N | .79 | SN74182N | 8.9  | SN74196N | .35  | SN74202N | 1.15 |
| SN7447N | .75 | SN74183N | 8.9  | SN74197N | .35  | SN74203N | 1.15 |
| SN7448N | .75 | SN74184N | 8.9  | SN74198N | .35  | SN74204N | 1.15 |
| SN7449N | .75 | SN74185N | 8.9  | SN74199N | .35  | SN74205N | 1.15 |
| SN7450N | .75 | SN74186N | 8.9  | SN74200N | .35  | SN74206N | 1.15 |
| SN7451N | .19 | SN74187N | 1.15 | SN74201N | .35  | SN74207N | 1.15 |
| SN7452N | .19 | SN74188N | 1.15 | SN74202N | .35  | SN74208N | 1.15 |
| SN7453N | .19 | SN74189N | 1.15 | SN74203N | .35  | SN74209N | 1.15 |
| SN7454N | .19 | SN74190N | 1.15 | SN74204N | .35  | SN74210N | 1.15 |
| SN7455N | .19 | SN74191N | 1.15 | SN74205N | .35  | SN74211N | 1.15 |
| SN7456N | .19 | SN74192N | 1.15 | SN74206N | .35  | SN74212N | 1.15 |
| SN7457N | .19 | SN74193N | 1.15 | SN74207N | .35  | SN74213N | 1.15 |
| SN7458N | .19 | SN74194N | 1.15 | SN74208N | .35  | SN74214N | 1.15 |
| SN7459N | .19 | SN74195N | 1.15 | SN74209N | .35  | SN74215N | 1.15 |
| SN7460N | .19 | SN74196N | 1.15 | SN74210N | .35  | SN74216N | 1.15 |
| SN7461N | .19 | SN74197N | 1.15 | SN74211N | .35  | SN74217N | 1.15 |
| SN7462N | .19 | SN74198N | 1.15 | SN74212N | .35  | SN74218N | 1.15 |
| SN7463N | .19 | SN74199N | 1.15 | SN74213N | .35  | SN74219N | 1.15 |
| SN7464N | .19 | SN74200N | 1.15 | SN74214N | .35  | SN74220N | 1.15 |
| SN7465N | .19 | SN74201N | 1.15 | SN74215N | .35  | SN74221N | 1.15 |
| SN7466N | .19 | SN74202N | 1.15 | SN74216N | .35  | SN74222N | 1.15 |
| SN7467N | .19 | SN74203N | 1.15 | SN74217N | .35  | SN74223N | 1.15 |
| SN7468N | .19 | SN74204N | 1.15 | SN74218N | .35  | SN74224N | 1.15 |
| SN7469N | .19 | SN74205N | 1.15 | SN74219N | .35  | SN74225N | 1.15 |
| SN7470N | .19 | SN74206N | 1.15 | SN74220N | .35  | SN74226N | 1.15 |
| SN7471N | .19 | SN74207N | 1.15 | SN74221N | .35  | SN74227N | 1.15 |
| SN7472N | .19 | SN74208N | 1.15 | SN74222N | .35  | SN74228N | 1.15 |
| SN7473N | .19 | SN74209N | 1.15 | SN74223N | .35  | SN74229N | 1.15 |
| SN7474N | .19 | SN74210N | 1.15 | SN74224N | .35  | SN74230N | 1.15 |
| SN7475N | .19 | SN74211N | 1.15 | SN74225N | .35  | SN74231N | 1.15 |
| SN7476N | .19 | SN74212N | 1.15 | SN74226N | .35  | SN74232N | 1.15 |
| SN7477N | .19 | SN74213N | 1.15 | SN74227N | .35  | SN74233N | 1.15 |
| SN7478N | .19 | SN74214N | 1.15 | SN74228N | .35  | SN74234N | 1.15 |
| SN7479N | .19 | SN74215N | 1.15 | SN74229N | .35  | SN74235N | 1.15 |
| SN7480N | .19 | SN74216N | 1.15 | SN74230N | .35  | SN74236N | 1.15 |
| SN7481N | .19 | SN74217N | 1.15 | SN74231N | .35  | SN74237N | 1.15 |
| SN7482N | .19 | SN74218N | 1.15 | SN74232N | .35  | SN74238N | 1.15 |
| SN7483N | .19 | SN74219N | 1.15 | SN74233N | .35  | SN74239N | 1.15 |
| SN7484N | .19 | SN74220N | 1.15 | SN74234N | .35  | SN74240N | 1.15 |
| SN7485N | .19 | SN74221N | 1.15 | SN74235N | .35  | SN74241N | 1.15 |
| SN7486N | .19 | SN74222N | 1.15 | SN74236N | .35  | SN74242N | 1.15 |
| SN7487N | .19 | SN74223N | 1.15 | SN74237N | .35  | SN74243N | 1.15 |
| SN7488N | .19 | SN74224N | 1.15 | SN74238N | .35  | SN74244N | 1.15 |
| SN7489N | .19 | SN74225N | 1.15 | SN74239N | .35  | SN74245N | 1.15 |
| SN7490N | .19 | SN74226N | 1.15 | SN74240N | .35  | SN74246N | 1.15 |
| SN7491N | .19 | SN74227N | 1.15 | SN74241N | .35  | SN74247N | 1.15 |
| SN7492N | .19 | SN74228N | 1.15 | SN74242N | .35  | SN74248N | 1.15 |
| SN7493N | .19 | SN74229N | 1.15 | SN74243N | .35  | SN74249N | 1.15 |
| SN7494N | .19 | SN74230N | 1.15 | SN74244N | .35  | SN74250N | 1.15 |
| SN7495N | .19 | SN74231N | 1.15 | SN74245N | .35  | SN74251N | 1.15 |
| SN7496N | .19 | SN74232N | 1.15 | SN74246N | .35  | SN74252N | 1.15 |
| SN7497N | .19 | SN74233N | 1.15 | SN74247N | .35  | SN74253N | 1.15 |
| SN7498N | .19 | SN74234N | 1.15 | SN74248N | .35  | SN74254N | 1.15 |
| SN7499N | .19 | SN74235N | 1.15 | SN74249N | .35  | SN74255N | 1.15 |
| SN7500N | .19 | SN74236N | 1.15 | SN74250N | .35  | SN74256N | 1.15 |

# 74LS00

|           |     |            |      |            |      |
|-----------|-----|------------|------|------------|------|
| SN74LS00N | .19 | SN74LS150N | .26  | SN74LS164N | 1.19 |
| SN74LS01N | .22 | SN74LS151N | 2.19 | SN74LS165N | .89  |
| SN74LS02N | .22 | SN74LS152N | .28  | SN74LS166N | 2.48 |
| SN74LS03N | .22 | SN74LS153N | .28  | SN74LS167N | 1.15 |
| SN74LS04N | .22 | SN74LS154N | .35  | SN74LS168N | 1.15 |
| SN74LS05N | .22 | SN74LS155N | .35  | SN74LS169N | 1.15 |
| SN74LS06N | .22 | SN74LS156N | .35  | SN74LS170N | 1.99 |
| SN74LS07N | .22 | SN74LS157N | .35  | SN74LS171N | .99  |
| SN74LS08N | .22 | SN74LS158N | .35  | SN74LS172N | .99  |
| SN74LS09N | .22 | SN74LS159N | .35  | SN74LS173N | .99  |
| SN74LS10N | .22 | SN74LS160N | .35  | SN74LS174N | .99  |
| SN74LS11N | .22 | SN74LS161N | .35  | SN74LS175N | .99  |
| SN74LS12N | .29 | SN74LS162N | .39  | SN74LS176N | 2.20 |
| SN74LS13N | .39 | SN74LS163N | .39  | SN74LS177N | 2.20 |
| SN74LS14N | .39 | SN74LS164N | .39  | SN74LS178N | 2.20 |
| SN74LS15N | .39 | SN74LS165N | .39  | SN74LS179N | 2.20 |
| SN74LS16N | .39 | SN74LS166N | .39  | SN74LS180N | 2.20 |
| SN74LS17N | .39 | SN74LS167N | .39  | SN74LS181N | 2.20 |
| SN74LS18N | .39 | SN74LS168N | .39  | SN74LS182N | 2.20 |
| SN74LS19N | .39 | SN74LS169N | .39  | SN74LS183N | 2.20 |
| SN74LS20N | .39 | SN74LS170N | .39  | SN74LS184N | 2.20 |
| SN74LS21N | .39 | SN74LS171N | .39  | SN74LS185N | 2.20 |
| SN74LS22N | .39 | SN74LS172N | .39  | SN74LS186N | 2.20 |
| SN74LS23N | .39 | SN74LS173N | .39  | SN74LS187N | 2.20 |
| SN74LS24N | .39 | SN74LS174N | .39  | SN74LS188N | 2.20 |
| SN74LS25N | .39 | SN74LS175N | .39  | SN74LS189N | 2.20 |
| SN74LS26N | .39 | SN74LS176N | .39  | SN74LS190N | 2.20 |
| SN74LS27N | .39 | SN74LS177N | .39  | SN74LS191N | 2.20 |
| SN74LS28N | .39 | SN74LS178N | .39  | SN74LS192N | 2.20 |
| SN74LS29N | .39 | SN74LS179N | .39  | SN74LS193N | 2.20 |
| SN74LS30N | .39 | SN74LS180N | .39  | SN74LS194N | 2.20 |
| SN74LS31N | .39 | SN74LS181N | .39  | SN74LS195N | 2.20 |
| SN74LS32N | .39 | SN74LS182N | .39  | SN74LS196N | 2.20 |
| SN74LS33N | .39 | SN74LS183N | .39  | SN74LS197N | 2.20 |
| SN74LS34N | .39 | SN74LS184N | .39  | SN74LS198N | 2.20 |
| SN74LS35N | .39 | SN74LS185N | .39  | SN74LS199N | 2.20 |
| SN74LS36N | .39 | SN74LS186N | .39  | SN74LS200N | 2.20 |
| SN74LS37N | .39 | SN74LS187N | .39  | SN74LS201N | 2.20 |
| SN74LS38N | .39 | SN74LS188N | .39  | SN74LS202N | 2.20 |
| SN74LS39N | .39 | SN74LS189N | .39  | SN74LS203N | 2.20 |
| SN74LS40N | .39 | SN74LS190N | .39  | SN74LS204N | 2.20 |
| SN74LS41N | .39 | SN74LS191N | .39  | SN74LS205N | 2.20 |
| SN74LS42N | .39 | SN74LS192N | .39  | SN74LS206N | 2.20 |
| SN74LS43N | .39 | SN74LS193N | .39  | SN74LS207N | 2.20 |
| SN74LS44N | .39 | SN74LS194N | .39  | SN74LS208N | 2.20 |
| SN74LS45N | .39 | SN74LS195N | .39  | SN74LS209N | 2.20 |
| SN74LS46N | .39 | SN74LS196N | .39  | SN74LS210N | 2.20 |
| SN74LS47N | .39 | SN74LS197N | .39  | SN74LS211N | 2.20 |
| SN74LS48N | .39 | SN74LS198N | .39  | SN74LS212N | 2.20 |
| SN74LS49N | .39 | SN74LS199N | .39  | SN74LS213N | 2.20 |
| SN74LS50N | .39 | SN74LS200N | .39  | SN74LS214N | 2.20 |

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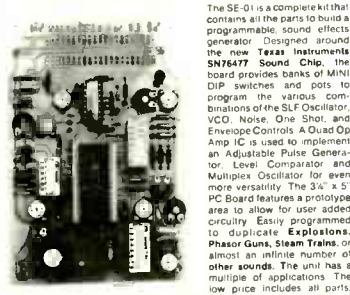
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# BULLET ELECTRONICS

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## Sound Effects Kit \$18.50



The SE-01 is a complete kit that contains all the parts to build a programmable sound effects generator. Designed around the new Texas Instruments SN76747 Sound Chip, the board provides banks of MINI DIP switches and pots to program the various combinations of the VLF Oscillator, VCO, Noise, One Shot, and Envelope Controls. A Quad Op Amp IC is used to implement an Adjustable Pulse Generator, Level Comparator and Multiplex Oscillator for even more versatility. The 3 1/2" x 5" PCB board features a prototype area to allow for user added circuitry. Easily programmed to duplicate Explosions, Phasors, Steam Trains, or almost an infinite number of other sounds. The unit has a multiple of applications. The low price includes all parts, assembly manual, programming charts, and detailed 76477 chip specifications. It runs on a 9V battery (not included). On board 100M $\Omega$  amp will drive a small speaker directly, or the unit can be connected to your stereo with incredible results! (Speaker not included). 76477 is included. Available separately for \$3.15 each.

## 7 Watt Audio Amp Kit \$6.95

SMALL, SINGLE HYBRID IC AND COMPONENTS FIT ON A 2" x 3" PCB BOARD (INCLUDED), RUNS ON 12VDC. GREAT FOR ANY PROJECT THAT NEEDS AN INEXPENSIVE AMP. LESS THAN 3% THD @ 5 WATTS. COMPATIBLE WITH SE-01 SOUND KIT.

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If you have trouble sleeping and you would like the rest of the neighborhood to share your misery then this little kit will be for you! There is no way to accurately describe the unearthly howls, screams and tones that come out of this kit. Four separate tone oscillators are mixed, cancelled and stepped at a varying rate. 10 Watts of crazy sounds. A great fun kit or a practical burglar alarm. Complete with PCB board and all necessary components less speaker. For 6-12 VDC. ORDER DA-02.

## New! 3TZ Time Zone Clock Kit

Microprocessor/ROM clock kit keeps local time (12 hour format), and 2 world time zones (24 hour format). Large 6" ORANGE readouts 10 min. ID timer for HAMS. Comes complete with attractive plastic case and wallplug XFMR.

- Quartz XTAL Timebase
- 3 Time Zones (Selectable)
- Feather-touch front panel switches
- Quartz XTAL Timebase
- 3 Time Zones (Selectable)
- Feather-touch front panel switches
- Quilted solder masked and plated PCB boards
- Seconds Reset/Hold feature

**\$54.40**

## SEE SPECIAL WINTER PRICES BELOW

### The Super Music Maker

REVISION 2  
**\$24.95**  
(Basic Kit)

Does not include speaker switches or 2708 ROM.

Now you can play hundreds of songs using the Bullet Super Music Maker. The unit features a single factory programmed microprocessor IC that comes with 20 pre-programmed short tunes. By adding the additional PROMS (2708's) the system can be expanded to play up to 1000 notes per PROM. Just think... a compact electronic instrument that will play dozens, hundreds or even thousands of selections of music. The kit comes with all electronic components (the PROM), and a drilled, plated and screened PCB Board which measures 4" x 4 1/2". The 7 watt amplifier section is on the same PCB board and drives an 8 ohm speaker (not included), from a whisper to ear splitting volume. Since the unit works on 12 VDC or 12 VAC, vehicle or portable operation is possible. What do you get for \$24.95? Everything but a speaker, transformer, case, switches, and PROM. Additional 2708 albums containing popular tunes are available for \$9.95 each or you can program your own PROMS using information provided with the kit instructions. Lists of available PROM albums are available on request. (Note: It is not possible to play chords or a melody with harmony simultaneously.)

- Envelope control gives decay to notes
- On board inverter allows single voltage (+12) operation

**OPTIONAL ACCESSORIES**

DIP Switches (One 8 pos., One 5 pos.) 2.00/each  
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Attractive Tan Plastic Case 6.50  
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- SPECIAL WINTER PRICES**
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| MICROPROCESSORS | RAM             | MEMORY       | INTERFACE     |
|-----------------|-----------------|--------------|---------------|
| 7801P ACCESSORS | 4027 (250K)     | \$4.25       |               |
| M-10            | \$9.20          | 6809 \$23.50 | 2101 (256K)   |
| 2.80A           | 9.50            | 8080A 4.50   | 2102 (1024x1) |
| 6502            | 7.84            | 8085A 5.70   | 2112 (256Kx4) |
| 6800            | 7.50            | 8035 5.50    | 2114          |
| 6802            | 1.46            | 8085 25.21   | 2112 4.50     |
| 8080A           | SUPPORT DEVICES | 2147 (4Kx1)  | 6.64          |
| 6520            | \$6.65          | 8251 \$4.90  | MISC          |
| 6522            | 9.95            | 8253 7.50    | 8282          |
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| 8726 | 2.15   | 8797    | 1.49   | 74LS243 | 1.79   | 74LS273 | 1.69   |
| 8728 | 2.30   | 74LS241 | 1.10   | 74LS244 | 1.10   | 74LS373 | 2.50   |
| 8795 | 1.49   |         |        |         |        |         |        |

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| 930 | DPST 4 pos w/cover | \$4.99 | 920 | SP 10 pos P.C. Rotary  | 7.81   |
| 932 | SPST 4 pos w/cover | 4.88   | 921 | 10 pos P.C. Rotary     | 6.81   |
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| SP15    | Pocket Size Volt-Ohm Milliammeter     | 19.95    |
| SP80    | Extra Sensitive Volt-Ohm Milliammeter | 40.95    |

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| RIBBON CABLE (Price per 10 feet)   | 20 pin \$5.00 | 25 pin \$ 6.30 | 26 pin \$ 6.45 | 34 pin \$8.30 |
|                                    | 37 pin \$9.50 | 40 pin \$10.00 | 50 pin \$13.00 |               |

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| D-SUBMINIATURE CONNECTORS | DE-9P \$1.65 | DA-15S \$3.10 | DC-37P \$3.85 | DD-50P \$4.75 |
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 10.0 Hz (600 MHz range)  
 Display: 9 digits 0.4" LED  
 Time base: Standard-10,000 mHz, 1.0 ppm 20-40°C.  
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Range: 20 Hz to 525 MHz  
 Sensitivity: Less than 50 MV to 150 MHz  
 Less than 150 MV to 500 MHz  
 Resolution: 1.0 Hz (5 MHz range)  
 10.0 Hz (50 MHz range)  
 100.0 Hz (500 MHz range)  
 Display: 7 digits 0.4" LED  
 Time base: 1.0 ppm TCXO 20-40°C  
 Power: 12 VAC @ 250 ma

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**SPECIFICATIONS:**

Range: 1 MHz to 500 MHz  
 Sensitivity: Less than 25 MV  
 Resolution: 100 Hz (slow gate)  
 1.0 KHz (fast gate)  
 Display: 7 digits, 0.4" LED  
 Time base: 2.0 ppm 20-40°C  
 Power: 5 VDC @ 200 ma

## 8 DIGITS 600 MHz \$159<sup>95</sup> WIRED



**SPECIFICATIONS:**

Range: 20 Hz to 600 MHz  
 Sensitivity: Less than 25 mv to 150 MHz  
 Less than 150 mv to 600 MHz  
 Resolution: 1.0 Hz (60 MHz range)  
 10.0 Hz (600 MHz range)  
 Display: 8 digits 0.4" LED  
 Time base: 2.0 ppm 20-40°C  
 Power: 110 VAC or 12 VDC

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CPU'S & SUPPORT CHIPS

Table of CPU and support chips: 8080, 8085, AMD2801, 8027, 8251, 8252, 8253, 8254, 8255, 8256, 8257, 8258, 8259, 8260, 8261, 8262, 8263, 8264, 8265, 8266, 8267, 8268, 8269, 8270, 8271, 8272, 8273, 8274, 8275, 8276, 8277, 8278, 8279, 8280, 8281, 8282, 8283, 8284, 8285, 8286, 8287, 8288, 8289, 8290, 8291, 8292, 8293, 8294, 8295, 8296, 8297, 8298, 8299, 8300, 8301, 8302, 8303, 8304, 8305, 8306, 8307, 8308, 8309, 8310, 8311, 8312, 8313, 8314, 8315, 8316, 8317, 8318, 8319, 8320, 8321, 8322, 8323, 8324, 8325, 8326, 8327, 8328, 8329, 8330, 8331, 8332, 8333, 8334, 8335, 8336, 8337, 8338, 8339, 8340, 8341, 8342, 8343, 8344, 8345, 8346, 8347, 8348, 8349, 8350, 8351, 8352, 8353, 8354, 8355, 8356, 8357, 8358, 8359, 8360, 8361, 8362, 8363, 8364, 8365, 8366, 8367, 8368, 8369, 8370, 8371, 8372, 8373, 8374, 8375, 8376, 8377, 8378, 8379, 8380, 8381, 8382, 8383, 8384, 8385, 8386, 8387, 8388, 8389, 8390, 8391, 8392, 8393, 8394, 8395, 8396, 8397, 8398, 8399, 8400, 8401, 8402, 8403, 8404, 8405, 8406, 8407, 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C/MOS

Table of C/MOS chips: 4001, 4002, 4003, 4004, 4005, 4006, 4007, 4008, 4009, 4010, 4011, 4012, 4013, 4014, 4015, 4016, 4017, 4018, 4019, 4020, 4021, 4022, 4023, 4024, 4025, 4026, 4027, 4028, 4029, 4030, 4031, 4032, 4033, 4034, 4035, 4036, 4037, 4038, 4039, 4040, 4041, 4042, 4043, 4044, 4045, 4046, 4047, 4048, 4049, 4050, 4051, 4052, 4053, 4054, 4055, 4056, 4057, 4058, 4059, 4060, 4061, 4062, 4063, 4064, 4065, 4066, 4067, 4068, 4069, 4070, 4071, 4072, 4073, 4074, 4075, 4076, 4077, 4078, 4079, 4080, 4081, 4082, 4083, 4084, 4085, 4086, 4087, 4088, 4089, 4090, 4091, 409



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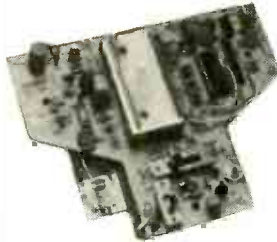
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New HY-GAIN printed circuit board assembly with PLL02A chip and 3 crystals. (Squelch pot, volume control and channel switch not included.) Boards sold as is, the way we bought them from the manufacturer. Board dimensions 6" x 6 1/2"

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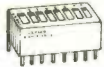
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Size 9.25 x 10.75  
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2 1/4" square, no shunt required.  
Easy-to-read dial.

Movements: 0-6, 0-10, 0-17

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3" Diam.,  
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**\$4.95/100' \$3.00/50'**

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Handle stores four blades  
2 single slot 5/32" & 3/32"  
1 Phillips 1 scratch awl  
6" long with one blade inserted  
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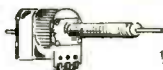
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1.5-20pF  
(ARCO PC-402)

**50c ea.**

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**5/\$1.00**

with On-Off  
1/4" hole mount,  
1/8" D shaft,  
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Primary - 115 vac  
Secondary - 32 v with  
24 v tap at 15 amps  
Dim. 4 1/2" h X 3 3/4" w X 4" deep



### SOLID GEL BATTERY

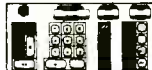
6 volt @ 8 a.h. with Charger



**\$14.95**

Epipower EP 680 may be charged constant voltage or constant current. Battery is self-contained and requires no maintenance. Connections made with quick connect lugs. All plastic case size 5 1/2" h x 2 3/4" w x 4 1/2" l, weight 4 lbs.

### TEXAS INSTRUMENT KEYBOARD



Has 3 slide switches, 26 different keys, key pad removable by 4 screws

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Part # Movement

J-60 7101 SPDT

L-3 7108 SPDT (momentary)

J-3 7201 DPDT (special large rocker)

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Edge Meter 250 UA, fits in 3/8" x 1 3/8" hole. Black background. Scale 1-20 Top, 0-5 Bottom.

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| VALUE/MFD | VOLTS  | DIAM./LGTH.     | PRICE             |
|-----------|--------|-----------------|-------------------|
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| 10,000    | @ 20V  | 1 1/2" x 5 3/4" | <b>\$3.00 ea.</b> |
| 2,700     | @ 25V  | 1 1/4" x 2 1/4" | <b>\$2.00 ea.</b> |
| 2,900     | @ 25V  | 1 1/4" x 2"     | <b>\$2.00 ea.</b> |
| 100,000   | @ 30V  | 3" x 5 1/2"     | <b>\$6.00 ea.</b> |
| 39,000    | @ 30V  | 1" x 5 3/4"     | <b>\$4.00 ea.</b> |
| 34,800    | @ 50V  | 3" x 5 1/2"     | <b>\$3.00 ea.</b> |
| 450       | @ 75V  | 1 1/4" x 2 1/4" | <b>\$2.00 ea.</b> |
| 500       | @ 100V | 1 1/2" x 3 1/4" | <b>\$2.00 ea.</b> |
| 50        | @ 450V | 1 1/4" x 2"     | <b>\$2.00 ea.</b> |

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MFG by Anderson Jacobson  
DAA Modem Model DC 230 with A-36 Telephone Coupler



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Rated 300 Baud, half or full duplex. DAA level adjustable 0 to -3, -4 to -5, -7 to -10, TTY and DAA outputs brought out to 15 pin Molex connectors. FSK oscillator sends 1070 Hz space and 1270 Hz mark. Receives 2025 Hz space and 2225 Hz mark. Telephone coupler has 4-ft. cord and plug. Size 4 1/4" W x 15 L x 3" Dp. designed to be recessed in desk or panel. Electronics in case, 6 3/4" W x 12 x 2 3/4" Dp. with 8-ft. 3-wire U-ground cord and plug. Operates on 115 vac, 50/60 Hz, 1/2 Amp. Supplied with connection sheet. Removed from equipment, excellent condition, guaranteed.

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2.2 uF @ 25V **\$1.00**  
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25 uF @ 25V **\$2.00**  
3 uF @ 50V **\$2.00**  
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10 uF @ 50V **\$2.00**  
250 uF @ 25V **\$2.00**  
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### MODEM CABLE ASSEMBLIES

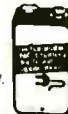
**\$5.50 ea.**



| Conn & Hood | 22 AWG # Cond | Length |
|-------------|---------------|--------|
| 25 P        | 14            | 15'    |
| 25 S        | 10            | 17'    |

### 9 VOLT NiCd RECHARGEABLE BATTERY

NEW. Replaces the popular 9V Transistor Battery.



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### MAHOGANY PROJECT BOX

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4 3/8" w x 7 3/8" l x 3/4" to 1 1/2" h

Has a lip for recessed face plate and a felt bottom

### POWER SUPPLY

+ 12 vdc .1 amps  
+ 5 vdc .4 amps



**\$3.95 ea.**

### IC SOCKETS GOLD-PLATED WIRE WRAP

14 pin **40c ea.**

16 pin **45c ea.**



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MFG By Rotron Inc.  
3 Blades 4 1/4" Square  
USED

110 VAC **\$5.95 ea.**

NEW

230 VAC Model MU3A1

**\$12.00 ea.**

### NEW SPRITE FAN

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Model SU2A5,  
115v AC, .19 amps.  
(Impedance protected.)  
3 1/4" x 3 1/4" x 1 1/4"

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### 7' POWER CORD HEWLETT PACKARD TYPE



Molded 3 Prong Plug with molded receptacle  
Belden 16 AWG

**\$3.00 ea.**

### 24-Volt POWER SUPPLY 5.4 AMPS

MFG by ACDC Electronics Inc.  
Model OEM 24N5-4-1



Input 105-125 vac 50/60 Hz. Has volt adj and O.L. adj. Output terminals contain +, out, - sen.

- sen, - out, ac neut, ac line and GND. 13 LBS.

**\$45.00**

**TERMS:** All material guaranteed unless otherwise stated. If you are not satisfied with our product, it may be returned within 10 days for a refund (less shipping). Please add \$4.00 for shipping and handling on all orders. COD's accepted for orders totaling \$50 or more. All orders shipped UPS unless otherwise specified. Florida residents please add 4% sales tax. Minimum order, \$15.00. Foreign orders - US funds only, add 20% for shipping and handling.

# 16K Memory

4116-200ns **8/15.95**

ALL MERCHANDISE 100% GUARANTEED!

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## EPROMS

|         |          |                      | Each  | 8 pcs |
|---------|----------|----------------------|-------|-------|
| 1702    | 256 x 8  | (1ns)                | 4.95  | 4.50  |
| 2708    | 1024 x 8 | (450ns)              | 2.99  | 2.75  |
| 2758    | 1024 x 8 | (5V) (450ns)         | 9.95  | 8.95  |
| TMS2516 | 2048 x 8 | (5V) (450ns)         | 6.95  | 5.95  |
| 2716    | 2048 x 8 | (5V) (450ns)         | 5.50  | 4.95  |
| 2716-1  | 2048 x 8 | (5V) (350ns)         | 9.00  | 8.50  |
| TMS2716 | 2048 x 8 | (450ns)              | 9.95  | 8.95  |
| TMS2532 | 4096 x 8 | (5V) (450ns)         | 12.95 | 11.95 |
| 2732    | 4096 x 8 | (5V) (450ns) (200ns) |       | CALL  |
| 2764    | 8192 x 8 | (5V) (450ns)         |       | CALL  |

## DYNAMIC RAMS

|          |            |         | 100 pcs |      |
|----------|------------|---------|---------|------|
| 4027     | 4096 x 1   | (250ns) | 2.50    | 2.00 |
| 4116-120 | 16,384 x 1 | (120ns) | 8/29.95 | CALL |
| 4116-150 | 16,384 x 1 | (150ns) | 8/18.95 | 1.95 |
| 4116-200 | 16,384 x 1 | (200ns) | 8/15.95 | 1.80 |
| 4116-300 | 16,384 x 1 | (300ns) | 8/14.95 | 1.75 |
| 4164     | 64,536 x 1 | (200ns) |         | CALL |

## STATIC RAMS

|            |          |                         | 100 pcs |      |
|------------|----------|-------------------------|---------|------|
| 2101       | 256 x 4  | (450ns)                 | 1.95    | 1.85 |
| 2102-1     | 1024 x 1 | (450ns)                 | .89     | .85  |
| 21L02-4    | 1024 x 1 | (L-) (450ns)            | 1.29    | 1.15 |
| 21L02-2    | 1024 x 1 | (LP) (250ns)            | 1.69    | 1.55 |
| 2111       | 256 x 4  | (450ns)                 | 2.99    | 2.49 |
| 2112       | 256 x 4  | (450ns)                 | 2.99    | 2.79 |
| 2114       | 1024 x 4 | (450ns)                 | 8/16.95 | 1.95 |
| 2114L-2    | 1024 x 4 | (L-) (200ns)            | 8/19.95 | 2.35 |
| 2114L-3    | 1024 x 4 | (L-) (300ns)            | 8/18.95 | 2.25 |
| 2114L-4    | 1024 x 4 | (L-) (450ns)            | 8/17.95 | 2.10 |
| 2147       | 4096 x 1 | (5ns)                   | 9.95    | CALL |
| TMS4044-4  | 4096 x 1 | (450ns)                 | 3.49    | 3.25 |
| TMS4044-3  | 4096 x 1 | (300ns)                 | 3.99    | 3.75 |
| TMS40L44-2 | 4096 x 1 | (LP) (200ns)            | 4.49    | 4.25 |
| TMM2016    | 2048 x 8 | (200ns) (150ns)         |         | CALL |
| HM6116     | 2048 x 8 | (200ns) (150ns) (120ns) |         | CALL |

LP = LOW POWER

## CRYSTALS

|            |      |
|------------|------|
| 32.768 KHZ | 3.95 |
| 1.0 MHZ    | 4.95 |
| 1.8432     | 4.95 |
| 2.0        | 3.95 |
| 2.097152   | 3.95 |
| 2.4576     | 3.95 |
| 3.2768     | 3.95 |
| 3.579545   | 3.95 |
| 4.0        | 3.95 |
| 5.0        | 3.95 |
| 5.0688     | 3.95 |
| 5.185      | 3.95 |
| 5.7143     | 3.95 |
| 6.5536     | 3.95 |
| 8.0        | 3.95 |
| 10.0       | 3.95 |
| 14.31818   | 3.95 |
| 18.0       | 3.95 |
| 18.432     | 3.95 |
| 20.0       | 3.95 |
| 22.1184    | 3.95 |
| 32.0       | 3.95 |

## MISC.

|          |       |
|----------|-------|
| AY5-2376 | 12.50 |
| 11C90    | 13.95 |
| XR2206   | 4.95  |
| 3242     | 7.95  |
| 3480     | 9.00  |
| MC4024   | 3.95  |
| MC4044   | 4.50  |
| 7103     | 9.50  |
| 7106     | 9.95  |
| 7107     | 12.95 |
| 76477    | 3.95  |
| 8038     | 3.95  |
| 95H90    | 7.99  |
| 9602     | 1.50  |

## DISC CONTROLLERS

|      |       |
|------|-------|
| 1771 | 24.95 |
| 1791 | 36.95 |
| 1793 | 44.95 |
| 1797 | 54.95 |

## UARTS

|          |      |
|----------|------|
| AY3-1014 | 6.95 |
| AY5-1013 | 3.95 |
| TR1602   | 4.95 |
| IM6402   | 7.95 |

## INTERFACE

|        |      |
|--------|------|
| 8T26   | 1.69 |
| 8T28   | 2.49 |
| 8T95   | .99  |
| 8T96   | .99  |
| 8T97   | .99  |
| 8T98   | .99  |
| DM8131 | 2.95 |
| DS8836 | 1.29 |

## CLOCK CIRCUITS

|         |       |
|---------|-------|
| MM5369  | 3.95  |
| MM5375  | 3.95  |
| MSM5832 | 7.45  |
| 7207    | 7.50  |
| 7208    | 15.95 |

## CONVERTERS

|           |      |
|-----------|------|
| MC1408 L8 | 4.95 |
| DAC-0800  | 4.95 |
| ADC-0804  | 4.95 |

## March Specials

|           |      |
|-----------|------|
| Z-80A-CPU | 6.00 |
| Z-80A-PIO | 6.00 |
| 8214      | 2.95 |
| 8216      | 1.50 |
| 6800      | 4.95 |
| 6810      | 3.95 |

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By Texas Instruments - not equivalent part number made by another manufacturer as sold by others:

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Specials end March 28, 1982  
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| 6504   | 6.95  |
| 6505   | 8.95  |
| 6507   | 9.95  |
| 6520   | 4.35  |
| 6522   | 9.95  |
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|            |       |
|------------|-------|
| Z80-CPU    | 8.95  |
| Z80A-CPU   | 6.00  |
| Z80-PIO    | 6.50  |
| Z80A-PIO   | 6.00  |
| Z80-CTC    | 5.95  |
| Z80A-CTC   | 8.65  |
| Z80-DART   | 15.25 |
| Z80A-DART  | 18.75 |
| Z80-DMA    | 17.50 |
| Z80A-DMA   | 27.50 |
| Z80-S10/0  | 23.95 |
| Z80A-S10/0 | 28.95 |
| Z80-S10/1  | 23.95 |
| Z80A-S10/1 | 28.95 |
| Z80-S10/2  | 23.95 |
| Z80A-S10/2 | 28.95 |
| Z80-S10/9  | 17.95 |
| Z80A-S10/9 | 22.95 |
| Z80B-CPU   | 18.95 |
| Z80B-CTC   | 17.95 |
| Z80B-PIO   | 17.95 |
| Z8671      | 39.95 |
| Z6132      | 34.95 |

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|        |      |         |      |         |      |         |      |
|--------|------|---------|------|---------|------|---------|------|
| 74LS00 | .25  | 74LS85  | 1.15 | 74LS166 | 2.40 | 74LS293 | 1.85 |
| 74LS01 | .25  | 74LS86  | .40  | 74LS168 | 1.75 | 74LS295 | 1.05 |
| 74LS02 | .25  | 74LS90  | .65  | 74LS169 | 1.75 | 74LS298 | 1.20 |
| 74LS03 | .25  | 74LS91  | .89  | 74LS170 | 1.75 | 74LS324 | 1.75 |
| 74LS04 | .25  | 74LS92  | .70  | 74LS173 | .80  | 74LS352 | 1.55 |
| 74LS05 | .25  | 74LS93  | .65  | 74LS174 | .95  | 74LS353 | 1.55 |
| 74LS08 | .35  | 74LS94  | .65  | 74LS175 | .95  | 74LS363 | 1.35 |
| 74LS10 | .25  | 74LS95  | .85  | 74LS181 | 2.15 | 74LS364 | 1.95 |
| 74LS11 | .35  | 74LS96  | .95  | 74LS189 | 9.95 | 74LS365 | .95  |
| 74LS12 | .35  | 74LS97  | .40  | 74LS190 | 1.00 | 74LS366 | .95  |
| 74LS13 | .45  | 74LS109 | .40  | 74LS191 | 1.00 | 74LS367 | .70  |
| 74LS14 | 1.00 | 74LS112 | .45  | 74LS192 | .85  | 74LS368 | .70  |
| 74LS15 | .35  | 74LS113 | .45  | 74LS193 | .95  | 74LS373 | .99  |
| 74LS20 | .25  | 74LS114 | .50  | 74LS194 | 1.00 | 74LS374 | 1.75 |
| 74LS21 | .35  | 74LS122 | .45  | 74LS195 | .95  | 74LS377 | 1.45 |
| 74LS22 | .25  | 74LS123 | .95  | 74LS196 | .85  | 74LS378 | 1.18 |
| 74LS26 | .35  | 74LS124 | 2.99 | 74LS197 | .85  | 74LS379 | 1.35 |
| 74LS27 | .35  | 74LS125 | .95  | 74LS221 | 1.20 | 74LS385 | 1.90 |
| 74LS28 | .35  | 74LS126 | .85  | 74LS240 | .99  | 74LS386 | .65  |
| 74LS30 | .25  | 74LS136 | .55  | 74LS241 | .99  | 74LS390 | 1.90 |
| 74LS32 | .35  | 74LS137 | .99  | 74LS242 | 1.85 | 74LS393 | 1.90 |
| 74LS33 | .55  | 74LS138 | .75  | 74LS243 | 1.85 | 74LS395 | 1.65 |
| 74LS37 | .55  | 74LS139 | .75  | 74LS244 | .99  | 74LS399 | 1.70 |
| 74LS38 | .35  | 74LS145 | 1.20 | 74LS245 | 1.90 | 74LS424 | 2.95 |
| 74LS40 | .35  | 74LS147 | 2.49 | 74LS247 | .76  | 74LS447 | .37  |
| 74LS42 | .55  | 74LS148 | 1.35 | 74LS248 | 1.25 | 74LS490 | 1.95 |
| 74LS47 | .75  | 74LS151 | .75  | 74LS249 | .99  | 74LS668 | 1.69 |
| 74LS48 | .75  | 74LS153 | .75  | 74LS251 | 1.30 | 74LS669 | 1.89 |
| 74LS49 | .75  | 74LS154 | 2.35 | 74LS253 | .85  | 74LS670 | 2.20 |
| 74LS51 | .25  | 74LS155 | 1.15 | 74LS257 | .85  | 74LS674 | 9.65 |
| 74LS54 | .35  | 74LS156 | .95  | 74LS258 | .85  | 74LS682 | 3.20 |
| 74LS55 | .35  | 74LS157 | .75  | 74LS259 | 2.85 | 74LS683 | 2.30 |
| 74LS63 | 1.25 | 74LS158 | .75  | 74LS260 | .65  | 74LS684 | 2.40 |
| 74LS73 | .40  | 74LS159 | .90  | 74LS266 | .55  | 74LS685 | 2.40 |
| 74LS74 | .45  | 74LS161 | .95  | 74LS273 | 1.65 | 74LS688 | 2.40 |
| 74LS75 | .50  | 74LS162 | .95  | 74LS275 | 3.35 | 74LS689 | 2.40 |
| 74LS76 | .40  | 74LS163 | .95  | 74LS279 | .55  | 81LS95  | 1.69 |
| 74LS78 | .50  | 74LS164 | .95  | 74LS280 | 1.98 | 81LS96  | 1.69 |
| 74LS83 | .75  | 74LS165 | .95  | 74LS283 | 1.00 | 81LS97  | 1.69 |
|        |      |         |      | 74LS290 | 1.25 | 81LS98  | 1.69 |

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# 8/4.95 ea.

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| 8741    | 39.95 |
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| 8755    | 44.95 |

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|        |       |
|--------|-------|
| 8202   | 45.00 |
| 8205   | 3.50  |
| 8212   | 1.85  |
| 8214   | 3.85  |
| 8216   | 1.80  |
| 8224   | 2.50  |
| 8226   | 1.80  |
| 8228   | 4.90  |
| 8237   | 19.95 |
| 8238   | 4.95  |
| 8239   | 4.85  |
| 8243   | 4.45  |
| 8250   | 14.95 |
| 8251   | 4.75  |
| 8253   | 9.25  |
| 8253-5 | 9.85  |
| 8255   | 4.75  |
| 8255-5 | 5.25  |
| 8257   | 8.75  |
| 8259   | 6.90  |
| 8272   | 39.95 |
| 8275   | 29.95 |
| 8279   | 9.50  |
| 8279-5 | 10.50 |
| 8282   | 6.65  |
| 8283   | 6.65  |
| 8284   | 5.70  |
| 8286   | 6.65  |
| 8287   | 6.50  |
| 8288   | 25.00 |
| 8289   | 49.95 |

### TV CIRCUITS

|        |      |
|--------|------|
| MC1330 | 1.89 |
| MC1350 | 1.29 |
| MC1358 | 1.79 |
| LM380  | 1.29 |
| LM386  | 1.50 |
| LM565  | .99  |
| LM741  | .29  |
| LM1310 | 2.90 |
| LM1800 | 2.99 |
| LM1889 | 1.49 |



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|                 |           |
|-----------------|-----------|
| 1-99            | 100       |
| 8 pin ST        | .13 .11   |
| 14 pin ST       | .15 .12   |
| 16 pin ST       | .17 .13   |
| 16 pin ST       | .20 .18   |
| 20 pin ST       | .29 .27   |
| 22 pin ST       | .30 .27   |
| 24 pin ST       | .30 .27   |
| 26 pin ST       | .40 .32   |
| 40 pin ST       | .49 .39   |
| ST = SOLDERTAIL |           |
| 8 pin WW        | .59 .49   |
| 14 pin WW       | .69 .52   |
| 16 pin WW       | .69 .58   |
| 18 pin WW       | .99 .90   |
| 20 pin WW       | 1.09 .98  |
| 22 pin WW       | 1.39 1.28 |
| 24 pin WW       | 1.49 1.35 |
| 23 pin WW       | 1.69 1.49 |
| 40 pin WW       | 1.99 1.80 |
| WW = WIREWRAP   |           |

### CONNECTORS

|              |      |
|--------------|------|
| FS232 MALE   | 3.25 |
| FS232 FEMALE | 3.75 |
| FS232 HOOD   | 1.25 |
| S-100 ST     | 3.95 |
| S-100 WW     | 4.95 |

### DIP SWITCHES

|            |     |
|------------|-----|
| 4 POSITION | .85 |
| 5 POSITION | .90 |
| 6 POSITION | .90 |
| 7 POSITION | .95 |
| 6 POSITION | .95 |

### 6800

|       |       |
|-------|-------|
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| 6802  | 10.95 |
| 6808  | 9.95  |
| 6809  | 24.95 |
| 6809E | 29.95 |
| 6810  | 4.60  |
| 6820  | 4.95  |
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| 6834  | 16.95 |
| 6840  | 14.95 |
| 6843  | 42.95 |
| 6844  | 44.95 |
| 6845  | 16.95 |
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| 6850  | 4.75  |
| 6852  | 5.75  |
| 6860  | 10.95 |
| 6862  | 11.95 |
| 6875  | 6.95  |
| 6880  | 2.95  |
| 68B00 | 10.95 |
| 68B21 | 12.95 |
| 68B50 | 12.95 |

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|                     |        |
|---------------------|--------|
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| PE-14T (with timer) | 108.50 |
| PE-24T (with timer) | 154.50 |

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| 2N2222         | .25     | 50/10.99  |
| 2N2907         | .25     | 50/10.99  |
| 2N3055         | .79     | 10/ 6.99  |
| 2N3904         | 10/1.00 | 100/ 8.99 |
| 2N3906         | 10/1.00 | 100/ 8.99 |
| 1N4148 (1N914) |         | 10/ 1.00  |
| 1N4004         |         | 25/ 1.00  |

### VOLTAGE REG's

|        |      |        |      |
|--------|------|--------|------|
| 7805T  | .79  | 7905T  | .89  |
| 7808T  | .99  | 7912T  | .89  |
| 7812T  | .79  | 7915T  | 1.19 |
| 7815T  | .99  | 7924T  | 1.19 |
| 7824T  | .99  |        |      |
| 7805K  | 1.39 | 7905K  | 1.49 |
| 7812K  | 1.39 | 7912K  | 1.49 |
| 7815K  | 1.39 | 79LO5  | .79  |
| 78LO5  | .69  | 79L12  | .79  |
| 78L12  | .69  | 79L15  | .79  |
| 78L15  | .69  |        |      |
| LM309K | 1.49 | LM317K | 3.95 |
| LM317T | 1.95 | LM323K | 4.95 |
|        |      | LM337K | 3.95 |

T = TO-220 K = TO-3 L = TO-92

### LINEAR

|         |      |
|---------|------|
| LM301V  | .34  |
| LM308V  | .98  |
| LM309K  | 1.49 |
| LM311   | .54  |
| LM317T  | 1.95 |
| LM317K  | 3.35 |
| LM318   | 1.49 |
| LM323K  | 4.35 |
| LM324   | .59  |
| LM337K  | 3.95 |
| LM339   | .99  |
| LM377   | 2.29 |
| LM380   | 1.29 |
| LM386V  | 1.50 |
| LM555V  | .39  |
| LM556   | .69  |
| LM565   | .99  |
| LM566V  | 1.49 |
| LM567V  | 1.29 |
| LM723   | .49  |
| LM733   | .98  |
| LM741V  | .29  |
| LM747   | .79  |
| LM748V  | .59  |
| LM1310  | 2.90 |
| MC1330V | 1.89 |
| MC1350V | 1.29 |
| MC1358  | 1.79 |
| LM1414  | 1.59 |
| LM1458V | .69  |
| LM1488  | .99  |
| LM1489  | .99  |
| LM1800  | 2.99 |
| LM1889  | 2.49 |
| LM3900  | .59  |
| LM3909V | .98  |
| LM3914  | 3.95 |
| LM3915  | 3.95 |
| LM3916  | 3.95 |
| 75451V  | .39  |
| 75452V  | .39  |
| 75453V  | .39  |

### 7400 SERIES

|      |     |       |      |       |      |       |       |
|------|-----|-------|------|-------|------|-------|-------|
| 7400 | .19 | 7451  | .23  | 74136 | .50  | 74186 | 18.50 |
| 7401 | .19 | 7453  | .23  | 74141 | .65  | 74190 | 1.15  |
| 7402 | .19 | 7454  | .23  | 74142 | 2.95 | 74191 | 1.15  |
| 7403 | .19 | 7460  | .23  | 74143 | 2.95 | 74192 | .79   |
| 7404 | .19 | 7470  | .35  | 74144 | 2.95 | 74193 | .79   |
| 7405 | .22 | 7472  | .29  | 74145 | .60  | 74194 | .85   |
| 7406 | .22 | 7473  | .34  | 74147 | 1.75 | 74195 | .85   |
| 7407 | .22 | 7474  | .35  | 74148 | 1.20 | 74196 | .79   |
| 7408 | .24 | 7475  | .49  | 74150 | 1.35 | 74197 | .75   |
| 7409 | .19 | 7476  | .35  | 74151 | .65  | 74198 | 1.35  |
| 7410 | .19 | 7480  | .59  | 74152 | .65  | 74199 | 1.35  |
| 7411 | .25 | 7481  | 1.10 | 74153 | .55  | 74221 | 1.35  |
| 7412 | .30 | 7482  | .95  | 74154 | 1.40 | 74246 | 1.35  |
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| 7485     | 74LS85     | 74S85     | 1.00   |
| 7486     | 74LS86     | 74S86     | 1.00   |
| 7487     | 74LS87     | 74S87     | 1.00   |
| 7488     | 74LS88     | 74S88     | 1.00   |
| 7489     | 74LS89     | 74S89     | 1.00   |
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| 7497     | 74LS97     | 74S97     | 1.00   |
| 7498     | 74LS98     | 74S98     | 1.00   |
| 7499     | 74LS99     | 74S99     | 1.00   |
| 7500     | 74LS100    | 74S100    | 1.00   |

## TEXAS INSTRUMENTS I.C. SOCKETS

**Solder Tail Single Board Dip Sockets**  
 Body — 94 V. polyimide with Copper Alloy contacts. Accommodates standard IC leads up to 0.014" thick and 0.020" wide. Contact is designed and limited to the underside to trap the broad "flange" of the IC case, allowing for "pop" insertion and high retention force. Socket is designed to achieve maximum density on boards.

**TIN Plated Solder Tail Single Board Low Profile Dip Sockets**  
 Body — 94 V. polyimide with Copper Alloy contacts. Accommodates standard IC leads up to 0.014" thick and 0.020" wide. Contact is designed and limited to the underside to trap the broad "flange" of the IC case, allowing for "pop" insertion and high retention force. Socket is designed to achieve maximum density on boards.

**GOLD Wire Solder Tail Single Board Low Profile Dip Sockets**  
 Body — 94 V. polyimide with Copper Alloy contacts. Accommodates standard IC leads up to 0.014" thick and 0.020" wide. Contact is designed and limited to the underside to trap the broad "flange" of the IC case, allowing for "pop" insertion and high retention force. Socket is designed to achieve maximum density on boards.

**WIRE WRAP DIP SOCKETS**  
 Standard configurations. Universal mounting and wire wrap compatibility. Contact width adjustable to 0.131" for use with standard wire wrap wire. Wire wrap wire is held in place by a 0.010" wide groove. All sockets are designed to achieve maximum density on boards.

**TIN PLATED WIRE WRAP DIP SOCKETS**  
 Standard configurations. Universal mounting and wire wrap compatibility. Contact width adjustable to 0.131" for use with standard wire wrap wire. Wire wrap wire is held in place by a 0.010" wide groove. All sockets are designed to achieve maximum density on boards.

**GOLD WIRE WRAP DIP SOCKETS**  
 Standard configurations. Universal mounting and wire wrap compatibility. Contact width adjustable to 0.131" for use with standard wire wrap wire. Wire wrap wire is held in place by a 0.010" wide groove. All sockets are designed to achieve maximum density on boards.

## TEXAS INSTRUMENTS GOLD EDGEBOARD CONNECTORS

**RELAY COST-EFFECTIVE CONTACT CONNECTORS**  
 (All Wire Wraps to be soldered into contact holes) — Copper plated, conformal surface design.

**WIRE SERIES 100'S 200'S EDGEBOARD CONNECTORS**  
 Standard configurations. Universal mounting and wire wrap compatibility. Contact width adjustable to 0.131" for use with standard wire wrap wire. Wire wrap wire is held in place by a 0.010" wide groove. All sockets are designed to achieve maximum density on boards.

**WIRE SERIES 133'S 250'S EDGEBOARD CONNECTORS**  
 Standard configurations. Universal mounting and wire wrap compatibility. Contact width adjustable to 0.131" for use with standard wire wrap wire. Wire wrap wire is held in place by a 0.010" wide groove. All sockets are designed to achieve maximum density on boards.

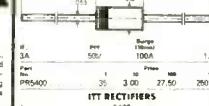
**WIRE SERIES 156'S 200'S EDGEBOARD CONNECTORS**  
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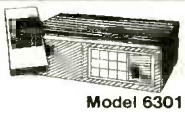
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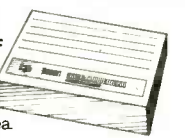
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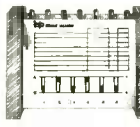
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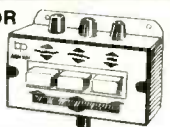
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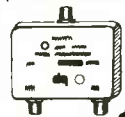
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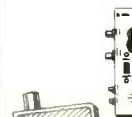


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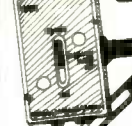
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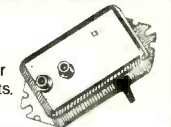


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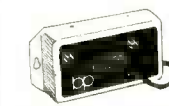


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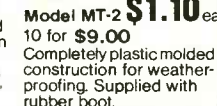


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| SN7445N | 84 | SN74174N | 88  | 74990 | 1.45 |        |      |
| SN7451N | 19 | SN74175N | 79  |       |      |        |      |
| SN7454N | 19 | SN74180N | 75  |       |      |        |      |
| SN7474N | 27 | SN74181N | 115 |       |      |        |      |
| SN7475N | 35 | SN74383N | 106 |       |      |        |      |

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|         |    |         |     |           |      |             |       |
|---------|----|---------|-----|-----------|------|-------------|-------|
| 74LS00  | 28 | 74LS158 | 89  | 2102      | .85  | 1103A       | .75   |
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| 74LS03  | 28 | 74LS162 | 88  | 8038      | 2.95 | Floppy disk | w/... |
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| 74LS08  | 29 | 74LS165 | 86  | 1488      | .95  | TMS4400     | 1.40  |
| 74LS09  | 28 | 74LS169 | 156 | 1489      | 1.30 | MC4008P     | 1.50  |
| 74LS10  | 28 | 74LS170 | 175 | 8726      | 1.30 | MC4026      | 1.55  |
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| 74LS20  | 22 | 74LS175 | 85  | 8216      | 1.95 | D3001       | 1.95  |
| 74LS21  | 26 | 74LS190 | 85  | 8218      | .85  | D3002       | 1.95  |
| 74LS26  | 40 | 74LS191 | 125 | 8216      | .85  |             |       |
| 74LS27  | 17 | 74LS195 | 86  | 2102      | .85  |             |       |
| 74LS28  | 37 | 74LS197 | 75  | 4508S     | .95  |             |       |
| 74LS30  | 29 | 74LS221 | 125 | 8038      | 2.95 |             |       |
| 74LS32  | 31 | 74LS240 | 165 | MS565     | .27  |             |       |
| 74LS38  | 31 | 74LS241 | 165 | AYS-1013A | 4.25 |             |       |
| 74LS42  | 83 | 74LS243 | 156 | 1488      | .95  |             |       |
| 74LS48  | 77 | 74LS244 | 156 | 1489      | 1.30 |             |       |
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| 74LS93  | 65 | 74LS259 | 195 | 2102      | .85  |             |       |
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| 74LS110 | 45 | 74LS278 | 45  | MS565     | .27  |             |       |
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| 74LS123 | 89 | 74LS293 | 195 | 1488      | .95  |             |       |
| 74LS125 | 89 | 74LS386 | 86  | 1489      | 1.30 |             |       |
| 74LS126 | 79 | 74LS387 | 75  | 8726      | 1.30 |             |       |
| 74LS138 | 64 | 74LS373 | 145 | 8212      | 1.95 |             |       |
| 74LS139 | 59 | 74LS376 | 145 | 8216      | 1.95 |             |       |
| 74LS151 | 49 | 74LS377 | 125 | 8218      | .85  |             |       |
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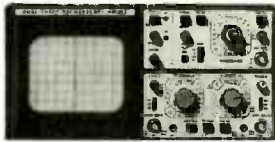
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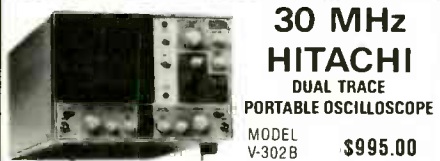
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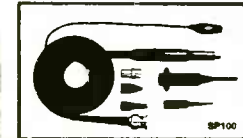
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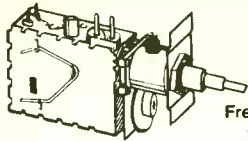
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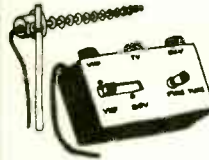
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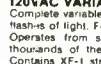
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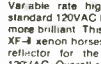
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**EXECUTIVE DECISION MAKER KIT**  
Here's another easy to build kit which is fun to use. Each time you need to make an "important" decision just operate the switch and one of two neon lamps will stay on. Features green "yes" lamp and orange "no" lamp. Operates from standard 120VAC. Size of board: 2" x 1".  
C4510 \$3.75



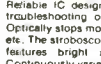
**3 CHANNEL COLOR ORGAN**  
Very popular 3 channel color organ causes lights of your choice to flash to the beat of music. Has 3 different filter stages for low, medium and high notes. Features level control and 3 separate AC outlets to connect Christmas lights, lamps, etc. Operates from 120VAC. Size of board: 3" x 5".  
C4530 \$8.50



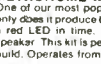
**AUDIO OSCILLATOR KIT**  
Very useful for demonstration or testing speakers, earphones, etc. Kit produces pleasant tone rich in harmonics. Features output transformer for coupling to speaker of your choice. Two transistor circuit is simple to construct. Operates from 9V battery. Requires speaker. Size of board: 2" x 1".  
C4511 \$3.00



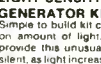
**STROBOSCOPE KIT**  
Reliable IC design kit for use in physics experiments, troubleshooting or demonstrating optical phenomena. Optically stops motion of gears, wheels, pulleys, flywheels, etc. The stroboscope operates from standard 120VAC and features bright xenon flash tube and IC design. Continuously variable flash rate from 100-5000 RPM. Size of board: 3 1/2" x 4 1/2".  
C-070 \$29.95




**METRONOME WITH SOUND AND LIGHT**  
One of our most popular kits now has a new feature. Not only does it produce beats in precise time but also it flashes a red LED in time. Features variable control and small speaker. This kit is perfect for music practice and is easy to build. Operates from 9V battery. Size of board: 1" x 2".  
C4533 \$3.50



**LIGHT SENSITIVE SOUND GENERATOR KIT**  
Simple to build kit creates a tone which varies depending on amount of light. Uses CDS cell and IC circuitry to provide this unusual effect. In total darkness the unit is silent, as light increases the unit goes from a clicking sound to a loud tone. Uses 2" speaker and operates from 9V battery.  
C4164 \$4.95




**DIGITAL POWER SUPPLY KIT**  
Regulated power supply, perfect for TTL or CMOS circuits. Regulated output voltage is 5VDC. Maximum output current is 500 amp. Features fused input, neon indicator light and IC regulator. Kit uses heavy duty transformer for trouble free performance. Operates from standard 120VAC. Size of board: 2" x 4".  
C4430 \$6.50



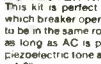
**46WS PHOTO STROBE FLASH KIT**  
Here's your chance to make a quality high power strobe flash for your camera. Can also be used as the master strobe with any of the slave kits. Features quality long life straight flashtube, heavy duty photoflash capacitor, neon ready light, transistorized inverter circuitry and shutter cord for connection to camera. Operates from 4.5VDC to 6VDC. Size of board: 3" x 2 1/2".  
C4512 \$9.95



**100WS SLAVE STROBE AC KIT**  
This kit is similar in operation to the DC slave strobe, however, this unit is more than double the light power output. Features heavy duty horseshoe flashtube, two heavy duty photoflash caps, neon ready light, solar cell sensor, and manual test button. Operates from 120VAC. Size of board: 3 1/2" x 4". NOTE: This kit is NOT for beginners since due to the power of the flash, hazardous potentials are present.  
C4491 \$34.95



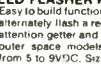
**AC TESTER KIT**  
This kit is perfect for testing AC outlets or determining which breaker operates a particular outlet! There's no need to be in the same room as the unit emits a penetrating tone as long as AC is present. Features green "ON" light and piezoelectric tone alert in a compact unit. Size of board: 2" x 1 1/2".  
C4485 \$4.50



**DUAL LAMP FLASHER KIT**  
Ultra miniature lamp flasher kit uses tiny grain of wheat bulbs and IC to flash 2 bulbs at the same time or alternating. Unit produces bright flashes and can be used on model planes, boats, attention getters, warning lights, etc. Operates from 9V battery. Size of board: 1 1/2" x 8".  
C4487 \$2.50



**LED FLASHER KIT**  
Easy to build functional kit uses the amazing 555 timer IC to alternately flash a red and green led. The kit makes a great attention getter and can be used in robots, warning lights, outer space models, convention badges, etc. Operates from 5 to 9VDC. Size of board: 1 1/2" x 1 1/2".  
C3287 \$2.49



**SIGNAL INJECTOR KIT**  
Signal injectors are useful for troubleshooting all types of radios, amplifiers, tuners, etc. This simple to build transistorized kit produces an output signal rich in harmonics. Every tool kit and test bench should have one of these. Small size allows use of compact cases if desired. Operates from 3VDC. Size of board: 5" x 1 1/2".  
C4513 \$3.00



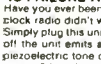
**TRI STATE LED FLASHER KIT**  
Simple to build kit which flashes a tri-state led. The kit has a trimmer control which can be rotated to provide continuous green, alternating red/green, or continuous red. Kit features IC circuitry and jumbo tri-state LED which, even though it's only a two lead device, can flash red or green. Operates from 9V battery. Size of board: 1 1/4" x 1 1/4".  
C4069 \$2.95



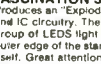
**46WS SLAVE STROBE DC KIT**  
Sensitive slave unit flashes in synchronization with your master strobe. Perfect way to obtain more light for portrait pictures. Comparable units sell for many times this low kit price. Features quality long life straight flashtube, neon ready light, solar cell sensor, heavy duty photoflash capacitor and transistorized inverter circuit. Operates from 4.5VDC to 6VDC. Size of board: 3 1/2" x 2 1/2".  
C4490 \$16.95



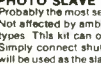
**AC FAILURE ALARM KIT**  
Have you ever been late because the AC went off and your clock radio didn't work, well that need not happen again! Simply plug this unit into the wall outlet and if the AC goes off the unit emits a tone. Features green ready light and piezoelectric tone device. Operates on 9V battery. Size of board: 2 1/2" x 2 1/2".  
C4483 \$4.75



**FASCINATION STAR KIT**  
Produces an "Expanding visual effect using 25 LEDs and IC circuitry. The center LED lights first then the next group of LEDs light and then another set lights until the outer edge of the star lights up. The process then reverses itself. Great attention getter for game rooms, discos, etc. Operates from 9V battery.  
C4432 \$10.95




**PHOTO SLAVE TRIGGER KIT**  
Probably the most sensitive trigger kit on the market. Not affected by ambient light. Much superior than LASCR types. This kit can operate from bounce or indirect flash. Simply connect shutter cord (included) to the strobe that will be used as the slave. When the master strobe is fired the slave strobe will also flash. Size of board: 1 1/2" x 1 1/2".  
C4450 \$6.00



**10 WATT SIREN KIT**  
This kit is perfect for use in burglar alarms, panic buttons, attention getters, etc. Kit produces a loud alternating tone output. Uses two IC's and a power transistor to provide reliable performance. Features variable sound control and 6 to 12VDC operation. Requires 8 ohm speaker. Size of board: 3 1/2" x 1 1/2".  
C4068 \$5.00



**SEQUENTIAL LED FLASHER KIT**  
This kit combines CMOS IC circuitry and 10 jumbo red LEDs to produce a unique visual display. LEDs continuously light sequentially from right to left. Easy to build kit makes a great conversation piece and attention getter. Operates from 9V battery. Size of board: 5 1/2" x 1 1/2".  
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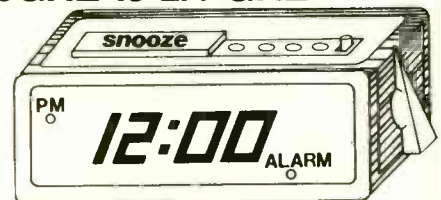
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- Mounting Clamp
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SCOPE: Will receive within the frequency band from satellites, primary microwave stations, and repeater microwave booster stations.

CONTENTS: Completely packaged in 19"x19"x4 1/2" corrugated carton complete with list.

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This system is not a kit and requires no additional devices or equipment other than a TV set to place in operation.

Dealer inquiries invited.



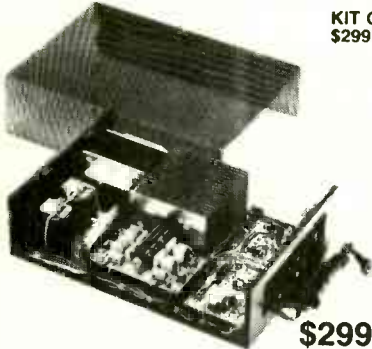
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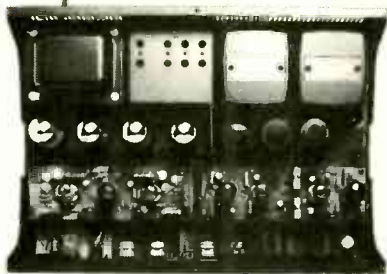


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- Frequency Response 30~30,000 Hz (-1dB)
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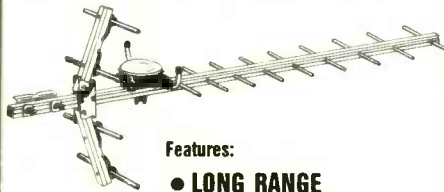


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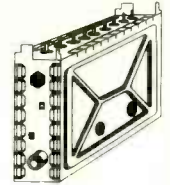
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Freq. Range UHF470 - 889MHz  
Antenna Input 75 ohms  
Channels 14-83 Output Channel 3



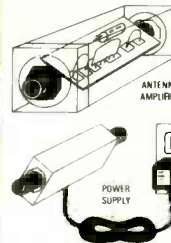
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|---|---------|---|---------|
| 1   | VT1-SW  | Varactor UHF Tuner, Model UES-A56F  | \$34.95 |
| 2   | CB1-SW  | Printed Circuit Board, Pre-Drilled  | 18.95   |
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MODEL ALL-1  
50 MHz — 900 MHz  
12 dB GAIN ± 0.5dB



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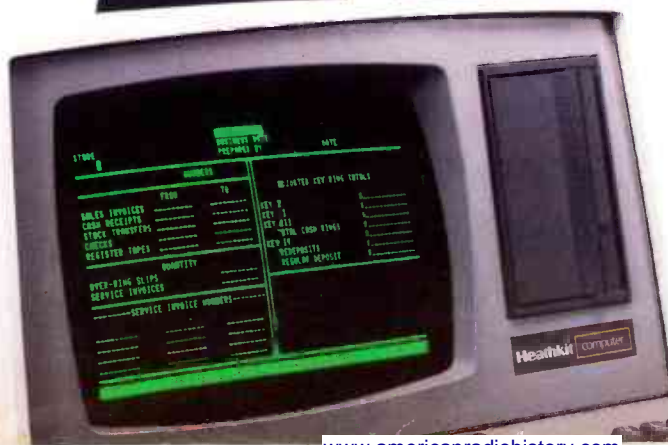
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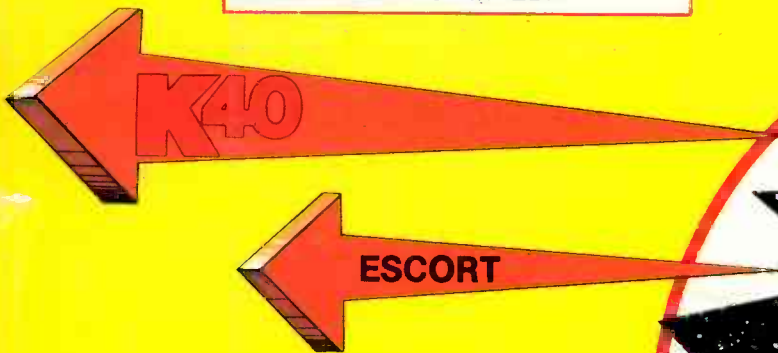
| TEST RESULTS      |                                       |
|-------------------|---------------------------------------|
| MANUFACTURER      | COMBINED X & K-BAND DISTANCE FROM GUN |
| K40               | 2.96 MILES                            |
| ESCORT            | 2.30 MILES                            |
| GUL               | 2.28 MILES                            |
| BEL               | 2.52 MILES                            |
| RADAR INTERCEPTOR | 1.92 MILES                            |
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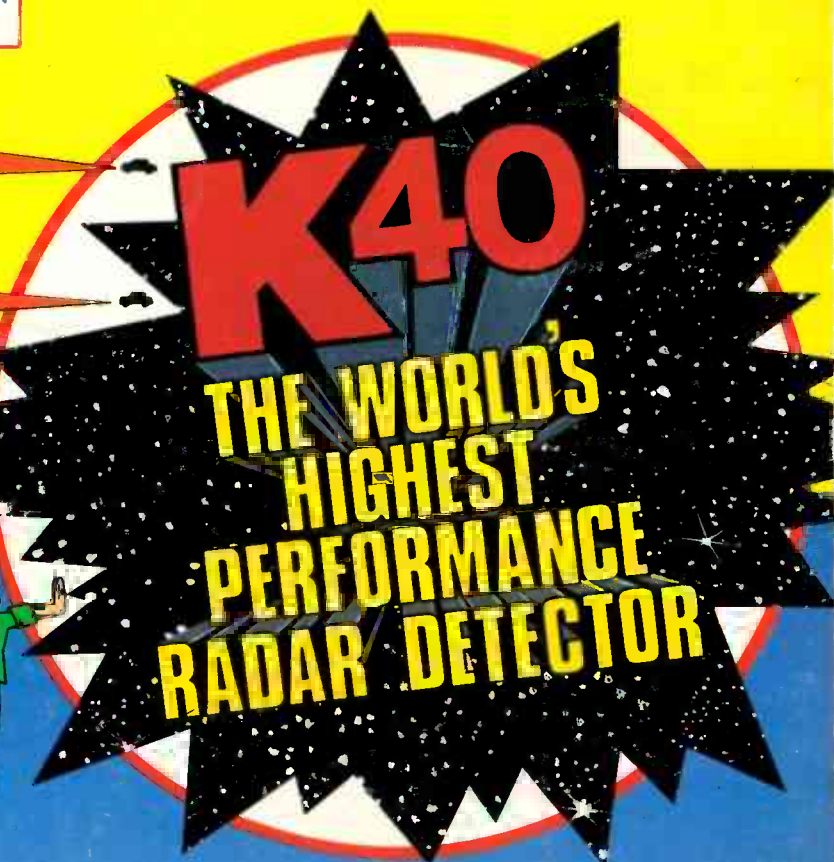
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